

THIRTEENTH MEETING OF THE HIPPARCOS SCIENCE TEAM

ESTEC, 20-21 March 1986

Attendance: HST: Dr. A.M. Cruise  
Dr. M. Crézé  
Prof. M. Grewing  
Dr. E. Hoeg  
Prof. J. Kovalevsky  
Dr. L. Lindegren  
Mr. C.A. Murray  
Dr. C. Turon

(Drs. Donati and Grenon were unable to attend)

ESTEC: M.A.C. Perryman, M. Schuyer, R.D. Wills,  
S. Vaghi

L. Emiliani, K. v. Katwijk, G. Ratier, H.  
O. Pace, M. Setzke, H. Hassan, K. Clausen  
(part-time)

ESOC: J. van der Ha, J. Sternberg

Matra: E. Zeis (part-time)

AGENDA: The agenda given in Annex I was adopted.

1. PROJECT STATUS REPORT

Emiliani reported on the technical and schedule status of the Project (Annex II). Attention was drawn to the forthcoming System Critical Design Review to which HST members were invited to participate, either through document review at their home institute or at ESTEC. (Availability of documentation: 16 May, Review in ESTEC: 20 May - 9 June).

Emiliani announced that he would be leaving his post as Hipparcos Project Manager in April, moving to the Columbus Project in Paris. Later in the meeting it was announced, by M. Delahais, that H. Hassan would take over as acting Project Manager thereafter.

Cruise, on behalf of the HST, expressed thanks to Emiliani for his significant contribution to the project over the past 6 years, and in particular his receptiveness to the scientific goals and requirements as represented by the HST.

2. SPACECRAFT STATUS

Clausen presented an overview of the spacecraft status. Problems areas were confined mainly to AOCS and EPSS. Part of the presentation was devoted to the on-board timing and datation. Offline, further clarification would be made by the Project (Action 1) in the form of a technical note and/or through clarification of the DDID.

3. PAYOUT LOAD STATUS

van Katwijk presented an overview of the payload status (Annex IV). This report covered the present hardware status, recent test results (payload OSTM thermal balance/thermal vacuum, straylight and FPA EM performance tests), future program, and areas still under analysis (contamination: particles and molecular). Kovalevsky stressed the importance of obtaining detailed information on the IFOV profile measurements - results from the FPA EM performance test would be distributed (Action 2).

Ratier presented an overview of the grid calibration methodology developed in TPD (Annex V). Hoeg requested that a uniform notation is used for the grid. Schuyer/Ratier pointed out that the co-ordinate system definitions are given in the Overall System Specification/Payload System Specification/Refocussing Assembly specifications, but that in any case calibration data will be put in a form understandable to the DRC.

#### 4. SYSTEM ASPECTS

a) Grid Ratio Constraints: Wills distributed figures (Annex VI) showing  $M_1$ ,  $M_2$  and the Cramer-Rao bound as a function of slit width. In view of the currently poor controllability of the grid writing process with respect to this parameter, HST were asked to comment on the criticality of the present specifications on slit width ( $3.2 \pm 0.05 \mu\text{m}$ ). Lindegren noted that increasing the slit width has a large effect on the double star observability/detectability, but that this effect has not been quantified. If possible Lund would undertake further simulations to assess the effect further (Action 3). ESTEC would review the impact on the accuracy due to the enhanced  $M_3$  at smaller slit widths (Action 4). Meanwhile MATRA/TPD/CSEM would continue to aim for the specifications. Zeis stressed the potential programmatic impact if the writing can not achieve the present specifications, unless the specification value can be relaxed.

In response to a question by Lindegren, Zeis noted that the value of  $3.2\mu\text{m}$  is a diffraction measurement slit width, the EPBG process having been correspondingly biased to yield such an expected value.

b) Star density constraints on INCA: Schuyer noted that current OBC/ESOC considerations lead to a continuous star density limit of  $2.3 \times$  mean density per FOV (based on 100000 programme stars) in order to arrive at a minimum length of the PSF duration of 5 min. An 'enhanced' Input Catalogue should not exceed this limit. Turon/Crézé considered that their own internal constraints were, in any case, more stringent.

- c) IDT/SM ITF Calibration: Wills noted that the SRD requirements on the IDT ITF is 1%, which is not met for the brightest stars assuming a general ITF model (Annex VII). HST provisionally agreed that the results of the CAPTEC work would be used by Wills to reformulate the specifications accordingly: for the IDT  $\sigma_{itf}/\Gamma_{oo}$  would be relaxed to 5% in the range B=3 to 1 mag, B-V = 0.5. For the SM, requirements would be placed on the ITF calibration only for stars fainter than B=5 mag, i.e. in the range over which the Tycho specifications extend (See also Action 5).
- d) SM Distortion Review: the Project Team's present understanding, which will form the basis of a revision in the appropriate OSS/PLSS specifications, was presented by van Katwijk (Annex VIII).
- e) IFOV Profile Calibration: Wills presented some results of the FPA measurements pertaining to 1 star colour, at different radial distances. Next measurements would come at payload level/PFM FPA testing. Colour effects appeared to be of less importance than the dependence within the FOV, due to the fact that the focus coil currents are optimised for one FOV position and that the focus coil current is therefore not optimum at other FOV positions. Wills noted that the present specifications did not permit the calibration of the long-range part of the IFOV profile because of the unavailability of bright star colours. Kovalevsky/Turon pointed out that all bright stars (say 4000 with  $H < 6$  mag) will have a precision in (B-V) better than 0.1 mag. Kovalevsky stressed that more positions (and not just a radial profile) and measurements further out in the profile are definitely needed.

Wills noted that 8 radial directions are available in the raw measurement data, and this raw data was requested by Kovalevsky. Wills noted that 8 radial directions would also be measured in orbit, but presently limited to 90 arcsec due to the adopted calibration mode. ESTEC would review the possibility of calibrating the longer range IFOV profile in orbit using a stationary IFOV and moving stars (Action 6). Kovalevsky noted his willingness to give inputs to this discussion, if requested.

f) Payload Test Data Availability: Perryman would request MATRA to make available the raw data resulting from the P/L PFM tests of the IDT modulation/SSR/background. Zeis stressed that the tests would not be fully representative in terms of modulation factors, the tape formats may not be easy to interpret, and that only 3 grid periods would be scanned at payload level, although these measurements could be repeated several times.

g) Fast Commissioning Support: outside of the main meeting, Kovalevsky and Emiliani discussed the status of the calibration task within FAST. Manpower problems within FAST meant that Kovalevsky could not presently commit to carry out tasks identified at SRU, Utrecht. Emiliani would investigate allocation of an ESA external fellowship in exchange for such a commitment.

## 5. INPUT CATALOGUE ASPECTS

a) Double stars in INCA: After a presentation by Turon and some discussions, Kovalevsky agreed with the revised Lund criterion for inclusion of double star entries in the Input Catalogue.

Two entries would be retained for stars with  $10 < \rho < 30$  arcsec,  $\Delta M < 2.5$  mag. One entry only for  $\rho < 10$  arcsec. Lindegren noted that, while further simulations were evidently desirable, Lund could not presently undertake to carry these out. To assess whether the SOS worked satisfactorily with this entry concept, Crézé would eventually carry out appropriate simulations.

Murray asked that the choice of cluster stars accounts for the need of a cluster reference frame (e.g. the selected stars should not be distributed linearly). Turon announced that the choice is ongoing, including such a consideration.

b) INCA Contents and Formats: Turon distributed a draft proposal (Annex IX). Lindegren requested a cross-reference to other INCA running numbers related to any given running numbers for each CCDM component. Murray will write to M. Chapront (BdL, Paris) requesting information on major planet ephemerides in same format as for minor planets. Turon will provide a revised proposal, to be reviewed by HST (Action 7).

*Again*  
van der Ha noted that Schütz (ESOC) will start working on the Input Catalogue after June. A meeting towards the end of 1986 might be foreseen between INCA/ESOC to discuss detailed implementation of the Catalogue - it was understood (as outlined in the MIP) that ESOC's work would entail inclusion of information on proper motions, minor and major planets ephemerides, variable stars, and conversion of INCA data to PSF parameters. Turon noted that minor planets updates would go to ESOC every 6 months approximately.

c) PSF Preparation: Crézé presented the current status of the catalogue simulations (Annex X). Items discussed included:

- a 90% survey completeness can be achieved, reasonably uniformly over magnitude. Perryman requested that detailed results are made available, and that the survey definition is rediscussed (e.g. completeness versus target accuracy). Crézé would distribute results to HST/ESA about the end of May (Action 8).
- more stars can be forced in the survey, but at the expense of losing flexibility in the modulation procedure;
- a detailed description of the algorithms would be made within the next 3 months, and these would be discussed with ESOC with the aim of achieving agreement on their implementation (Action 9).
- Murray expressed reservations on selecting 'proper motion only' stars for particular types of observation. He would try to formulate his concerns more explicitly. Kovalevsky would discuss the concept with Walter. Crézé noted that he did not feel particularly happy with the concept. At this stage he was simply showing that such manipulation could be achieved.

## 6. DATA REDUCTION ASPECTS

a) Hoeg presented present plans for TDAC simulation work (Annex XI).

b) Murray reported on the simulated data analysis meeting held in ESTEC on 19 March. Some minor errors in the RGO analysis had been identified (true phase determination, OTF calibration).

Insufficient time had been available to review the CSS results. Lindegren revised the format for IDT data comparison tapes - this was distributed to ESTEC, RGO, CSS and a re-submission of the analysis results on Run 9 was requested by Perryman. The next discussion of the simulated data analysis would be held at the NDAC meeting at RGO (20-21 May).

Cruise distributed a technical note summarising his findings related to the analysis of the FAST SM simulated data.

c) Global Observing Programme: Kovalevsky presented results of continuing work on the GOP carried out by van Daalen et al. at Delft (Annex XIII). Two main conclusions can be drawn:

- with smoothing, errors are degraded more with respect to a geometrical reduction (which itself shows marginal degradation with respect to the nominal GOP) for 1 GC. For one RGC the degradation is not so strong, and a catalogue of 120000 stars should be acceptable in terms of the final achievable accuracy.
- from variable star density experiments, Delft have concluded that local star density enhancements have little effect on the global accuracy at the GCR level, only on the local accuracy.

In view of these results, INCA can proceed in the construction of the catalogue based on a maximum number of 120000 stars, as long as the minimum PSF duration constraint is respected. The finally defined star distribution can then be passed to Delft who could recommend on the global observing time as a function of magnitude for the extreme geometric/smoothing reduction options.

7. ESOC ACTIVITIES (ANNEX XIII)

van der Ha gave an overview of the current ESOC activities, and a short overview of the calibration plans.

van der Ha presented an overview of the proposed Performance Monitoring, and distributed the ESOC Monitoring Software Requirement. HST, and in particular M. Crézé and R. Le Poole, were invited to review this document and provide comments if appropriate (Action 10).

Sternberg presented a status report on the DDID, and a few specific items were clarified. Kite (ESOC) would start working on details of the tape production in the near future. An informal meeting between Sternberg/Kovalevsky would take place to discuss further details at ESOC on 28 April. A future revision of the DDID would include clarification of the timing issues, incorporation of appropriate information from the SICD, and futher details of the housekeeping records.

8. MISCELLANEOUS

- a) Agreement: A sixth draft was distributed. It would be discussed between FAST/INCA at the INCA meeting in Paris on 16 April to which Professors Bernacca and Fricke, the respective Steering Committee Chairmen, would also participate.
- b) French Translation of Ad Astra: Kovalevsky and Turon had been invited to review the appropriate sections of the translation on the DRC and INCA activities.

Perryman reported on the difficulties experienced on the English version with Dr. Dommanget (Bruxelles). Criticisms had been brought to the SPC on the absence of details of the Belgian participation and the work of the Observatoire Royal de Belgique. Letters of complaint had also been written by Obs. Royal (Professor Melchior) to the ESA Director of Science (Professor Bonnet). HST were not in favour of introducing any institute names in the French version of the brochure.

c) ST Proposal: Perryman noted that the proposal for ST time to continue the Hipparcos/Extragalactic reference link was in the process of finalisation. The deadline for the proposals was now 15 September 1986.

9. NEXT MEETING

The next meeting of the HST will be held in ESTEC on 23-24 September 1986, provisionally preceded by a half day meeting on simulated data comparison.

M.A.C. Perryman



# HIPPARCOS

MEETING  
HIPPARCOS  
13 May HST

ACTION No	DESCRIPTION (not more than 4 lines)	REF.	
		DATE 20-21/3/86	PAGE
1	Production of binning technique and/or classification of D000	Next HST	(Schuyler /ESOC) Project
2	Distribute results of FPA EM Performance Test measurements of 1FOV profile to FAST/NOMC as a function of the 5 positions in FOV	1	NEXT MAP
3	Send to perform simulations for double stars at slit width 3.9 um and, if possible, 3.05, 3.35 um.	May 15	L. Lindgren MAP
4	ESTEC to review Acc. Report for effects of M3 on phase error, to assess slit width acceptability	May 15	M. Schuyler MAP
5	ESTEC proposed new spec on SM/DT ITF given in main minutes communicate unacceptability to ESTEC; propose alternative calibration method if unacceptable	May 15	HST MAP
6	Review possibility of long-range 1FOV profile calibration	Next HST	M. Schuyler MAP
7	HST to review ESOC Monitoring S/W Requirements Document	April 30	HST/Les Pack/Gezze MAP
8	Distribute further results of simulation work to HST/ESA	May 31	M. Cizek MAP
9	ESTEC/HST to review draft INCA contexts / formats	Next HST	ESTEC/HST/ESOC MAP
9	Create to propose PSF preparation algorithms for consideration by ESTEC/ESOC	July 31	M. Cizek MAP
Signatures			

Thirteenth Meeting  
of the  
HIPPARCOS SCIENCE TEAM  
20-21 March 1986  
Agenda

Place: Room 32004      Start: 09.30

1. Project Status Report (L. Emiliani, 10 mins)
2. Payload Status Report:
  - mirrors/detector/grid status (K. van Katwijk, 30 min)
  - thermal vacuum tests report (K. van Katwijk, 20 min)
  - grid calibration methodology (L. Fontijn, tbc, 30 min)
3. Spacecraft Status Report (K. Clausen, 30 min)
4. Input Catalogue (120 min):
  - double star status and DRC requirements (C. Turon)
  - INCA contents and formats (C. Turon)
  - PSF preparation/algorithms (M. Creze)
5. Miscellaneous (60 min):
  - Agreement
  - Ad Astra, French translation + publicity plans
  - ST proposal status (delay to 15 September)
6. ESOC Activities (120 min):
  - general status report (J. van der Ha)
  - DDID status, including raw data archive (J. Sternberg)
  - plans for payload monitoring (J. van der Ha)
  - calibration (J. van der Ha)

Friday

7. System Aspects (120 min):
  - star density constraints on INCA (M. Schuyer)
  - SM/IDT ITF calibration (R. Wills)
  - SM distortion review (K. van Katwijk)
  - IFOV profile calibration (R. Wills)
  - grid ratio constraints (E. Zeis, tbc)
  - timing tech. note status (M. Schuyer/J. van der Ha)
  - payload test data availability (E. Zeis, tbc)
  - FAST commissioning support status (S. Vaghi)
8. Data Reduction Aspects (90 min):
  - Simulated data analysis debrief (C. Murray)
  - NDAC processing of FAST SM data (M. Cruise)
  - TDAC planning (E. Hoeg)
9. AOB/Next Meeting



HIPPARCOS SUMMARY STATUS

(20.03.1986)

P R E S E N T A T I O N

T O T H E

HIPPARCOS SCIENCE TEAM

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## SATELLITE STATUS

### QUALIFICATION

#### MAJOR ACHIEVEMENT :

- S/L STRUCTURAL MODEL SUCCESSFULLY QUALIFIED IN STATIC/AcouSTIC/VIBRATIONS

INTESPACE  
FEB. 1986

#### NEXT STEP :

- THERMAL QUALIFICATION BY FOKKER

IABG  
JUNE 1986

### BUDGETS

- MASS                    STILL CRITICAL (NEED FOR CERENKOV SHIELDING) - SEEKS UNDER CONTROL.

- POWER                EXTREMELY CRITICAL (NEGATIVE MARGIN SAA 0° ECLIPSE !)  
NOT YET UNDER CONTROL BECAUSE :

- a) Difficult to get freezing of heater power
- b) Difficult to get EOL figures derived from EM measurements and WCA
- c) Difficult to get reliable measurements on certain EM units



### MISSION PERFORMANCES

CONFIDENCE THAT THE 2 mas SPEC WILL BE ACHIEVED HAS BEEN GAINED FROM OSTM-EM TEST RESULTS :

### MAJOR ACHIEVEMENTS

- P/L MECHANICAL/THERMAL STABILITY SUCCESSFULLY VERIFIED DURING TB/TV TESTS
- P/L STRAYLIGHT TESTS SUCCESSFULLY COMPLETED
- FPA FUNCTIONAL TESTS SUCCESSFULLY PERFORMED
  - (FPA ready to undergo mechanical tests)

### NEXT STEPS

- VERIFICATION OF EM OPTICAL PERFORMANCES OF TELESCOPE (WFE)
- End-to-end P/L tests on EM

OTHER ACHIEVEMENT : On orbit calibration fully settled through delivery to ESA of operational software requirements (CAPTEC)

Planned April /  
May 1986

July to October 86

IAL LIEGE NOV 85

MATRA DEC 85

MATRA FEB 86



## SYSTEM DESIGN

### THREE MODIFICATIONS :

- HIPPARCOS WILL NOW BE LAUNCHED BY ARIANE IV  
DUA has been agreed between MATRA and ESA and submitted to ARIANESPACE  
One open point : date of updated coupled analysis
- IMPLEMENTATION OF SHIELDING AGAINST PARTICLES (CERENKOV EFFECT) IS ON-GOING
- POTENTIAL OPERATIONAL CHANGE : N2H4 SUN ACQUISITION SEQUENCE
  - . 10 RPM deployment implemented
  - . Feasibility study completed by MATRA CMT
  - . Decision to be taken by ESA mid-March

## SYSTEM TECHNICAL CONCERNS

### CONTAMINATION

Molecular contamination  
Particulate contamination

### ESD

Grounding of all conductive items not yet guaranteed : detailed review is on-going at MATRA and the point will be discussed with each concerned subcontractor.

### RADIATION EFFECTS

On optical transmitting elements (grid, relay optics) are still under detailed assessment.



## SCHEDULE

- Successfull achievements (with respect to delayed dates agreed in September 1985) :
  - P/L OSIM and EM
  - On Board software V1
  - S/C structure
  - S/C Harness
  - Data handling S/S
  - EGSE and integration preparation at AERITALIA
- Some delays encountered for Telecommunications S/S  
Thermal Control S/S
- Most critical areas (EM)
- EPSS } All possible work-around solutions at system level have now been exhausted and  
- AOCS } any additional delay wrt dates set in January 1986 directly impact the satellite.
- PFM schedule extremely critical :
  - Detection S/S is the most critical
  - S/C S/S PFM deliveries not completely secured.

## HIPPARCOS SYSTEM CDR

- ° KEY DATES

	AVAILABILITY OF DOCUMENTATION FROM MATRA .....	MAY 16, 1986
CDR KICK-OFF	.....	MAY 22, 1986
REVIEW IN ESTEC	.....	MAY 20 - JUNE 9, 1986
REVIEW IN MATRA	.....	JUNE 16-20, 1986

- ° REVIEW PANELS (ESTEC REVIEW)

SYSTEM  
MISSION PERFORMANCE  
AIV  
P.A. & CONF. MGMT.  
SOFTWARE  
THERMO-MECHANICAL  
AVIONICS  
ELECTRICAL  
AOCS  
OPTICS & DETECTION

NOTE : PANELS FOR REVIEW IN MATRA SLIGHTLY DIFFERENT

- ° SELECTED HST MEMBERS ARE INVITED TO PARTICIPATE IN MISSION PERFORMANCE PANEL



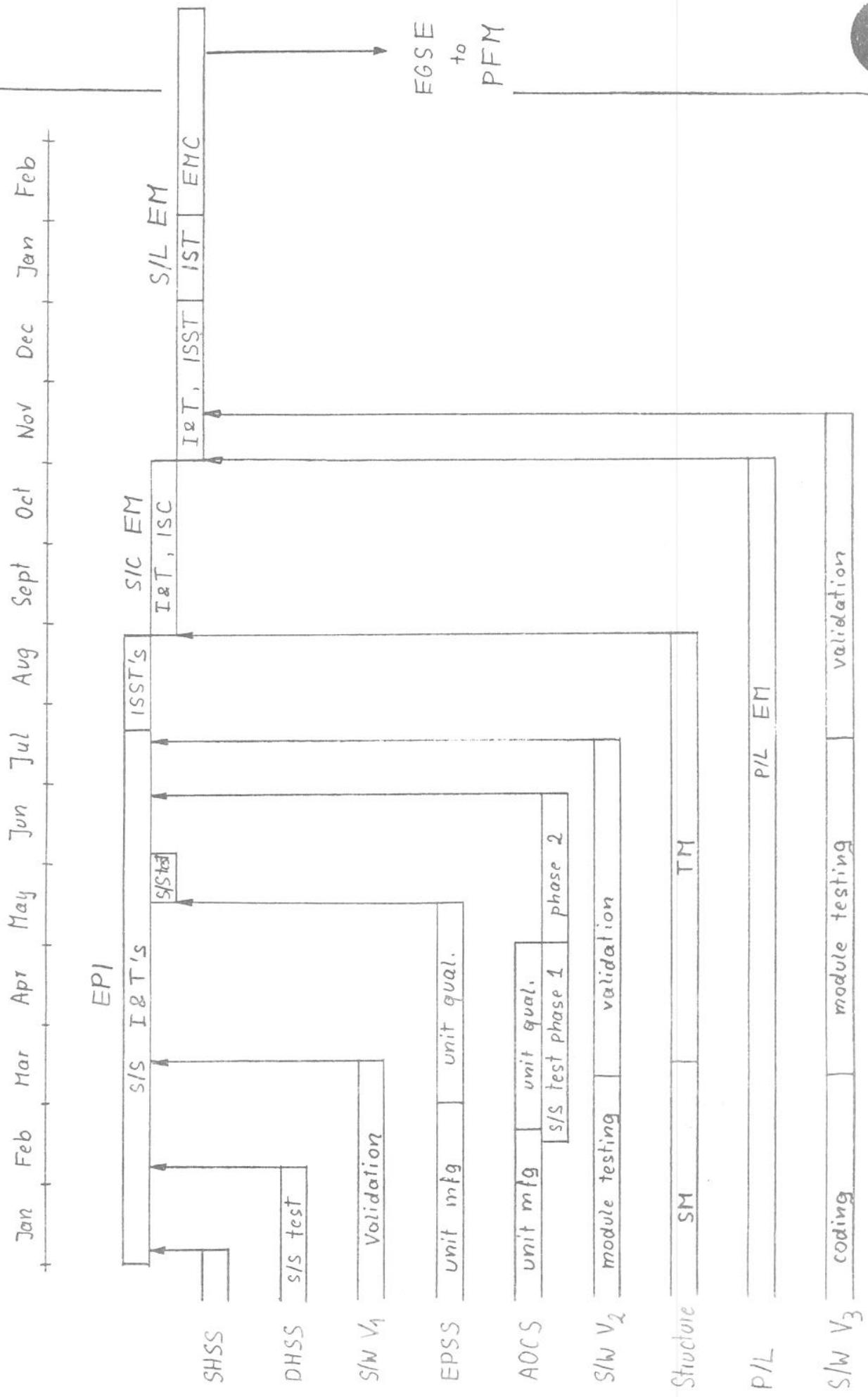
ANNEX III



K. CLAUSEN

HST MEETING - MARCH 86

S/C STATUS



S/C SYSTEM ISSUES:

INITIAL SUN ACQUISITION

CHANGE FROM SLEW WITH COLD GAS RCA AT 1 R.P.M.

TO SLEW WITH HYDRAZINE RCA AT 10 R.P.M.

RTAD INITIALIZATION

TRADE OFF BETWEEN PERFORMANCE OF SUN POINTING ON BOARD  
AND COMPLEXITY OF ISPR ALGORITHM ON GROUND

RTAD GROUND SUPPORT FOR OCCULTATION AND ECLIPSE

ASSESSMENT OF GYP - SM THERMAL DISTORTION RATE AND IMPACT ON RTAD  
REQUIRED ATTITUDE AND RATE UPDATE FROM GROUND

## TIMING AND DATATION

SCIENTIFIC DATA:

- DATATED WITHIN A TM FORMAT BY FOLLOWING SYNCHRONIZATION SCHEME (H/W IN FGE)

BCP 1	15/160 Hz	TM FORMAT START
BCP 4	150 Hz	IDT PILOTING
IDT SAMPLE	1200 Hz	IDT, SM SAMPLING

DELTA BETWEEN BCP 1 AND BEGIN OF TM TRANSMISSION IS IN "DATATION CHANNEL"

- ACCURACY ALLOCATION

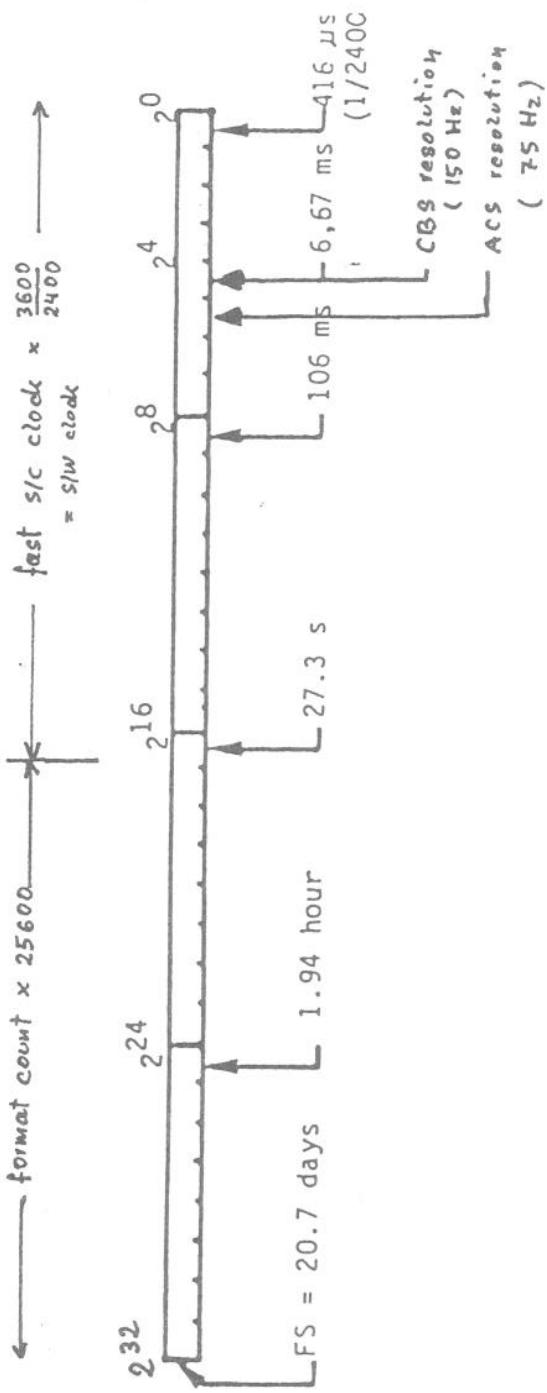
S/L:	IDT SAMPLE TO TM FRAME SYNC	±	4 $\mu$ s ABSOLUTE
		±	3,5 $\mu$ s STABILITY OVER 1 FRAME
G/S:	TM FRAME SYNC TO UTC	±	1 ms ABSOLUTE
		±	1,5 $\mu$ s STABILITY OVER 5 MINUTES

## TIMING AND DATATION

### ON BOARD CLOCKS:

- |   |      |      |                         |                  |
|---|------|------|-------------------------|------------------|
| - | OBC  | H/W: | 3600 Hz RESET WITH BCP1 | (FAST S/C CLOCK) |
|   | S/W: |      | 2400 Hz RESET WITH BCP1 | (FICTIONOUS)     |
| - | CLE  | H/W: | 9360 Hz RESET WITH BCP4 | (ESS DATATION)   |
|   | S/W: |      | 75 Hz RESET WITH BCP1   | (INTERRUPT)      |

ON BOARD TIME







HIPPARCOS SCIENCE TEAM  
MEETING 20-21 MARCH 1986

PAYLOAD STATUS REPORT

PREPARED BY  
K.VAN KATWYK

## CONTENTS

- PRESENT HARDWARE STATUS
- RECENT TEST RESULTS
- NEAR FUTURE PROGRAM
- AREAS STILL UNDER ANALYSIS
- ANNEXES A,B,C

## PRESIDENT HARDWARE STATUS

### MIRRORS

TECHNOLOGY : PADS' REDESIGN INDUCING POLISHING  
 DIFFICULTIES (TRIANGULAR  
 ASTIGMATISM  $\rightarrow$  DIFFERENTIAL DEFOCUS)

MODEL	WFE	CHROMA	
BEAMCOMBINER *	$\approx \lambda/20$	$\approx 0.8 \text{ mas}$	CUTTING TO BE DONE
	$\approx \lambda/50$	$\approx 0.6 \text{ mas}$	
	$\approx \lambda/60$	$\approx 1.0 \text{ mas}$	
FLATFOLDING MIRROR	$\approx \lambda/96$	$\approx <1 \text{ mas}$	OLD PADS DESIGN
	$\approx \lambda/40$	$\approx ? \text{ mas}$	NOT READY
SPHERICAL MIRROR	$\approx \lambda/91$	$\approx <1 \text{ mas}$	OLD PADS DESIGN
	$\approx \lambda/50$	$\approx ? \text{ mas}$	NOT READY

\* PERFO REQU'TS SIMULTANEOUSLY FOR BOTH FOV'S

## PRESENT HARDWARE STATUS

### GRID + DEFLECTORS

TECHNOLOGY : VARIATION OF SLITWIDTH (GRIDRATIO) SEE  
DEDICATED PRESENTATION

"CERENKOV MASKS" ON DEFLECTORS DEFINED

### BEST AVAILABLE GRIDS (BOTH OUT OF SPEC)

Fg . SCANFIELD ORIENTATION SLIGHTLY OUT OF SPEC

• SLITWIDTH  $3,52 \pm 0,03 \mu\text{m}$

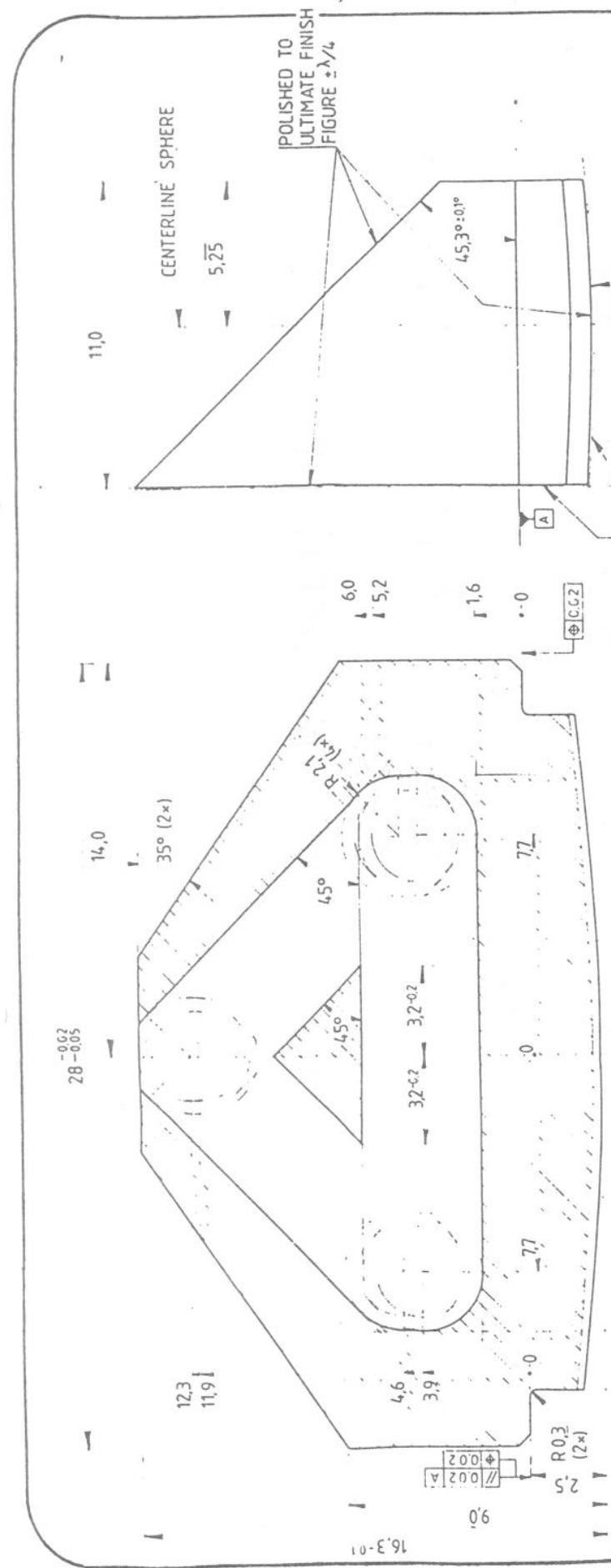
F10 . CHEVRON PATTERN (1,3,2) REVERSED WRT VERTICAL

• SLITWIDTH  $3,28 \pm 0,02 \mu\text{m}$

### STRUCTURE + THERMAL CONTROL

SHIELDING AGAINST CERENKOV EFFECT IMPLEMENTED  
(BASED ON BACK GROUND NOISE  $\text{IBG} = 84 + 10\%$  MAIN CHAIN

$\text{IBG} = 2400 + 50\%$  SN-CHAIN  
SUBSYSTEMS QUALIFIED, PFM H/W IN PRODUCTION

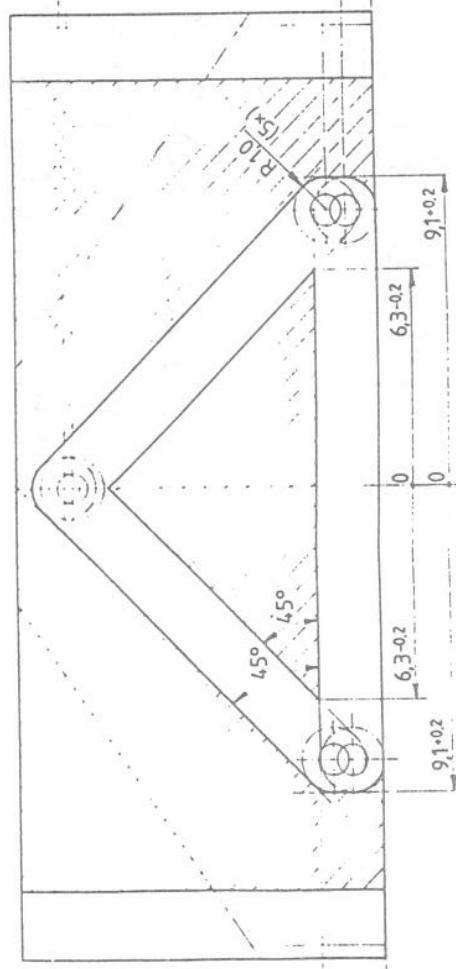


(5) Date 19/3/86



AR-IRALIN COATING

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TECHNISCHE DIENST TWO - TH DELFT

## PRESENT HARDWARE STATUS

- RELAY OPTICS TECHNOLOGY: DARKENING OF GLASSES DUE TO IRRADIATION ; DIFFICULTY TO SHIELD AGAINST SOLAR FLARE PROTONS  
CERENKOV SHIELDING IMPLEMENTED  
FILTERS (GG-375) IN BT-CHANNEL IMPLEMENTED
- FOCAL PLANE BAFFLE VIGNETTING FOR EXTREME SM POINTS RESOLVED  
( $<1\%$  VS  $5\%$  REQU'IT)  
MODIFICATION TO BE IMPLEMENTED

## PRESENT HARDWARE STATUS

- DETECTION  
TECHNOLOGY : HIGH TENSION SUPPLY (TRAFOS) CRITICAL  
EM-RESULTS MAIN DETECTOR ASSY : AS EXPECTED  
STARMAPPER ASSY : DETECTION EFFICIENCY  
LOWER THAN EXPECTED ON TUBE, BUT OK  
EM EQUIPMENT USED IN FPA-EM TESTING  
FPM HARDWARE IN PRODUCTION / UNDER TEST

## RECENT TEST RESULTS

### Payload OSTM TBTU TEST (Oct/Nov'85) SEE ANNEX A

- EXTREMELY STABLE SHORT TERM TEMP. CONTROL
- COUPLING BETWEEN EXTERNAL ENVIRONMENT AND PERFO LIKE BASIC ANGLE VARIATION + GRID ROTATION
- HEATER POWER DEMAND OF PAYLOAD TO BE FINALISED
- SPGRID PERFO : RESOLUTION BETTER THAN 5 nm (6,7 mas)
- TEST ASSESSMENT REPORT STILL OUTSTANDING  
(CONVERSION FROM BC  $\gamma = 20'$  TO BC  $\gamma = 58^\circ$ ;  
INTERPRETATION OF MOISTURE RELEASE EFFECT  
ON REFOC PRESETTING )

## RECENT TEST RESULTS

- STRAY LIGHT TEST (DEC'85) SEE ANNEX B  
MEASUREMENT OF ATTENUATION RELATIVE TO POINT SOURCE AT VARIOUS FIELD POSITIONS + EXTRAPOLATION TO EARTH/MOON CONFIGURATIONS  
STRONG INFLUENCE OF REFLECTION OF CENTRAL PART OF BEAM COMBINER (UNPAINTED ZERODUR)  
→ IMPROVEMENT WITH BLACK FOIL COVER AT CENTRAL PART (ALSO FOR ESD REASONS)  
Good CONFIDENCE TO MEET STRaylight PERFO  
FOR PFM HARDWARE.

## RECENT TEST RESULTS

- FPA EM PERFO TEST (JAN/FEB'86) SEE ANNEX C  
PERFO LIMITATIONS DUE TO  
OPTICAL QUAUTY OF PROJECTOR  
VIBRATION OF SCANNING SOURCE  
VIBRATION OF TEST ROOM  
LIGHTLIGHTNESS OF TEST SPECIMEN
- ACHIEVEMENTS :  
MECHANISM REPRODUCIBILITY  
PILOTING CAPABILITY  
FOV PROFILE (SLIGHTLY OUT OF SPEC)
- DYNAMIC/INTEGRITY TESTS  
SATELLITE STM COUPLED TEST (FEB'86)  
PAYLOAD OSTM DELTA QUALIF TEST (MAR'86)

## NEAR FUTURE PROGRAM

EM TELESCOPE WFE TEST IN VACUUM (APR/MAY '86)  
PAYLOAD PERFO TEST (JULY/SEP '86)

PFM HARDWARE DELIVERY (MAY/JUNE '86)  
TELESCOPE WFE TEST IN VACUUM (AUG '86)  
FPA PERFO TEST (AUG/SEP '86)



ANNEX IV



G R I D C A L I B R A T I O N M E T H O D O L O G Y

(DEVELOPED IN T.P.D. BY MR. FONTIJN)

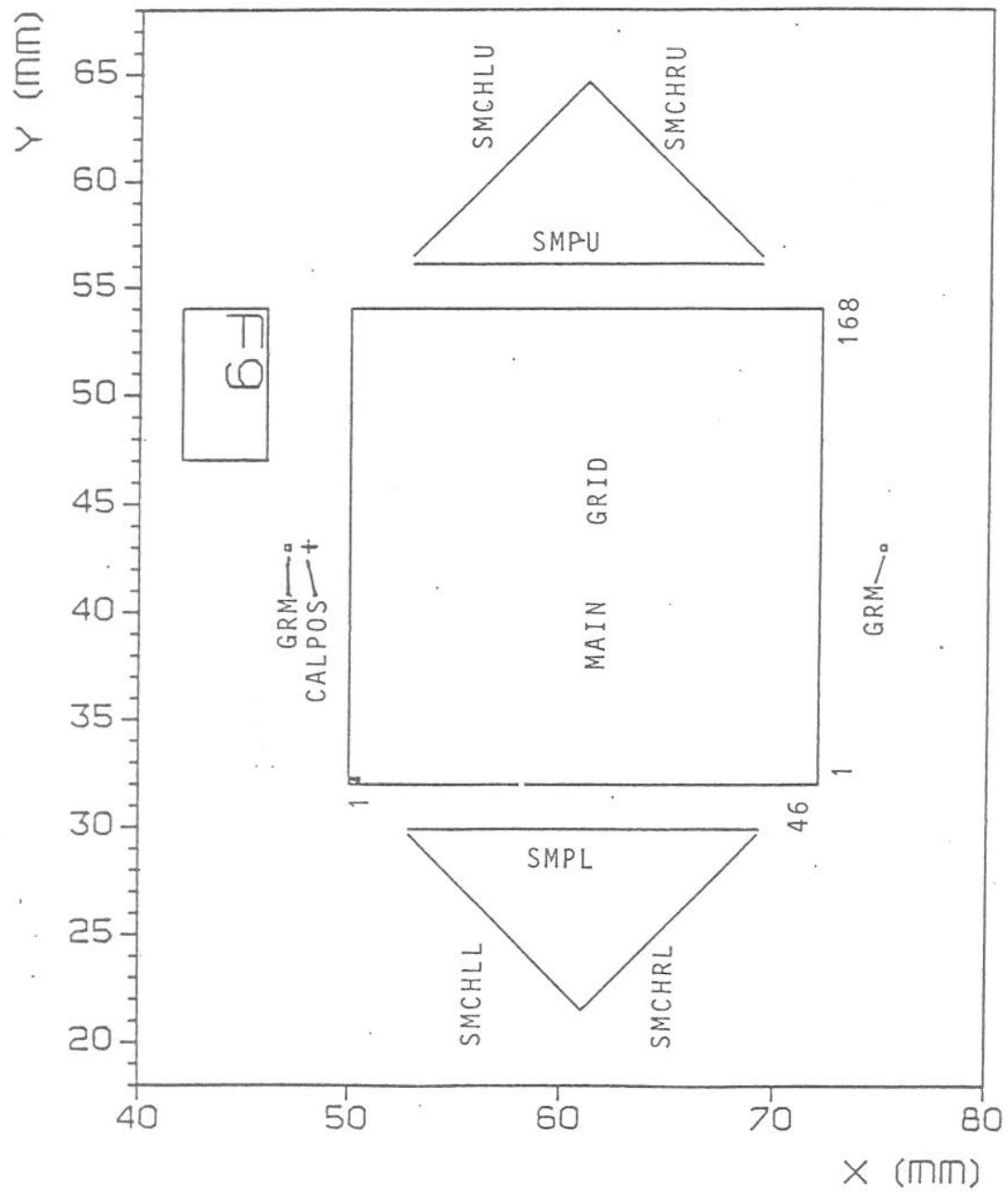
G. RATIER

HST 20 MARCH 1986



## GRID CALIBRATION SEQUENCES

- MANY SEQUENCES ARE USED FOR CHECKING THE PERFORMANCES/ADJUSTMENT OF THE TPD EBPG MACHINE.
- SOME SEQUENCES ARE USED TO VERIFY THAT THE MANUFACTURING REQUIREMENTS ARE MET (E.G., S.S.I.)
- M.S.I. CALIBRATION IS PERFORMED ON MAIN GRID (MG) AND STAR MAPPER (SM).



ABBREVIATIONS USED IN GRID CALIBRATION



SEQUENCE (DURATION)	SUBSEQUENCE (FILE #)	# OF SCANFIELDS MEASURED	# OF SLITS MEASURED PER SCANFIELD	PURPOSE
MG1 (49 mm)	MG1.1 (001)	4	8	Verify the presence of all scan-fields & calibration pattern CALPOS. Determine the overall grid gains & rotations.
	MG1.2 (002)	1	1 (10 times)	Test the EBPG measurement accuracy for slit width and position
	MG1.3 (003)	1	8 (10 times)	Test the repeatability of scan-field measurements
	MG1.4 (004)	1	80 (10 times)	Derive the scanfield distortion and test its repeatability
	MG1.5 (005)	16	80	Assess the SSI properties and uniformity of the scanfield distortion
	MG1.6 (006)	16 (same as in MG1.5)	8	Test the effect of the number of slit measurements per scanfield
	MG1.7 (007)	16 (same as in MG1.5)	1	Test the MSI determination accuracy with a single measurement at scanfield center
	MG1.8   MG1.9 : (008) (009)	REPEAT OF MG1.7		
	MG1.10 (010)	4 X 46 (4 rows)	1	Assess the MSI transverse gradient (coarse)

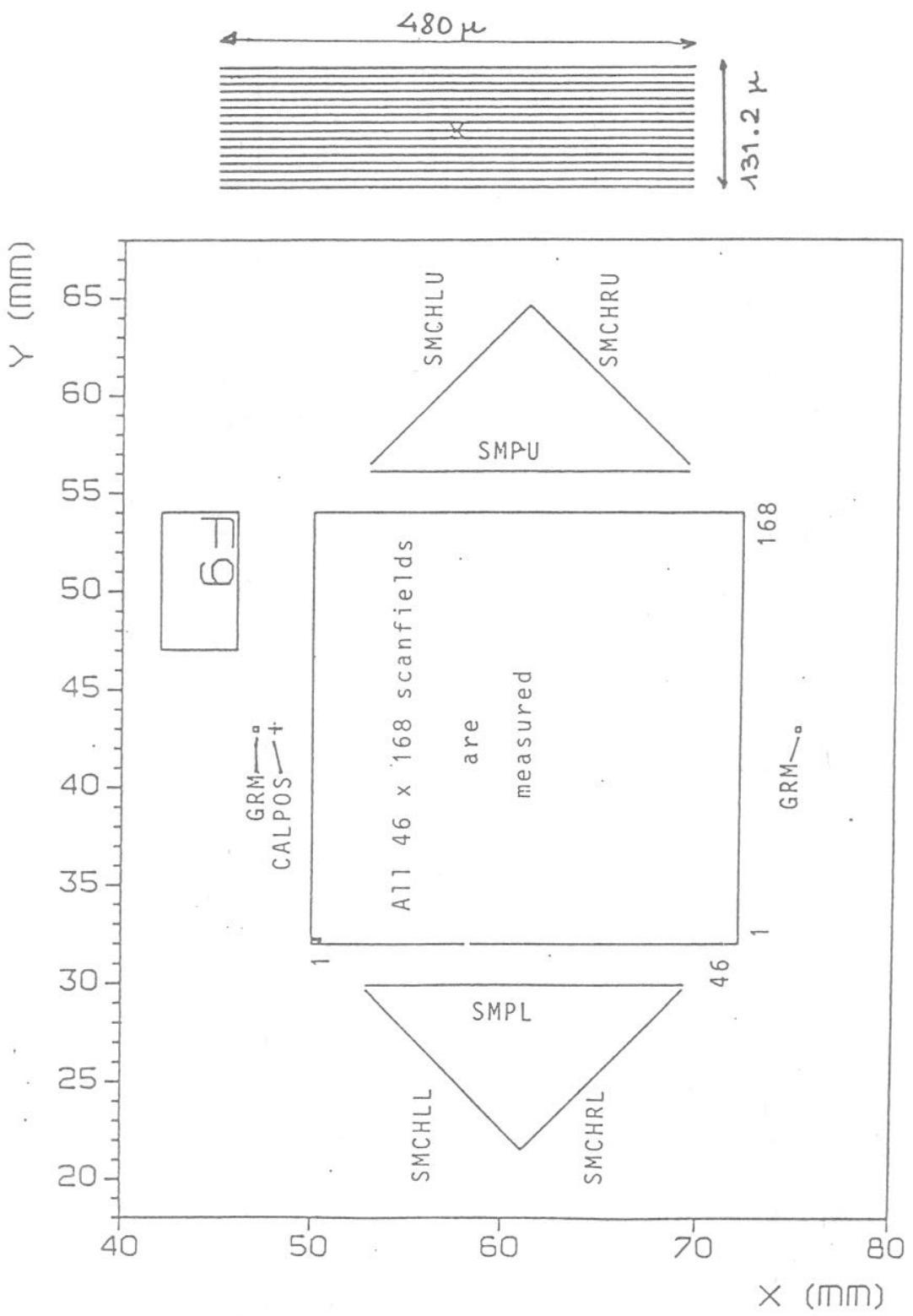
MAIN GRID



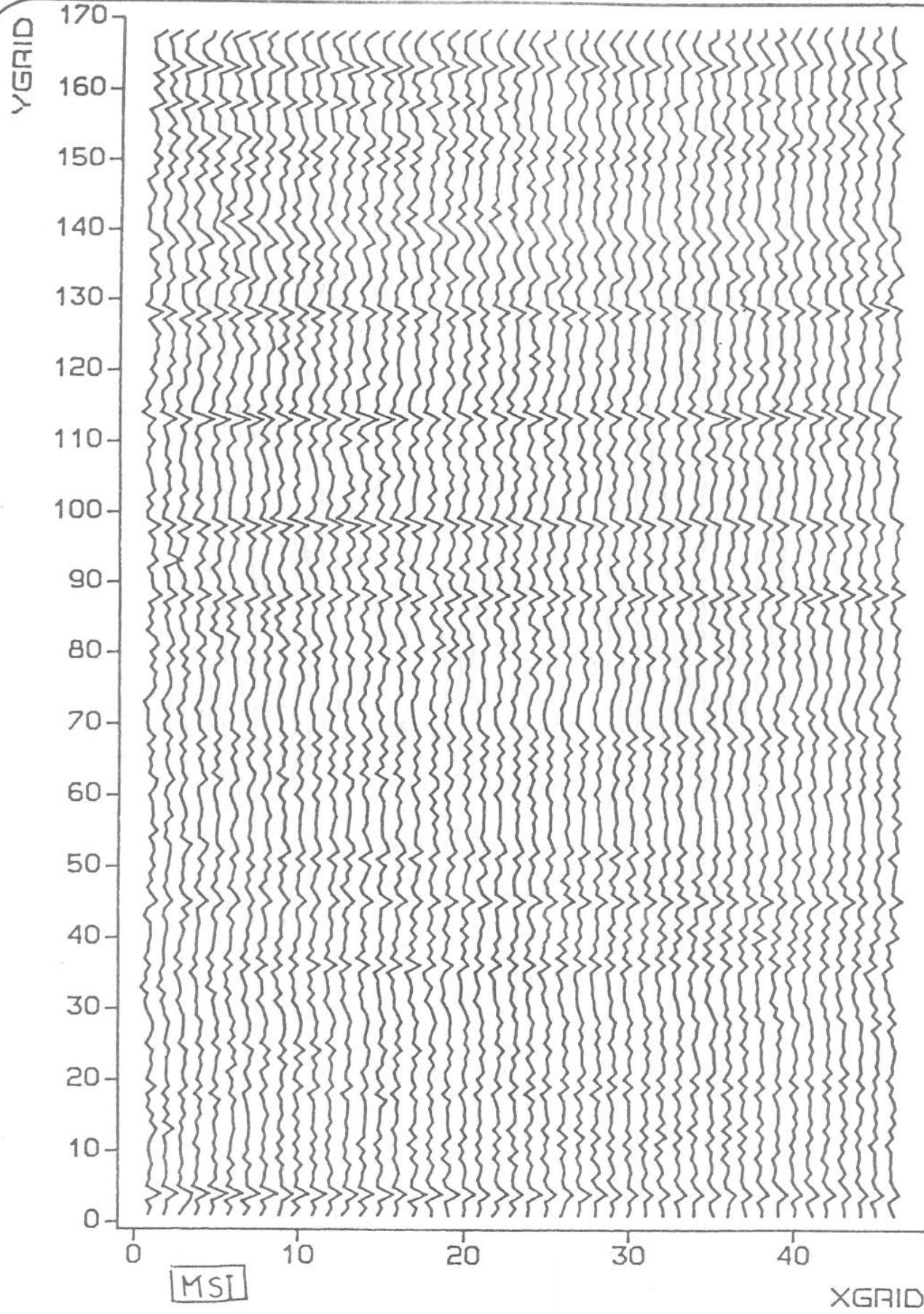
SEQUENCE (DURATION)	SUBSEQUENCE (FILE #)	# OF SCANFIELDS MEASURED	# OF SLITS MEASURED PER SCANFIELD	PURPOSE
MG. CSEM (4 mn)	(011)	46. (1st row)	2	Compare TPD measurements with CSEM optical data on the same slit
MG. DIFFR (6 mn)	(012)	20 (center of MG)	12	Derive a mean slit width for comparison with optical diffraction measurements and derive the corresponding correction factor
MG2 (50 mn)	MG2.1 (013)  MG2.2 (014)	4 X 16 (same as MG1.10)  4 X 56 (Center part of 4 lines)	8  8	Assess the MSI transverse gradient (fine)  Determine the scanfield rotation (correlated/uncorrelated parts)
(2 H 44 mn)	MG3.1 (015)	46 X 168 (all scanfields)	1 (scanfield center)	Derive the MSI matrix

MAIN GRID

Date



MAIN GRID CALIBRATION SEQUENCE

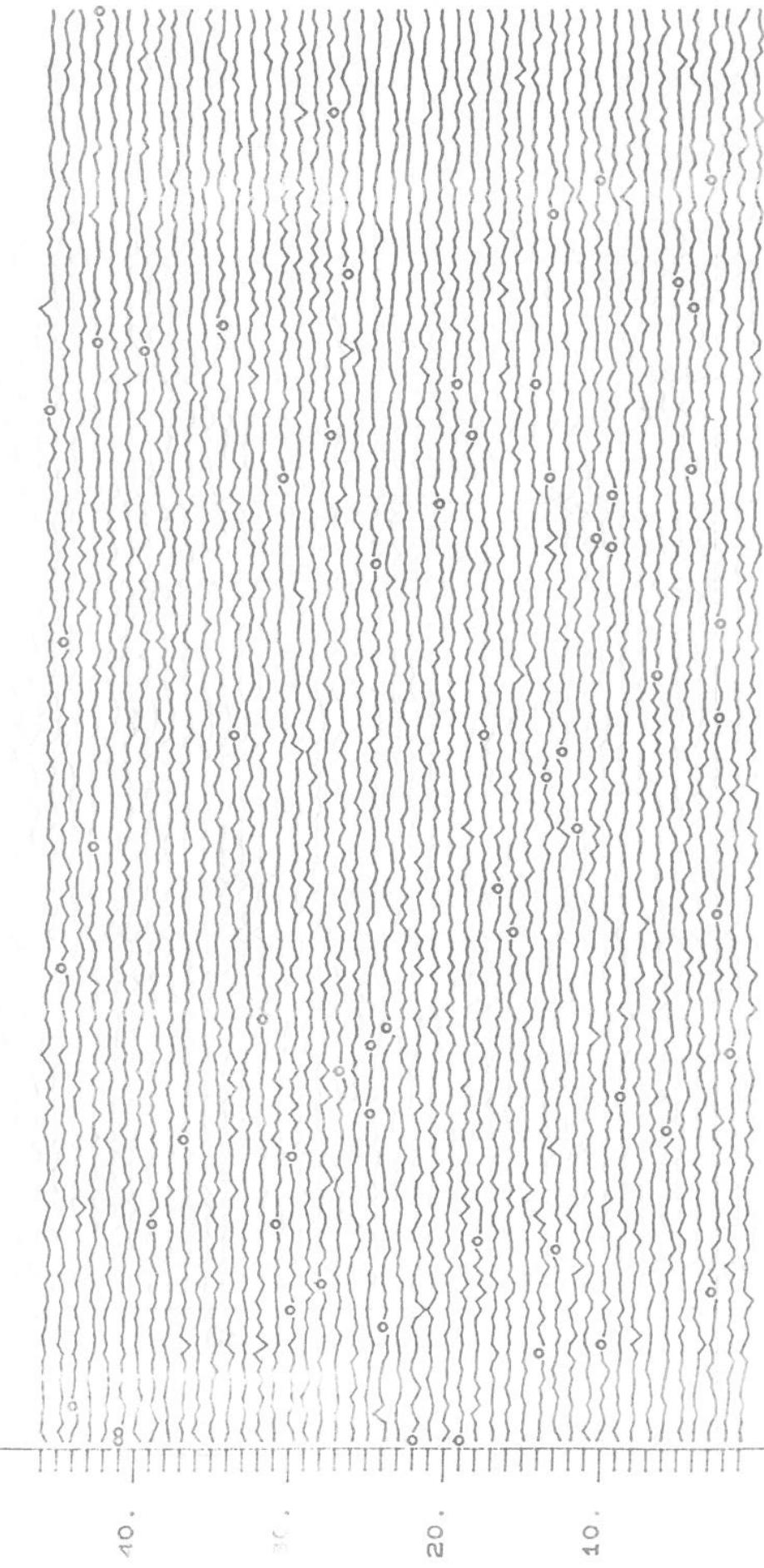


FILE T.TPDPO8AO15

MEAN SLITWIDTH : 3292.

SLITWIDTH ON THE WHOLE GRID  
X-SCANFIELD

SCALE 1 200.NM



Y-SCANFIELD

10.0, 20.0, 30.0, 40.0, 50.0, 60.0, 70.0, 80.0, 90.0, 100., 110., 120., 130., 140., 150., 160.

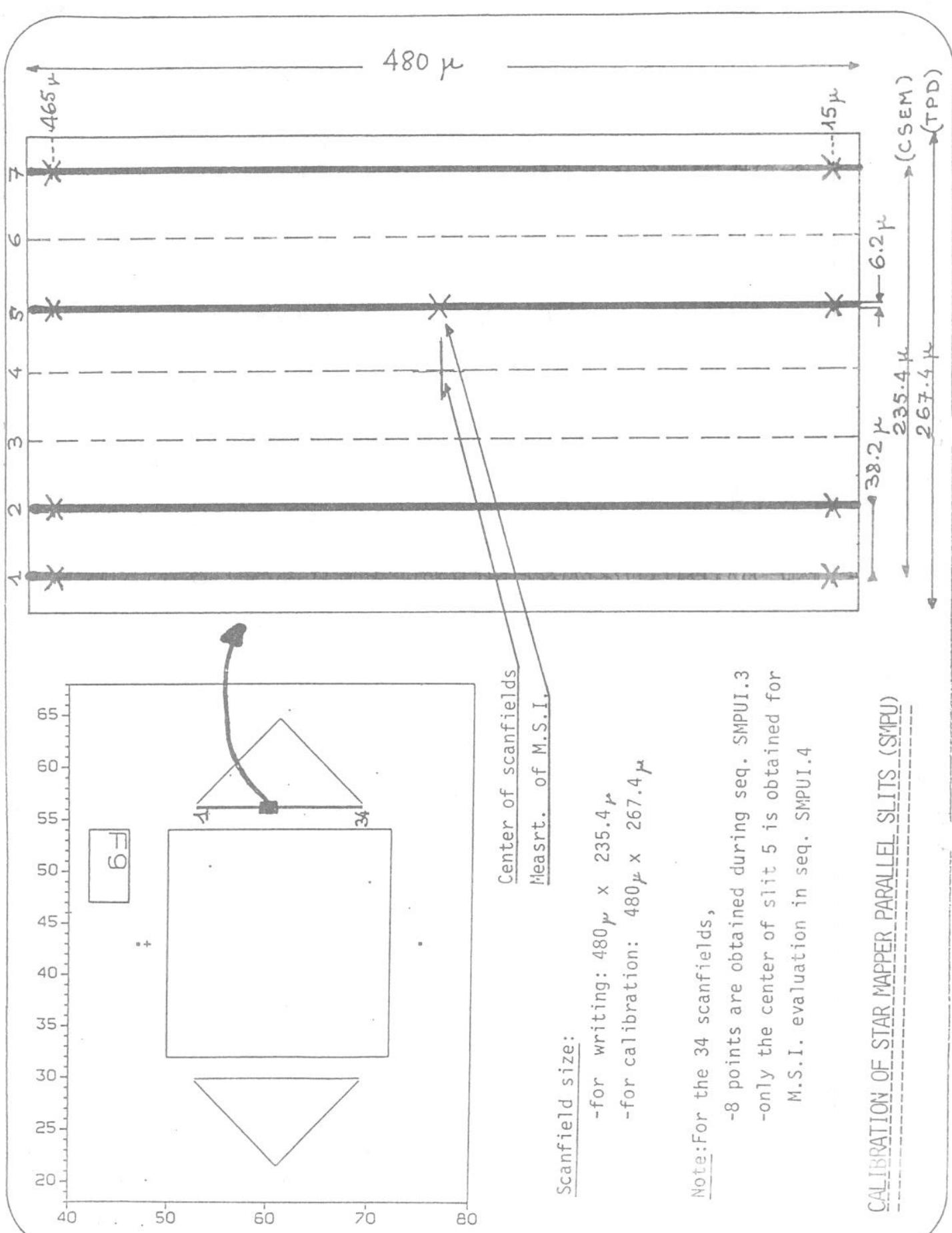


SEQUENCE (DURATION)	SUBSEQUENCE (FILE =)	= OF SCANFIELDS MEASURED	= OF SLITS MEASURED PER SCANFIELD	PURPOSE
SMPUI.1 (11 mn)	SMPUI.1 (016)	1	20 (5 times)	Determine the scanfield pattern
	SMPUI.2 (017)	1 (same as SMPUI.1)	8 (5 times)	Test the effect of the number of measurements upon scanfield determination
	SMPUI.3 (018)	34 (all scanfields of SMPUI)	8	Derive MSI, scanfield gain, rotation and assess SSI
	SMPUI.4 (019)	34	1	Derive MSI for <u>SMPU</u>
SMPUI.1 (11 mn)	(020 to 023)	Same sequence as above for SMPL		
SMCHLUI.1 (14 mn)	SMCHLUI.1 (024)	1	7 X 4	Determine the scanfield pattern
	SMCHLUI.2 (025)	1 (same as in SMCHLUI.1)	2 X 4	Test the effect of the number of measurements upon scanfield determination
	SMCHLUI.3 (026)	1 (same as in SMCHLUI.1)	4 X 4 (moved by 2 m)	Check small scale periodic effect
SMCHLUI.C0.3 (027 to 029)	Same as SMCHLUI.2 for 3 different scanfields			

STAR MAPPER GRID

Date:

CE



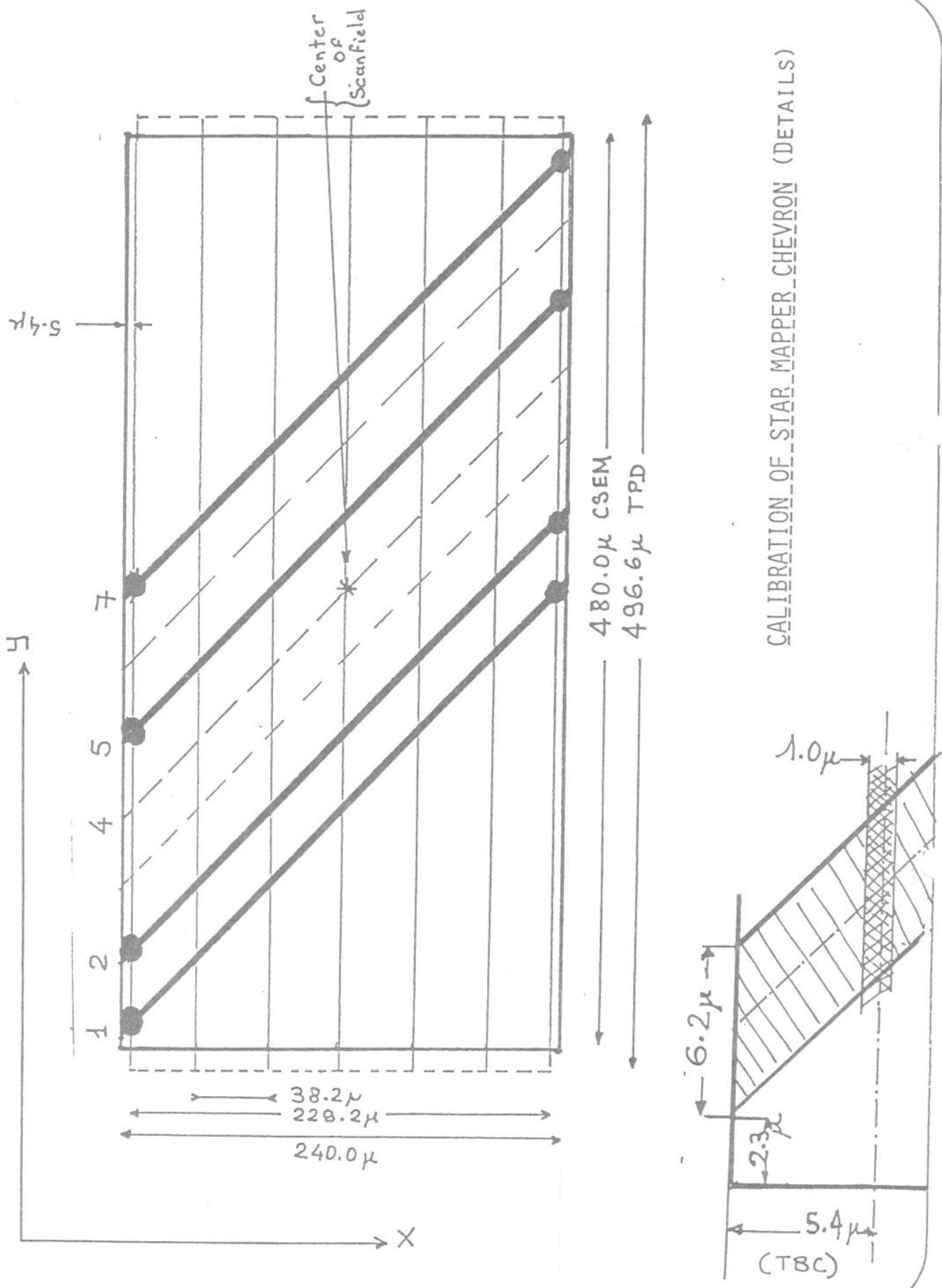
Date .....



SEQUENCE (DURATION)	SUBSEQUENCE (FILE =)	= OF SCANFIELDS MEASURED	= OF SLITS MEASURED PER SCANFIELD	PURPOSE
SMCHRUS1 (14 mn)	Same as (030 to 035)	SMCHLU1	for	SMCHRU
SMCHLL1 (14 mn)	(036 to 041)			SMCHLL
SMCHRL1 (14 m)	(042 to 047)			SMCHRL
SMCHLU2 (1 H 30 mn)	SMCHLU2.CO.34 (048 to 081)	34 (all scanfields for SMCHLU)	2 X 4	Derive MSI for SMCHLU
SMCHRU2 (1 H 30 mn)		Same as above for SMCHRU (082 to 115)		
SMCHLL2 (1 H 30 mn)		Same as above for SMCHLL (116 to 149)		
SMCHRL2 (1 H 30 mn)		Same as above for SMCHRL (150 to 183)		

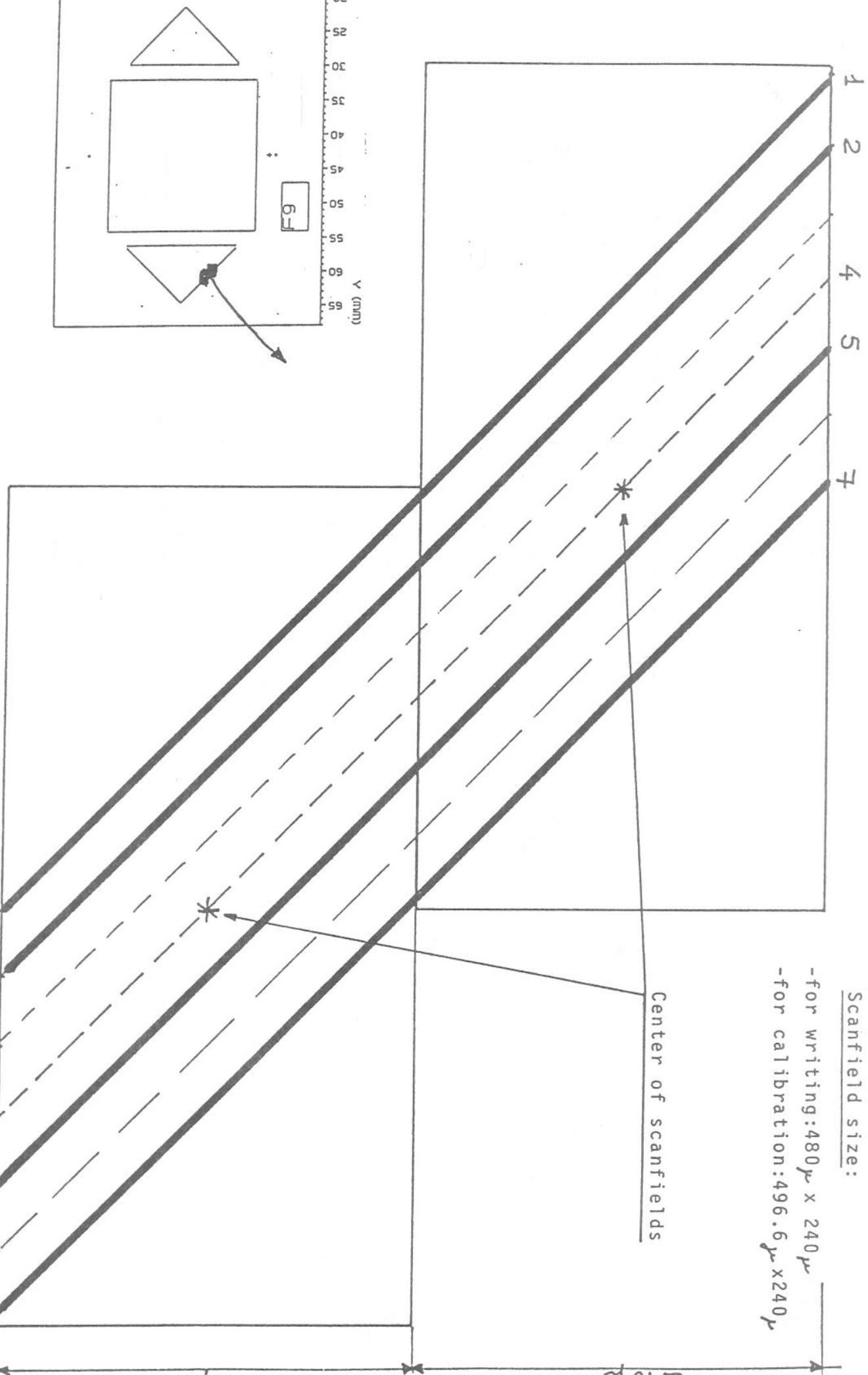
STAR MAPPER GRID

Date



Date .....

CALIBRATION OF STAR MAPPER CHEVRON (SMCHLU)



Date.....

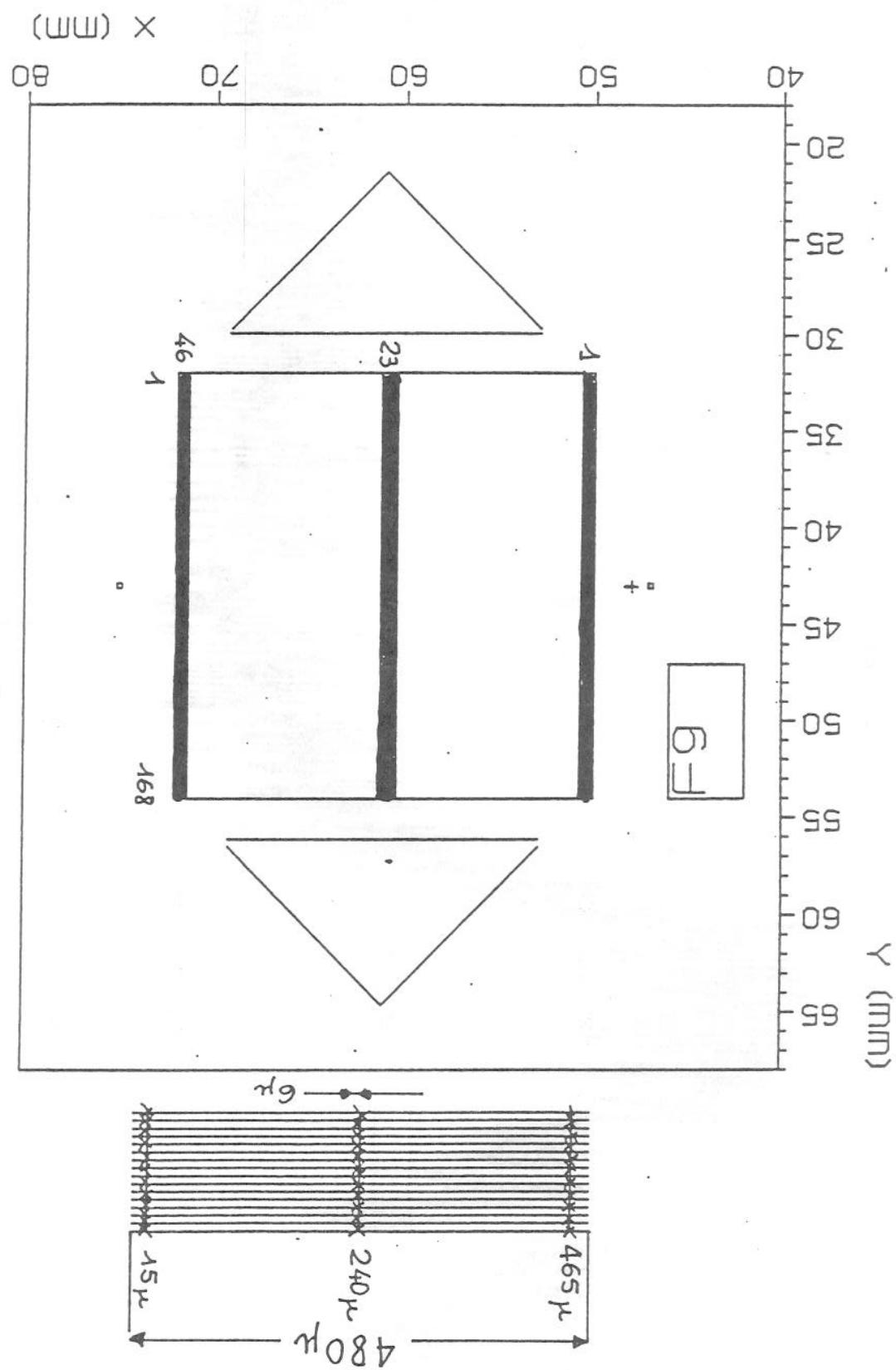
MAIN GRID			
SEQUENCE (DURATION)	SUBSEQUENCE (File #)	# OF SCANFIELDS MEASURED	# OF SLITS MEASURED PER SCANFIELD
MG4 (30 mn)	MG4.1 (184)	4 (same as in MG1.1)	2 X 4
	MG4.2 (185)		Repeat MG1.1 in order to assess the rotation of the substrate wrt EBG during the whole calibration period
	MG4.3 (186)		

SPECIAL RUNS REQUESTED BY ESA			
=====			
MG.ESA (4 hours)	3 X 168	3 X 16	Increase knowledge of grid parameters along 9 different scans dealing with all the slits



Date.....



SPECIAL RUNS " MG,ESA "



- FILE Z . TPDP10AO41

MEAN SLITWIDTH : 3087.

SLITWIDTH

3200.

3100.

3087.

3000.

2900.

2800.

500.0

1000.

1500.

2000.

2500.

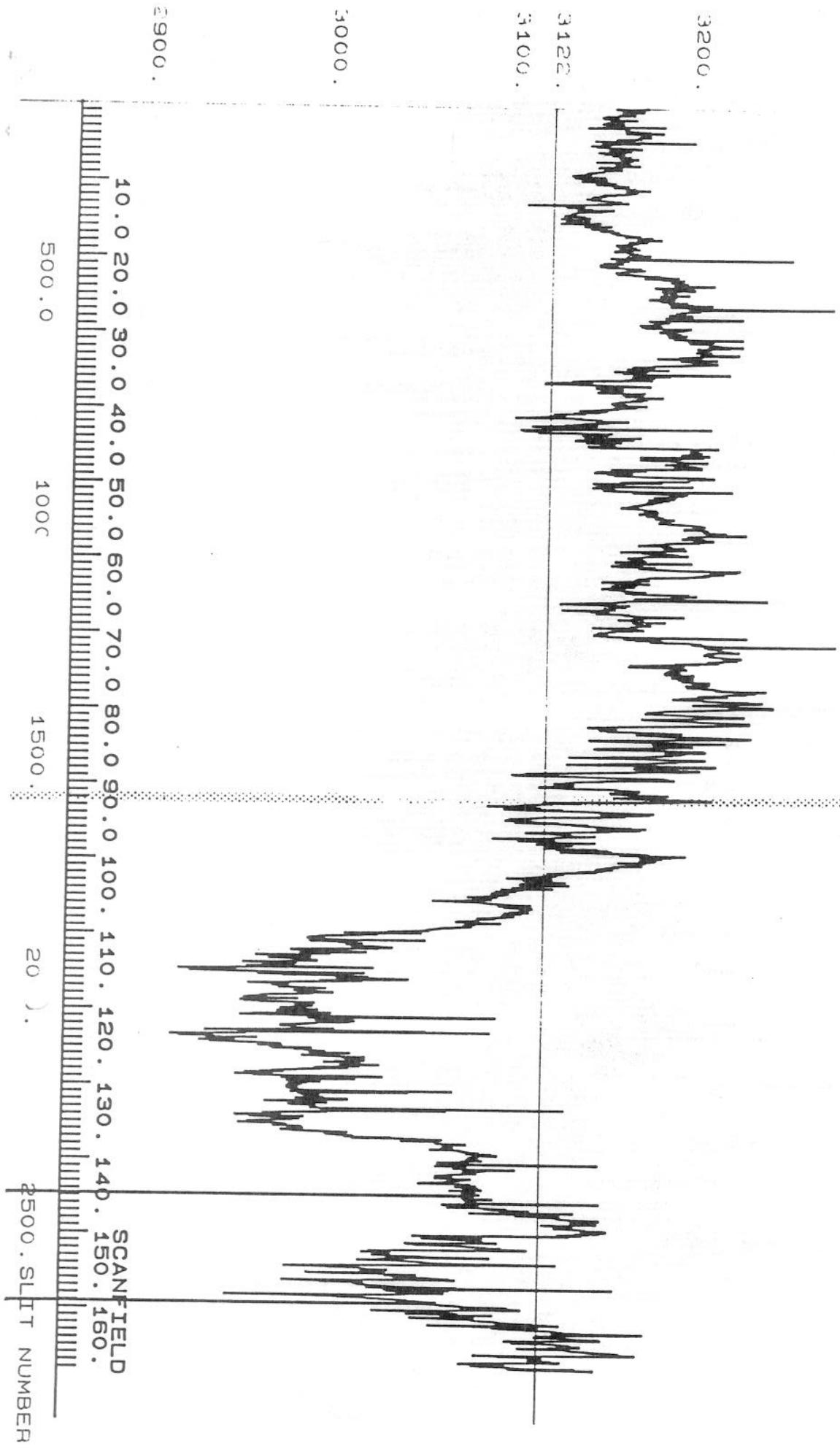
S - IT NUMBER

SCANFIELD

10.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0 100. 110. 120. 130. 140. 150. 160.

FILE Z.TPDP10AO42

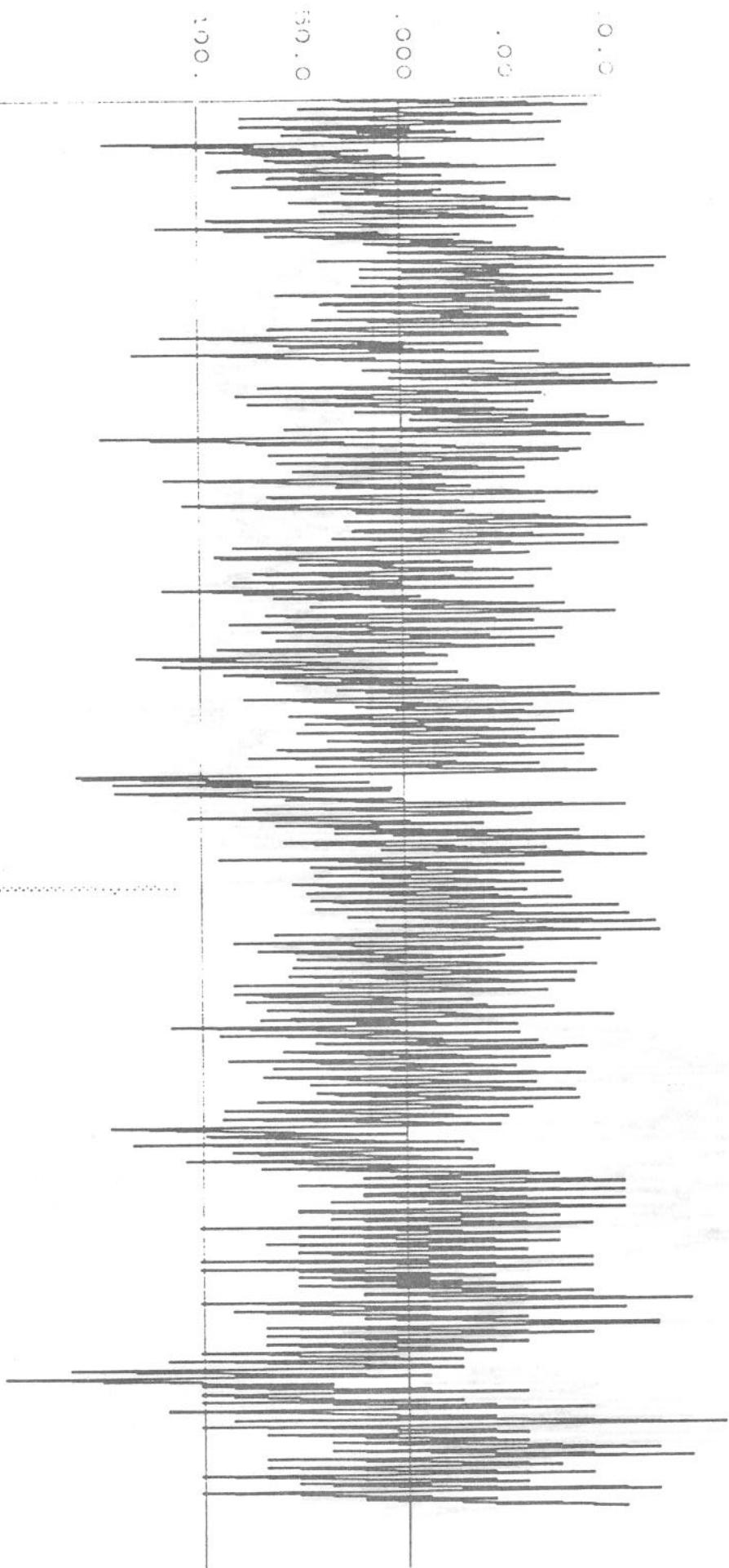
MEAN SLITWIDTH : 3122.  
SLITWIDTH



-FILE Z.TPDP10AO41

RESIDUAL ON SLIT POSITION 52.1 NM (RMS)

WITH L.S.I. CORRECTION

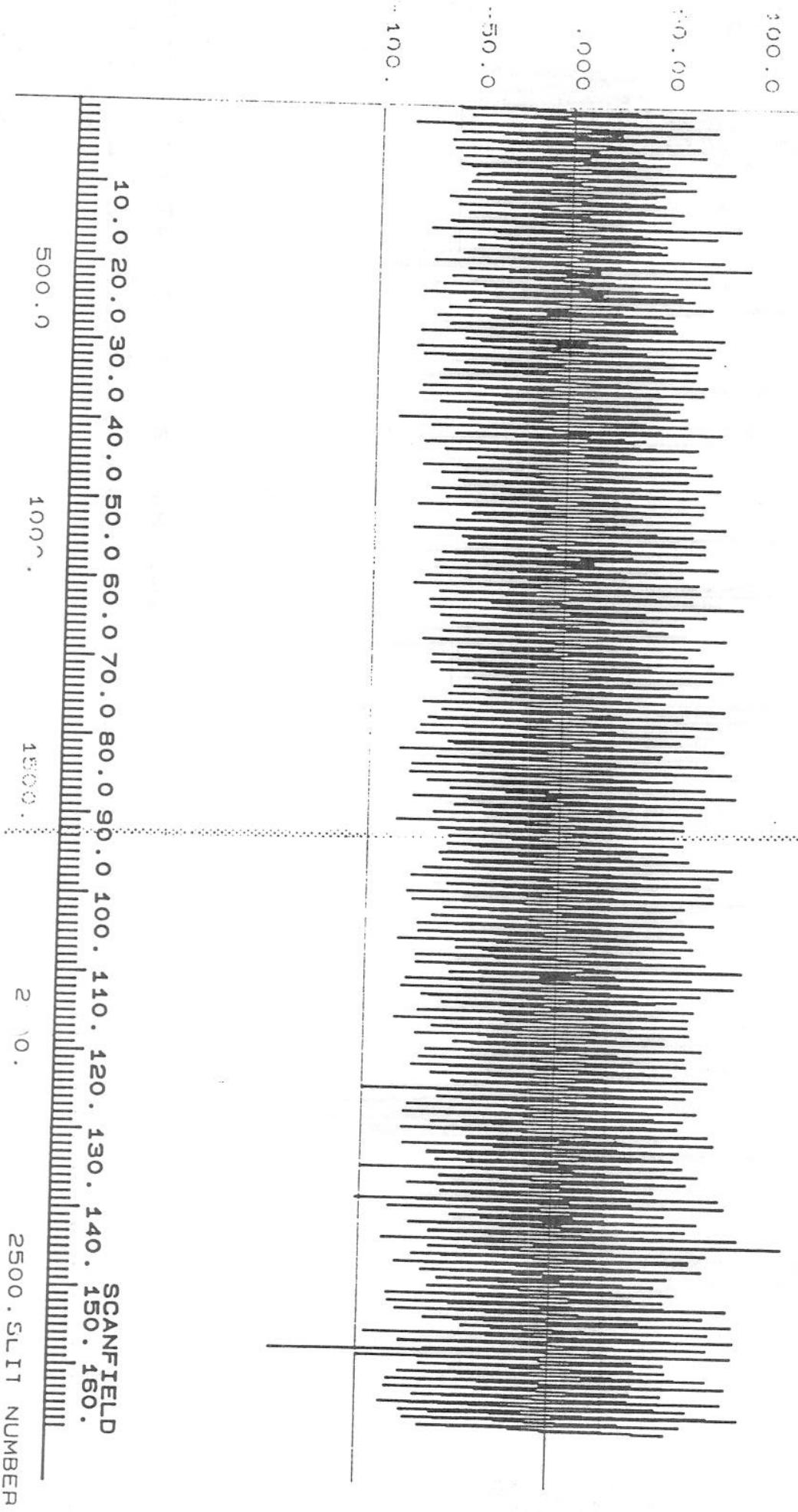


SCANFIELD

10.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0 100. 110. 120. 130. 140. 150. 160.

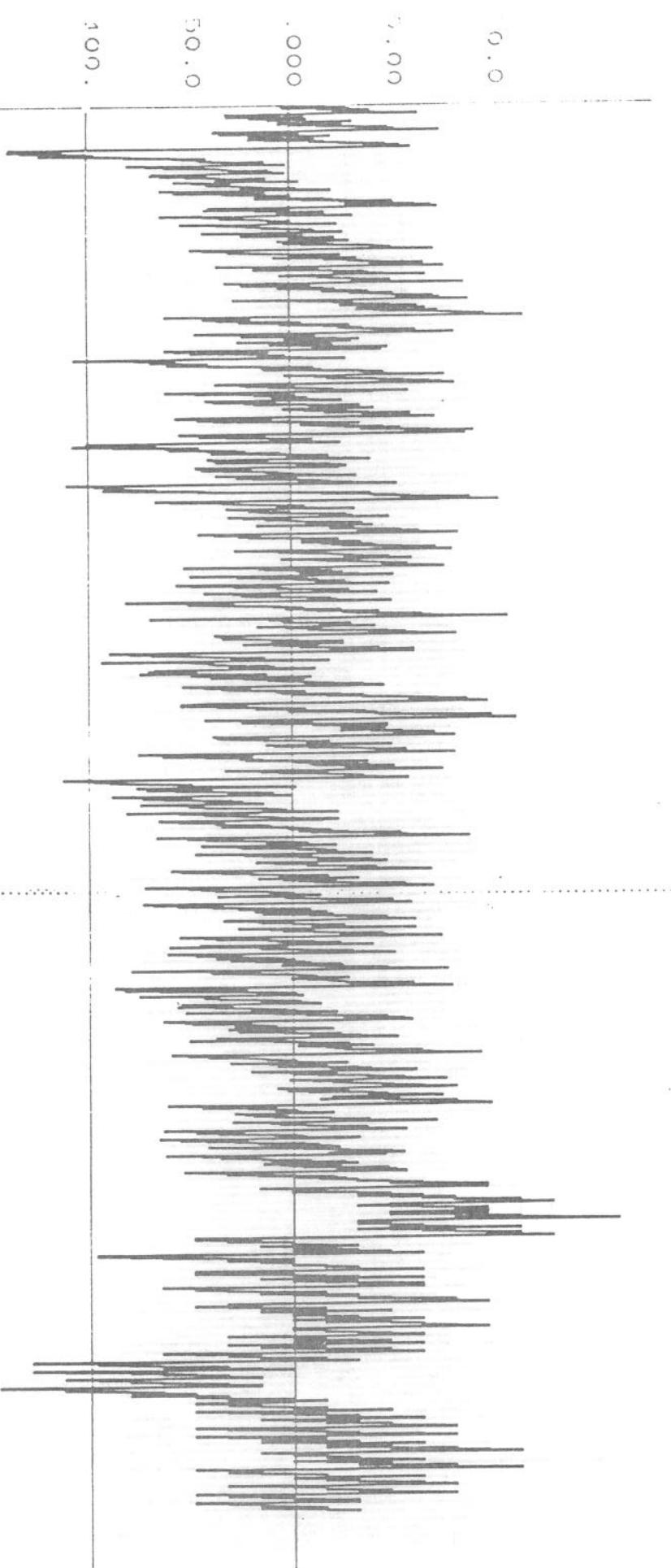
500.0 1000. 1500. 2000. 2500. SLIT NUMBER

FILE Z.TPDP10A041  
RESIDUAL ON SLIT POSITION 39.9 NM (RMS)  
WITH M.S.I. CORRECTION



10.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0 100. 110. 120. 130. 140. 150. 160.  
SLIT NUMBER

FILE Z.TPDP10A042  
RESIDUAL ON SLIT POSITION 42.0 NM (RMS)  
WITH L.S.I. CORRECTION



10.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0 100. 110. 120. 130. 140. 150. 160.  
SCANFIELD

500.0 1000. 1500.

2000.

2500. SLIT NUMBER

FILE Z.TPDP10A042

RESIDUAL ON SLIT POSITION 24.6 NM (RMS)  
WITH M.S.I. CORRECTION

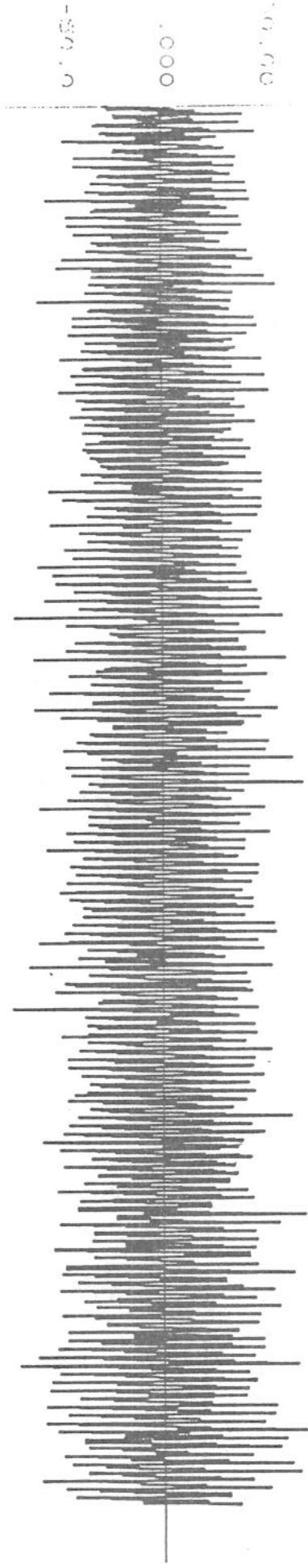
LOC. 0

LOC. 0

.000

-300. 0

-600. 0



10.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0 100. 110. 120. 130. 140. 150. 160.

200. 400. 600. 800. 1000. 1200. 1400. 1600. 1800. 2000. 2200. 2400. 2600. 2800. 3000.

LOC. 0.

LOC. 0.

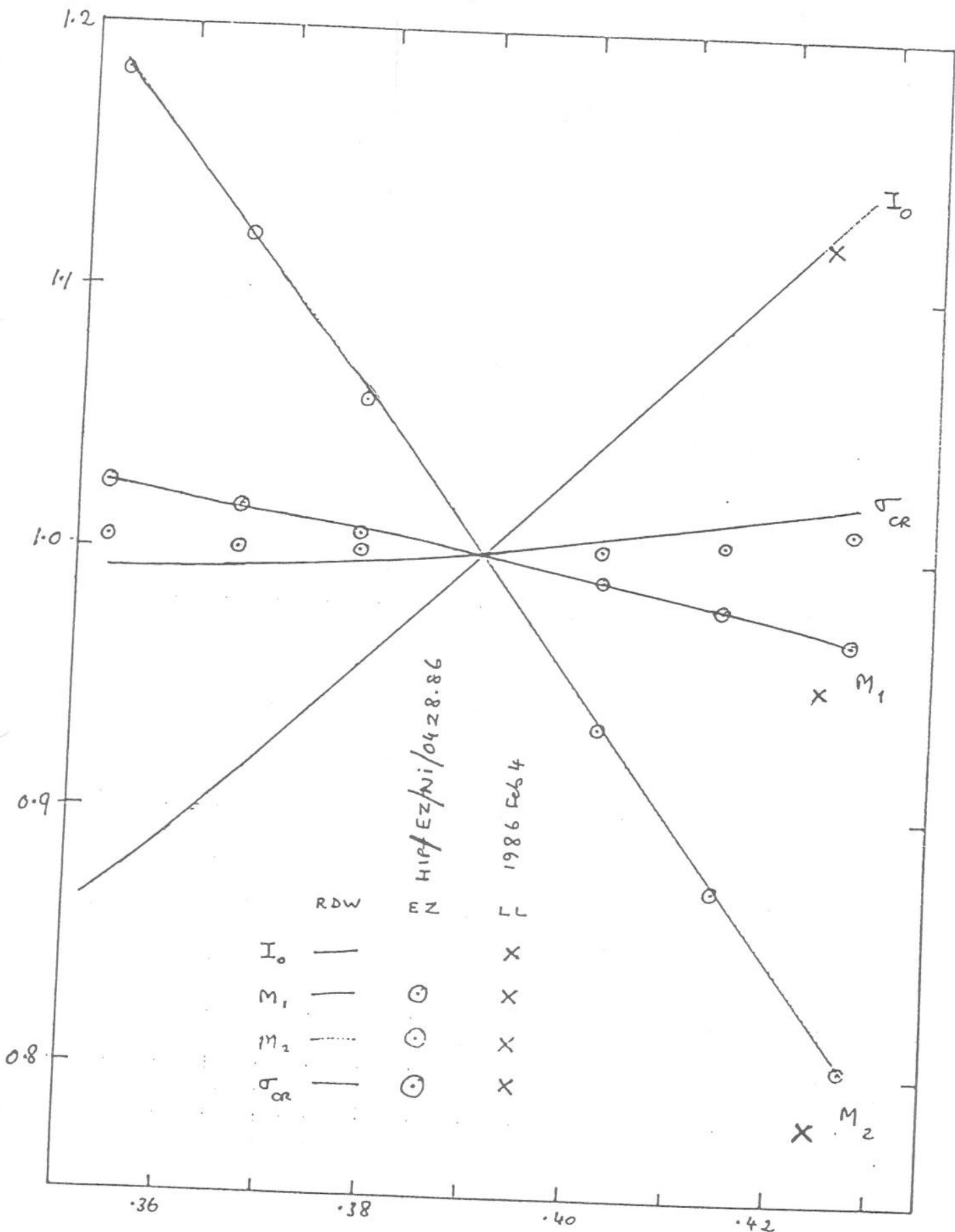
SCANFIELD  
2500. SLIT NUMBER



KDW → MS, SV, RB, GR, KVK, MACP

ANNEX VI  
HST

Performance variation with grid slit width  
 $B = 9$ ,  $B-V = 0.5$





MAIN MISSION ITF CALIBRATION

$$I_{obs} = I_{pf} (r_{00} + r_{10} \times 10^{-2} I_{obs} + r_{11} \times 10^{-4} \times I_{obs}^2 + \dots)$$

$$I_{true} = r_{00} I_{pf}$$

$$I_{obs} = I_{true} (1 + C_{ITF}/r_{00})$$

$$C_{ITF} = r_{10} \times 10^{-2} I_{obs} + r_{11} \times 10^{-4} I_{obs}^2$$

$$\sigma_{ITF}^2 = E[(\hat{C}_{ITF} - C_{ITF})^2]$$

| B<br>(mag) | V<br>(mag) | $I_{obs}$<br>( $s^{-1}$ ) | $C_{ITF}$              | $\sigma_{ITF}/r_{00}$<br>(%) |
|------------|------------|---------------------------|------------------------|------------------------------|
| 9.9        | 9.4        | $10^3$                    | $-1.79 \times 10^{-7}$ | -                            |
| 7.4        | 6.9        | $10^4$                    | $-1.79 \times 10^{-6}$ | -                            |
| 4.9        | 4.4        | $10^5$                    | $-1.77 \times 10^{-5}$ | 0.1                          |
| 4.2        | 3.7        | $2 \times 10^5$           | $-3.4 \times 10^{-5}$  | 0.3                          |
| 3.2        | 2.9        | $5 \times 10^5$           | $-8.3 \times 10^{-5}$  | 0.9                          |
| 3.0        | 2.5        | $6 \times 10^5$           | $-9.9 \times 10^{-5}$  | 1.2                          |
| 2.4        | 1.9        | $10^6$                    | $-1.54 \times 10^{-4}$ | 2.7                          |

$$(B-V = 0.5)$$

# STAR MAPPER ITF CALIBRATION

$$N_o^* = 4 \int I_o^* SSR(t) dt$$

$$C = r_{oo} (1 + C_{ITF})$$

| $N_o^*$<br>(cts) | $\sigma_{ITF}/C$<br>(%) |
|------------------|-------------------------|
| $10^3$           | 0.15                    |
| $2 \times 10^3$  | 0.30                    |
| $5 \times 10^3$  | 0.74                    |
| $6 \times 10^3$  | 0.88                    |
| $8 \times 10^3$  | 1.17                    |
| $10^4$           | 1.47                    |
| $2 \times 10^4$  | 2.9                     |
| $4 \times 10^4$  | 5.8                     |
| $8 \times 10^4$  | 11.5                    |

For  $B=5$  and  $B-V=0$   $N_o^*(B_T) \approx 4000$  cts

For  $B=5$  and  $B-V=1.5$   $N_o^*(V_T) \approx 5000$  cts

## TRANSFORMATION/DISTORTION

- REFERENCE FRAMES
- BREAKDOWN OF TRANSFORMATION COMPONENTS
- MIRROR SURFACE APPROXIMATION
- ASTIGMATISM DUE TO BASIC ANGLE
- EFFECT OF GRID MOVEMENT ON DISTORTION
- STARMAPPER DISTORTION

## REFERENCE FRAMES

FIELD COORDINATES  $(\theta, \gamma)$  IN ARCSEC  
GRID COORDINATES  $(G, H)$  IN ARCSEC OR NONDIMENSIONAL

OPTICAL REFERENCE FRAME USED FOR GRID ALIGNMENT:  
"SCAN PLANE" - PARALLEL TO BEAM COMBINER NORMALS  
- THROUGH SPH. MIRROR CENTER OF CURVATURE  
"VERT. PLANE" - PARALLEL TO BEAM COMB. BISSECTORIX OF NORMALS  
- THROUGH SPH. MIRROR CENTER OF CURVATURE  
 $\Rightarrow$  CENTER OF GRID WHERE  $\gamma = \text{MAX}$

REMARK:  $(G, H)$  DEPEND ON FOCAL LENGTH VIA  
DIMENSIONS (mm) ON GRID AND NORMALISATION  
OF FOV SIZE

## BREAKDOWN OF TRANSFORMATION COMPONENTS

MAIN FIELD SCAN DIRECTION  $G = G_N + G_L + G_M + G_S$   
 $G =$  STAR POSITION AS SENSED BY PRIMARY DETECTOR,  
AT  $B-V=0,50 \Rightarrow$  TRANSFORM. (FOV, GRIDFREQU., DETECTOR)

$G_N$  = NOMINAL DISTORTION TRANSFORMATION, LIMITED TO  $3^\circ$   
 $\int F \cdot \gamma + D_N$  DEGREE POLYNOMIAL IN  $(\gamma, \delta)$  OF BOTH MAIN AND SM FIELDS  
 $D_N = \epsilon^e + 3^\circ$  DEGREE TERMS ONLY OF  $G_N$   
 $(G_N, D_N)$  DO NOT DEPEND ON OPTICS, ONLY VIA F  
 $G_L$  = LARGE SCALE COMPONENT, LIMITED TO  $2^\circ$  DEGREE  
POLYNOMIAL IN  $(\gamma, \delta)$  OF LEAST SQUARE FIT ON MAIN FIELD  
 $G_M$  = MEDIUM SCALE COMPONENT, LIMITED TO  $168 \times 46$   
DISCRETE SCAN FIELDS  
 $G_S$  = SMALL SCALE COMPONENT, RESIDUAL OF TRANSFORMATION  
(TO BE EXPRESSED IN RANDOM, SAWTOOTH DISTORTION, ETC)

## BREAKDOWN OF TRANSFORMATION COMPONENTS

S<sub>M</sub>-FIELD SCAN DIRECTION  $g^* = g_N^* + g_L^* + g_M^* + g_F^* + g_R^*$   
 $g^*$  = STAR POSITION AS SENSED BY SM DETECTOR, BASED  
ON MAX. CORRELATION OF SRR AND FILTER, AT B-V=0, SO  
AFTER AVERAGING OVER BT AND VT CHANNEL

$g_N^*$  = SAME AS FOR MAINFIELD  
 $g_L^*$  = EXTRAPOLATED FROM MAINFIELD LEAST SQUARE FIT  
 $g_M^*$  = MEDIUM SCALE COMPONENT, LIMITED TO  
DISCRETE SCANFIELDS  
 $g_F^*$  = FOV DEPENDENT "PHASE SHIFT" DUE TO ASTIGMATISM  
OF OPTICS AND HALF PUPIL OFFSET, ON CHEVRONS ONLY  
 $g_R^*$  = RESIDUAL OF TRANSFORMATION

## MIRROR SURFACE APPROXIMATION

SPHERICAL MIRROR  $X = R - \sqrt{R^2 - \rho^2} \approx \rho^2/2R + \rho^4/8R^3$   
 FOR  $\rho \leq 145$  mm AND  $R = 2800$  mm

BEAM COMBINER  $X = \frac{1}{2}\rho^2 CK + \rho^4 AD$  PER MIRROR HALF  
 AFTER ROTATION (BASIC ANGLE  $/4$ )  $\pm 14.5$  degr  
 AND VERT. SHIFT (COMPENSATION)  $\pm 4.0$  mm THEN  

$$X = \frac{1}{2}\rho^2 CK \left[ \left\{ \cos \varphi / \cos(\gamma/4) \right\}^2 + \left( \sin \varphi + t/\rho \right)^2 \right] +$$

$$+ \rho^4 AD \left[ \left\{ \cos \varphi / \cos(\gamma/4) \right\}^2 + \left( \sin \varphi + t/\rho \right)^2 \right]^2$$
 FOCAL LENGTH  $f_\varphi \approx f / \{ \cos^2 \varphi / \cos^2(\gamma/4) + \sin^2 \varphi \}$

$$\left. \begin{aligned} f_0 &= 1347778 \text{ mm} \\ f_{90} &= 1437922 \text{ mm} \end{aligned} \right\} \begin{array}{l} \text{IN SCAN DIRECTION} \\ \text{IN VERT. DIRECTION} \end{array}$$

$$\left. \begin{aligned} f &= 1437922 \text{ mm} \\ \gamma &= 58 \text{ degr} \end{aligned} \right\}$$

## ASTIGMATISM DUE TO BASIC ANGLE

### BEAM COMBINER + SPHERICAL MIRROR COMBINED FOCAL LENGTH

$$f^* = \frac{f_{BC} - f_{SM}}{f_{BC} + f_{SM} - d} \quad d = (BC - SM) \text{ distance.}$$

$f_{BC} < 0, f_{SM} > 0, d < 0$   
 $f_0^* = 1/(1/1400 + 1/f_0) \Rightarrow 1398,5473 \text{ (mm)}$  IN SCAN DIRECTION  
 $f_{90}^* = 1/(1/1400 + 1/f_{90}) \Rightarrow 1398,6382 \text{ (mm)}$  IN VERT. DIRECTION  
 DIFFERENTIAL FOCUS 0,0909 (mm) ASTIGMATISM 0,0914

Back

BEST FOCAL LENGTH FROM LAS ANALYSES  $f_0^* = 1398,6090 \text{ (mm)}$

### CONTRIBUTION OF BEAM COMBINER:

$$f_0 = 1/(1/f_0^* - 1/1400) \Rightarrow 1407658 \text{ (mm)}$$

### APPARENT FOCAL LENGTH IN VERT. DIRECTION:

$$f_{90} = f_0 / \cos^2(\gamma/4) \Rightarrow 1501807 \text{ (mm)}$$

$$f_{90}^* = 1/(1/1400 + 1/f_{90}) \Rightarrow 1398,6961 \text{ (mm)}$$

DIFFERENTIAL FOCUS 0,0871 (mm) ASTIGMATISM

BOTH METHODS  $\Rightarrow$  ASTIGMATISM  $\approx 90 \mu\text{m}$

## EFFECT OF GRID MOVEMENT ON DISTORTION

### DISPLACEMENT COMPONENTS OF GRID SURFACE

$$u = u_0 - \gamma y + \beta z \quad \text{IN OPTICAL DIRECTION (x)}$$

$$v = v_0 - \alpha z + \gamma x \quad \text{IN SCAN DIRECTION (y)}$$

$$w = w_0 - \beta x + \alpha y \quad \text{IN VERT. DIRECTION (z)}$$

### APPARENT IMAGE DISPLACEMENT COMPONENTS

$$\delta = \left\{ \begin{array}{l} u_0(\langle y \rangle - y) / f + v_0 - \alpha z + \beta (\langle y \rangle - y) z / f - \beta (\langle y \rangle - y) y / f \end{array} \right\} / f$$

$$\epsilon = \left\{ \begin{array}{l} u_0(\langle z \rangle - z) / f + w_0 + \alpha y + \beta (\langle z \rangle - z) z / f - \beta (\langle z \rangle - z) y / f \end{array} \right\} / f$$

$\langle y \rangle, \langle z \rangle$  PUPIL CENTROID COORDINATES

$f$  = FOCAL LENGTH

$$\rightarrow \left\{ \begin{array}{l} g = 147,34 \Delta x - 1,1576 \times \Delta z - 7,8571 y \Delta \theta z + 9,061735 \underbrace{(x^2 \Delta \theta y - xy \Delta \theta x)}_{\text{SHIFT}} \\ h = 147,34 \Delta y - 1,1576 y^* \Delta z + 7,8571 x \Delta \theta z + 9,061735 \underbrace{(xy^* \Delta \theta y - yy^* \Delta \theta x)}_{\text{SCALE + ROTATION + QUADRATIC}} \end{array} \right.$$

WITH  $y^* = y \pm 63,9/11$  DEPENDENT ON FOV  
 $(dg, dh)_{\text{mas}}, (\Delta x, \Delta y, \Delta z)_{\mu\text{m}}, (\Delta \theta x, \Delta \theta y, \Delta \theta z)_{\text{as}}, (x, y, z)_{\text{mm}}$

## STAR MAPPER DISTORTION

$G_F^*$  = FOV DEPENDENT "PHASE SHIFT", ON CHEVRONS ONLY

WITH PUPIL CENTROID AT 63.9 (mm)  
ASTIGMATISM OF 90 (um)  
FOCAL LENGTH OF 1400 (mm)  
NOMINAL, KNOWN AND CONSTANT SHIFT IS  $G_F^* = \pm 605.2$  (mas)

IN ADDITION CROSS EFFECTS DUE TO OPTICS DISTORTION  
AND GRID ROTATION NEED TO BE ADDED.

SM DISTORTION SPECIFICATION UNDER REVIEW

*W.W.*

cc. R&W  
MS  
ESOC JvdH  
J.S.

**DRAFT**

## WHAT WILL BE AVAILABLE IN THE "INPUT CATALOGUE" ?

C. Turon

10/03/86

\*\*\*\*\*

Make a clear distinction between :

- I. - The "INCA" Data Base which includes all available data and cross-identifications on all proposed stars (210 000 stars).
- II. - A subset of this base (100 - 120 000 stars) that will be observable by Hipparcos.  
For these stars, any desirable subset of data may be taken from the INCA Data Base.

### I - Data in the "INCA" Data Base (210 000 stars).

1. all known cross-identifications (from which any subset may be extracted in answer to specific requests) ;
2. so-called "fundamental" data : position, proper motion if available, B (or H) and/or V magnitude, a code for variability, the spectral type.  
The positions and magnitudes given here are those used within INCA simulations.
3. "measurements". These include the measurements available within SIMBAD, and specific INCA "measurements" described in detail underneath (taken from INCA report N° 11 to ESA, January 1986, pp.37-38).
  - a) : pH (Hipparcos photometry).
    - . H magnitude
    - .  $\sigma$  H
    - . code for source (from 0 to 99)
    - . S if standard stars for Hipparcos
    - . V magnitude
    - .  $\sigma$  V
    - . code for source (from 0 to 99)
    - . (B-V)
    - .  $\sigma$  (B-V)

- . code for source (from 0 to 99)
  - . code for reference
- b) vH (Hipparcos variable stars).
  - . magnitude at maximum luminosity
  - . type of magnitudes
  - . magnitude at minimum luminosity
  - . magnitude adopted for simulation
  - . percentage of the period when the star is brighter than the Hipparcos limiting magnitude
  - . code for reference
- c) sH (Hipparcos simulation).
  - . number of the version
  - . pressure
  - . observability parameter
  - . code for reference
- d) CCDM (specific data for multiple stars).
  - . letter for the component
  - .  $\Delta \alpha$  with respect to the  $\alpha$  given in the CCDM
  - .  $\Delta \delta$  with respect to the  $\delta$  given in the CCDM
  - . code for reference
  - . magnitude
  - . position angle  $\vartheta$  in degrees
  - . separation  $\rho$  in arcseconds
  - . 0 if there is an orbit in an annex catalogue
  - . letter of the associated component if  $\rho < 10''$
  - . coded spectral type
  - . code for reference
- e) pos (position of the star).
  - . right ascension
  - .  $\sigma_\alpha$
  - . declination
  - .  $\sigma_\delta$
  - . Equinox
  - . Mean epoch of the observations
  - . code for reference
- f) pm (proper motion).
  - .  $\mu_\alpha \cos \delta$
  - .  $\sigma_{\mu_\alpha \cos \delta}$
  - .  $\mu_\delta$
  - .  $\sigma_{\mu_\delta}$
  - . code for reference

**II - Data in the Input Catalogue** (100 - 120 000 selected stars).  
 One "main catalogue". Four annex catalogues".

**MAIN CATALOGUE.**

**1. Running number.**

All selected stars will be numbered once sorted out by increasing right ascension. In this context, "star" is used for "separate entry" to be taken into account for the preparation of the PSF (either single star or components with a separation larger than 10").

In addition :

- 1) a 2-digit code will indicate :
  - the number of entries for the considered system,
  - the number of components considered in this entry, in case of joint system ( $\varrho < 10''$ ) ;
- 2) in case of double or multiple stars, the CCDM number (Catalogue of Double or Multiple Stars), allowing us to enter the annex catalogue N°1, dedicated to detailed information on these stars.

Examples :

| type of star   | running number | code     | CCDM number                | considered components |
|--|----------------|----------|----------------------------|-----------------------|
| simple star  | 581            | 11       |                            |                       |
| double star<br>$\varrho < 10''$                                    | 582            | 12       | 00012+23,15                | AB                    |
| double star<br>$\varrho \geq 10''$                                 | 583<br>586     | 21<br>21 | 00123-10,20<br>00123-10,20 | A<br>B                |
| triple star<br>$\varrho_{AB} < 10''$<br>$\varrho_{AB,C} < 10''$    | 590            | 13       | 12567+01,A2                | ABC                   |
| triple star<br>$\varrho_{AB} < 10''$<br>$\varrho_{AB,C} \geq 10''$ | 591<br>595     | 22<br>21 | 01465-51403<br>01465-51,03 | AB<br>C               |

**2. Data necessary for ESOC.**

- position + rms Equinox 2000, Epoch 1990
- H magnitude + rms + flag for standard stars
- flag for variable star = code for variation amplitude.  
 Indicates an entry in Annex Catalogue N°3, dedicated to detailed information on variable stars
- parameter resulting from mission simulation.

3. Additional data useful to DRC, given if available.

- V magnitude + rms
- B-V + rms
- HD spectral type
- trigonometric parallax + rms
- annual proper motion + rms
- radial velocity + rms
- flag for type of binarity
- flag for veiling glare due to programme stars
- flag for veiling glare due to bright non-programme stars

4. Additional information (if available).

- best ESA priority
- ~~tridimensional MK spectral type~~
- code indicating that the star is included in some catalogues  
(uvby photometry, Geneva photometry, ...)

5. Identifications.

- HD number
- DM number
- } other identifications

For ESA :

- identification of proposals asking for this star,  
running numbers in each proposal, ESA priority in this  
proposal.

6. Sources and references.

- for positions
- for proper motions
- for B magnitude
- for V magnitude
- for trigonometric parallax
- for radial velocity
- for MK spectral type

## 7. Double stars.

Adopted rule : . 1 entry if  $\rho < 10''$

. 2 entries if  $\rho \geq 10''$

AB

A, B

### a) for close double stars ( $\rho < 10''$ )

In the main catalogue, the position and magnitude of the photo-center are given. Positions and magnitudes of both components (if available) are given in Annex Catalogue N°1.

### b) for wide double stars ( $\rho \geq 10''$ )

. If the two components are requested separately by proposers, the information on both components will be found in the main catalogue, under two separate entries.

. If only one of the two components is requested by proposers : either

this component only appears in the main catalogue ;  
information on the second one may be found in Annex Catalogue N°1 ;

or

both components appear in the main catalogue with two separate entries.

. In both cases, within which limits in  $\rho$  and  $\Delta m$  the second component should be included in the main catalogue ? (if its position and magnitude are known).

## 8. Multiple systems.

Adopted rule :

. 1 entry for any subset of components such that  $\rho < 10''$  ;

. additional entry for any component at a distance  $\rho \geq 10''$  from each of the other components.

## 9. Variable stars.

The adopted rule for the H magnitude depends on the type of variability.

It may be :

- the magnitude at minimum luminosity (for eruptive variables),
- the magnitude at maximum luminosity (for eclipsing variables),
- a mean (or weighted mean) magnitude, depending on the type of light curve.

Detailed information on variability is given in Annex Catalogue N°3.

Ephemerides for large amplitude variable stars are given in Annex Catalogue N°4.

ANNEX CATALOGUE N°1 : Detailed information on double and multiple stars.

- Input Catalogue running number
- CCDM number
- considered component
- delta " } with respect to " as given in the CCDM number
- delta  $\delta$  } with respect to  $\delta$
- source of position
- magnitude
- position angle :  $\theta$  } with respect to the A component
- separation :  $\rho$  } reference
- reference
- O if orbital double star, orbital elements given in Annex Catalogue N°2
- if the above data are joint information on a close binary, identification letter of the second component
- spectral type

ANNEX CATALOGUE N°2 : Orbital elements for orbital double stars.

- Input Catalogue running number
- CCDM number
- orbital elements

ANNEX CATALOGUE N°3 : Detailed information on variable stars.

- Input Catalogue running number
- name of the variable star
- type of variability
- magnitude at maximum luminosity
- type of magnitude
- magnitude at minimum luminosity
- period of variation (in days)
- epoch (in Julian days)
  - . of last minimum for eclipsing variables and T Tauri type stars,
  - . of last maximum for all other types of variable stars
- percentage of the period when the variable star is observable by Hipparcos
- reference

ANNEX CATALOGUE N°4 : Ephemerides for large amplitude variable stars.

- Input Catalogue running number
- name of the variable star
- epoch
- magnitude

DRAFT

WHAT WILL BE AVAILABLE IN THE "INPUT CATALOGUE" ?  
for Minor Planets

C. Turon

10/03/86

\*\*\*\*\*

Here again, there may be a distinction between the Data Base on Hipparcos minor planets and the data necessary for satellite operation or data reduction.

I - CONTENT OF THE MINOR PLANETS DATA BASE.

Chebychev coefficients for the various parameters describing each minor planet are given at successive epochs, every 30 days. The coefficients are valid over overlapping intervals of 34 days. 8 coefficients are presently given. This number may be modified according to the results of further tests.

For each epoch, are given :

- a running number for the Hipparcos minor planets
- the number of the minor planet
- Chebychev coefficients for the right ascension (J2000)
- Chebychev coefficients for the declination
- Chebychev coefficients for the ecliptic longitude
- Chebychev coefficients for the ecliptic latitude
- Chebychev coefficients for the distance
- Chebychev coefficients for the phase angle
- Chebychev coefficients for the magnitude

Any subset of this Data Base may be selected for ESA or DRC.

Remark for ESOC :

The data on minor planets should be updated during the year prior to the launch but also during the mission itself, every 6 (TBC) months.

(geocentric, J2000, (i.e. only need to correct for satellite orbit))



## PROGRAM STAR FILE PREPARATION

- 1 Observing Strategy Distortions and possible actions  
at PSF level.
- 2 Modulation of Observing strategy parameters :
  - parameters
  - control of data acquisition
  - modulation scheme.
- 3 Cost/Quality considerations :
  - simulation results with and without modulation
  - additionnal ressource requirements
    - updates of the covariance matrix
    - observing calendar
    - frequency of updates
  - special processing
    - "proper motion stars" in dense fields
    - alternate observations in very dense fields
- 4 Observability
- 5 Dates

# observing strategy effects

Pressure dominates

1° if PR is such that

$$\sum x_0 \geq 20$$

$\gamma_0$  does not work

2° when 1 high Pressure + 1 medium pressure

| Even Frame      |          | add frame |    |
|-----------------|----------|-----------|----|
| HP field        | MP field | HP        | MP |
| 1               | 1        | 7         | 3  |
| 2               | 2        | 6         | 2  |
| 3               | 3        | 5         | 1  |
| 4               |          | 4         |    |
| $\sum x_0 = 20$ |          |           |    |
| 5               |          | 3         |    |
| 6               |          | 2         |    |
| 7               |          | 1         |    |

A.P. favours stars in MP fields

3° stars with  $Lx_0 \ll \gamma_0$  are unfavoured -  
in dense fields

# Control of Data Acquisition (1)

## Basic Tool:

The Covariance Matrix of Astrometric Units

$$B = A^{-1}$$

$$A = [a_{jk}] , \quad a_{jk} = \sum_i d_{ij} d_{ik} P_i \quad (1)$$

$$P_i = P(m) \tau_i$$

$\tau_i$  = observing time dedicated to the star  
under consideration during field  
crossing  $i$

## 2 Standard observing history (Target)

- field crossings are predicted on the basis of a strict Nominal Scanning Law  
(= Nominal Observing Calendar = NOC )

-  $\bar{\tau}_i = \bar{\tau}$  = target observing time per field Crossing

$$\rightarrow \bar{A} \rightarrow \bar{B} = \bar{A}^{-1}$$

INCA can provide either

$\bar{\tau}$  and  $\bar{B}$  once the starting point of observations is known

produce the code

# Control of Data Acquisition (2)

## State of observations at time $t$

It is derived from  $\bar{B}$  by substituting progressively actual observations to standard ones in (1)

$$\tilde{B}(t_i) = \tilde{A}^{(t_i)} \quad \tilde{A}^{(t_i)} = [\tilde{a}_{jk}^{(t_i)}]$$

$$\tilde{a}_{jk}^{(t_i)} = \tilde{a}_{jk}^{(t_{i-1})} + \alpha_{ij} \alpha_{ih} P(m)(T_i - \bar{T})$$

$$\text{at } t=0 \quad \tilde{B}(0) = \bar{B}$$

A few terms in  $\tilde{B}$  will be compared to identical term in  $\bar{B}$  indicating Under or Over observation

$$b_{33}, b_{55}, ?, \dots \quad \vec{s}(+) = \left( \frac{\bar{b}_{33}}{\tilde{b}_{33}(+)}, \frac{\bar{b}_{55}}{\tilde{b}_{55}(+)}, \dots \right)$$

## Expected yield

The efficiency of the next observation to come is measured by comparing  $\bar{B}$  (or  $\tilde{B}$ ) to a matrix  $B^*$

from which this observation has been excluded

$$B^*(t_i) = A^*(\bar{T}) \quad A^*(+) = [a_{jh}^*(+)]$$

$$a_{ih}^* = a_{ih} - \alpha_{ij} \alpha_{id} P(m) \bar{T}$$

See example

Expected yield  
(Efficiency)

$$\vec{s}(+) = \left( \frac{b_{33}^*(+)}{b_{33}}, \dots \right)$$

once per day, for each star expected  
to be observed during day  $D+1$

compute

## 1 THE STATE OF OBSERVATIONS :

$$r_1(\pi), r_2(\mu_\alpha), r_3(\mu_\beta)$$

IF  $r_1 < (1 - \varepsilon_1)$  OR  $r_2 < (1 - \varepsilon_2)$  OR  $r_3 < (1 - \varepsilon_3)$  THEN UNDEROBSERVED  
 $\varepsilon = 0.02$

IF  $r_1 > (1 + \varepsilon'_1)$  AND  $r_2 > (1 + \varepsilon'_2)$  AND  $r_3 > (1 + \varepsilon'_3)$  THEN OVEROBSERVED  
 $\varepsilon' = 0.002$

ELSE NORMAL

## 2 THE EXPECTED EFFICIENCY :

$$\delta_1(\pi), \delta_2(\mu_\alpha), \delta_3(\mu_\beta)$$

IF  $\delta_1 > (1 + \varepsilon''_1)$  OR  $\delta_2 > (1 + \varepsilon''_2)$  OR  $\delta_3 > (1 + \varepsilon''_3)$  THEN EFFICIENT  
 $\varepsilon'' = 0.002$   
ELSE NOT EFFICIENT

Assuming that parallaxes are not requested  
for some stars (RHO\*)

$\varepsilon'_1$  and  $\varepsilon''_1$  are set to arbitrarily large  
values so that  $r_1 > 1 + \varepsilon'_1$  and  $\delta_1 < 1 + \varepsilon''_1$   
Systematically

# OBSERVING DECISIONS

Default Values

$$\text{minimum time (number of slots)} \quad x_1 = \max(x_0, \text{INT}(y_0/2))$$

target time

$$y_1 = y_0/G_0$$

$$(y_0 = T_{\text{cib}}/N(p)(1-\alpha_c))$$

observing flag

$$OF = 1$$

EFFICIENT?

YES

NO

FA?

1

OF = 1

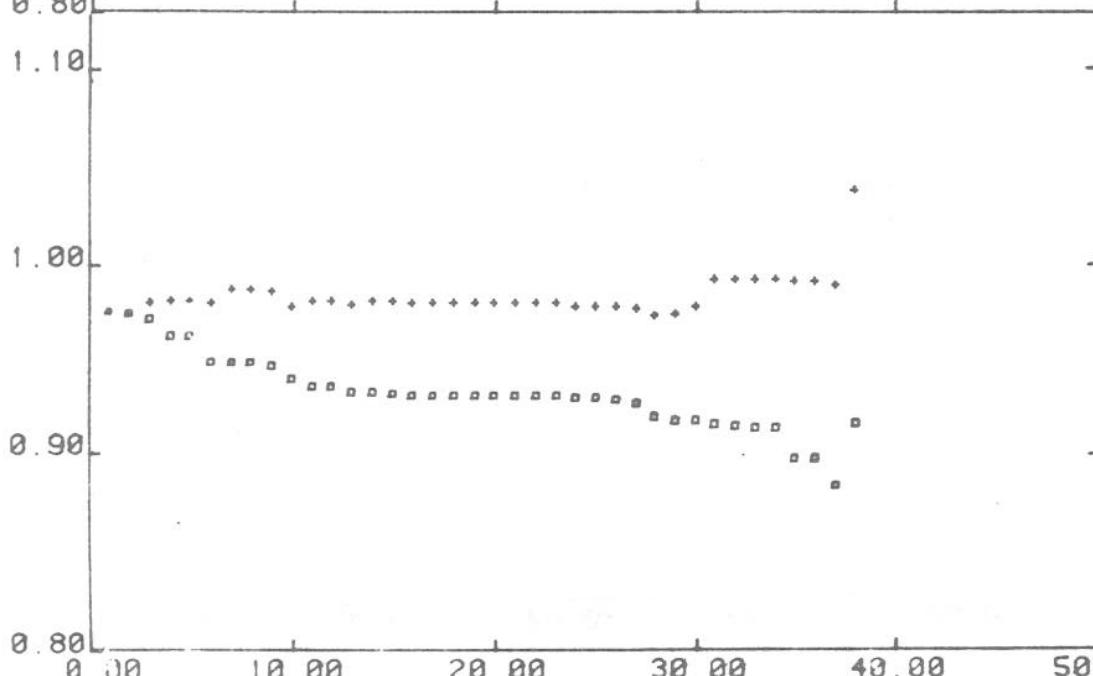
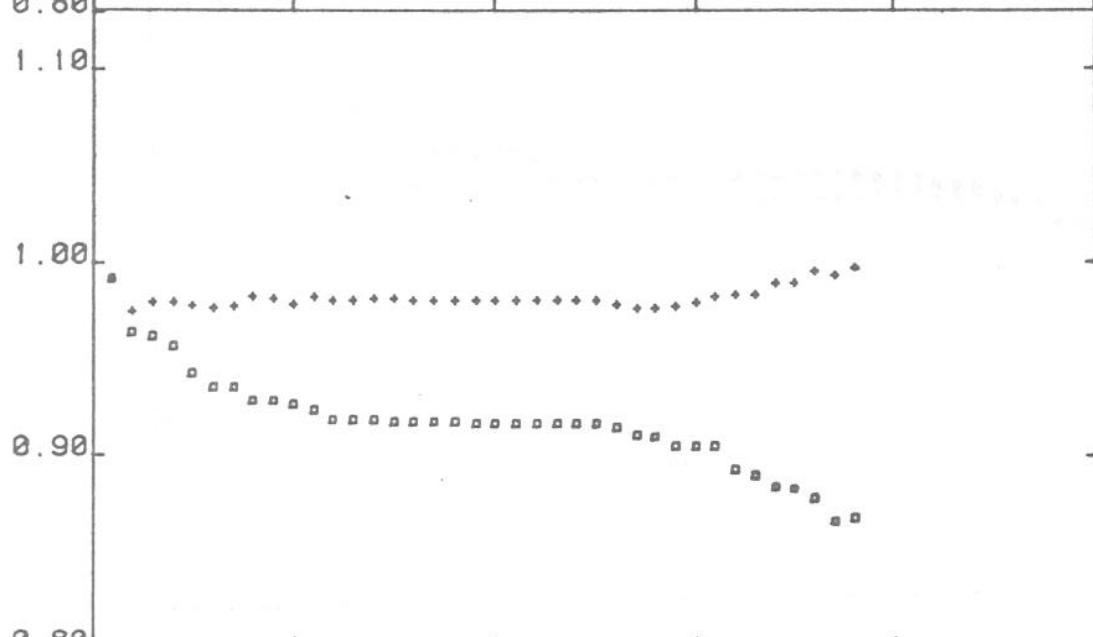
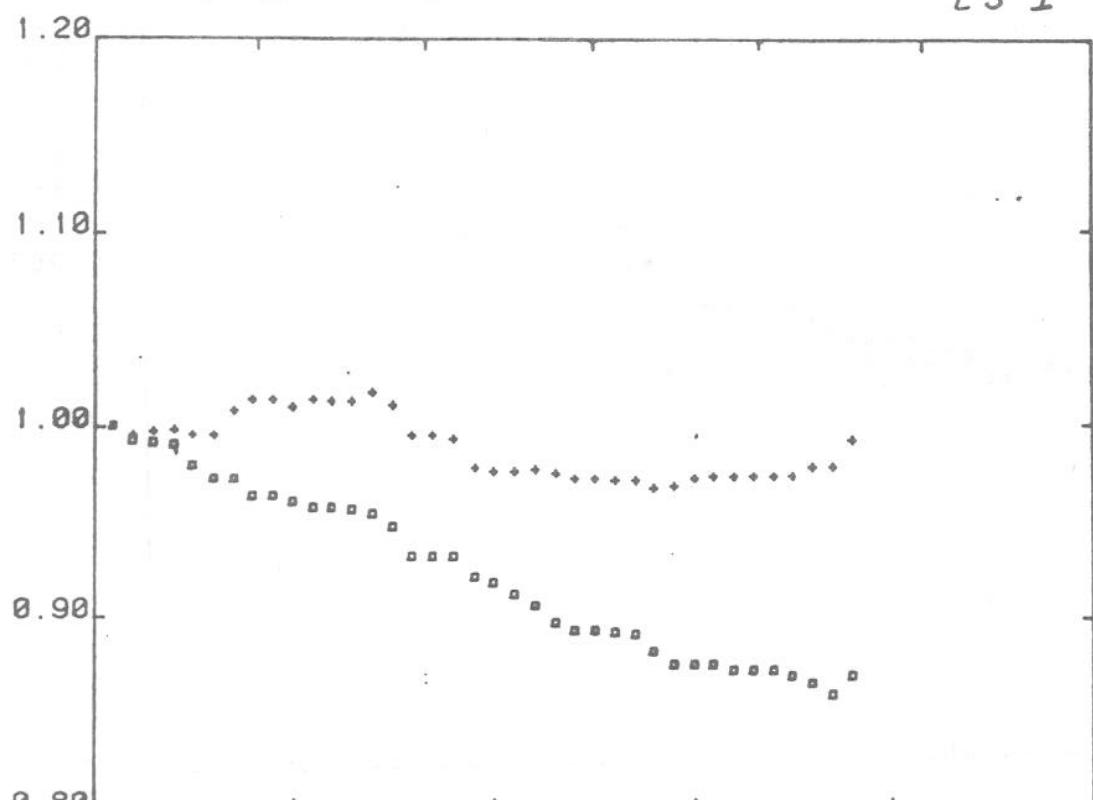
STATE ?

STATE ?

|         | UNDER       | NORMAL               | OVER       | UNDER     | NORMAL               | OVER                 |
|---------|-------------|----------------------|------------|-----------|----------------------|----------------------|
| set     | $y = y_1/5$ | $y = y_1/5$          | $y = 2y_1$ | $y = y_1$ | $y = y_1/5$          | $y = y_1/5$          |
| default | $x = x_1$   | $x = \min(x_0, x_1)$ | $x = x_1$  | $x = x_1$ | $x = \min(x_0, x_1)$ | $x = \min(x_0, x_1)$ |

L3 I

$\beta + 59^\circ$   
 $y_0 = 3.06$   
PRT = 1.13

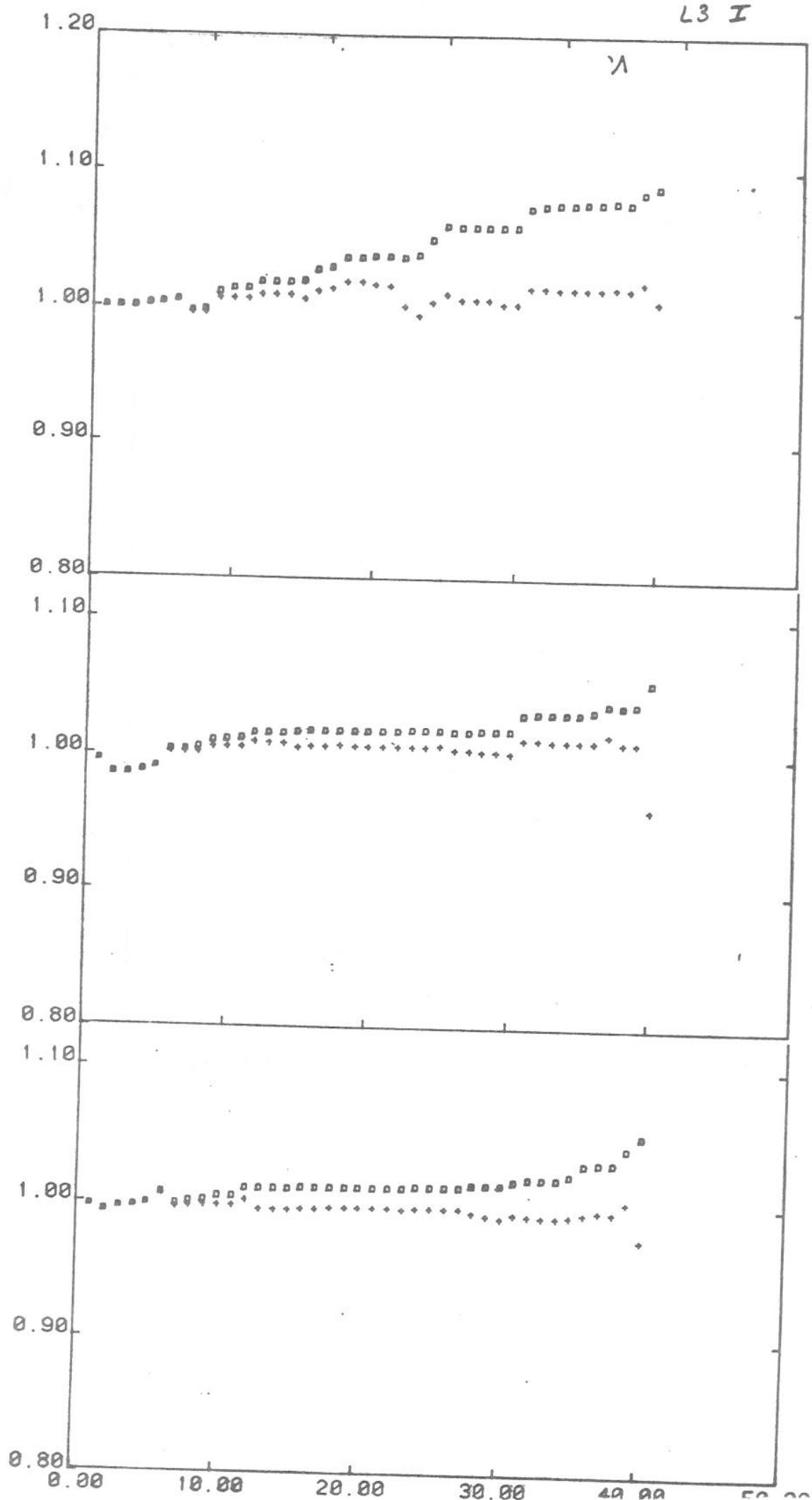


L3 I

$\beta = +59^\circ$

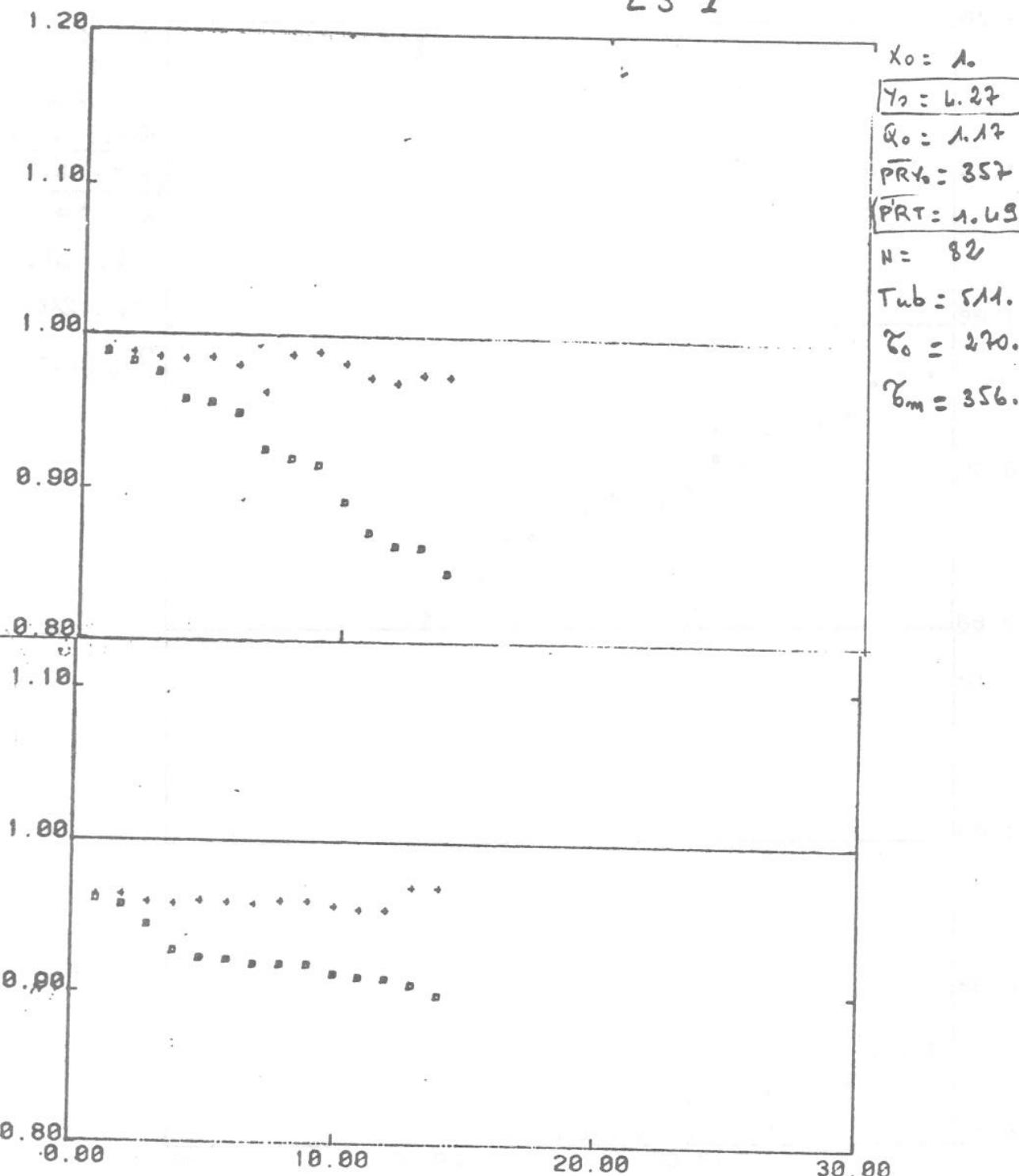
$y_0 = 3.82$

PRT = 1.9



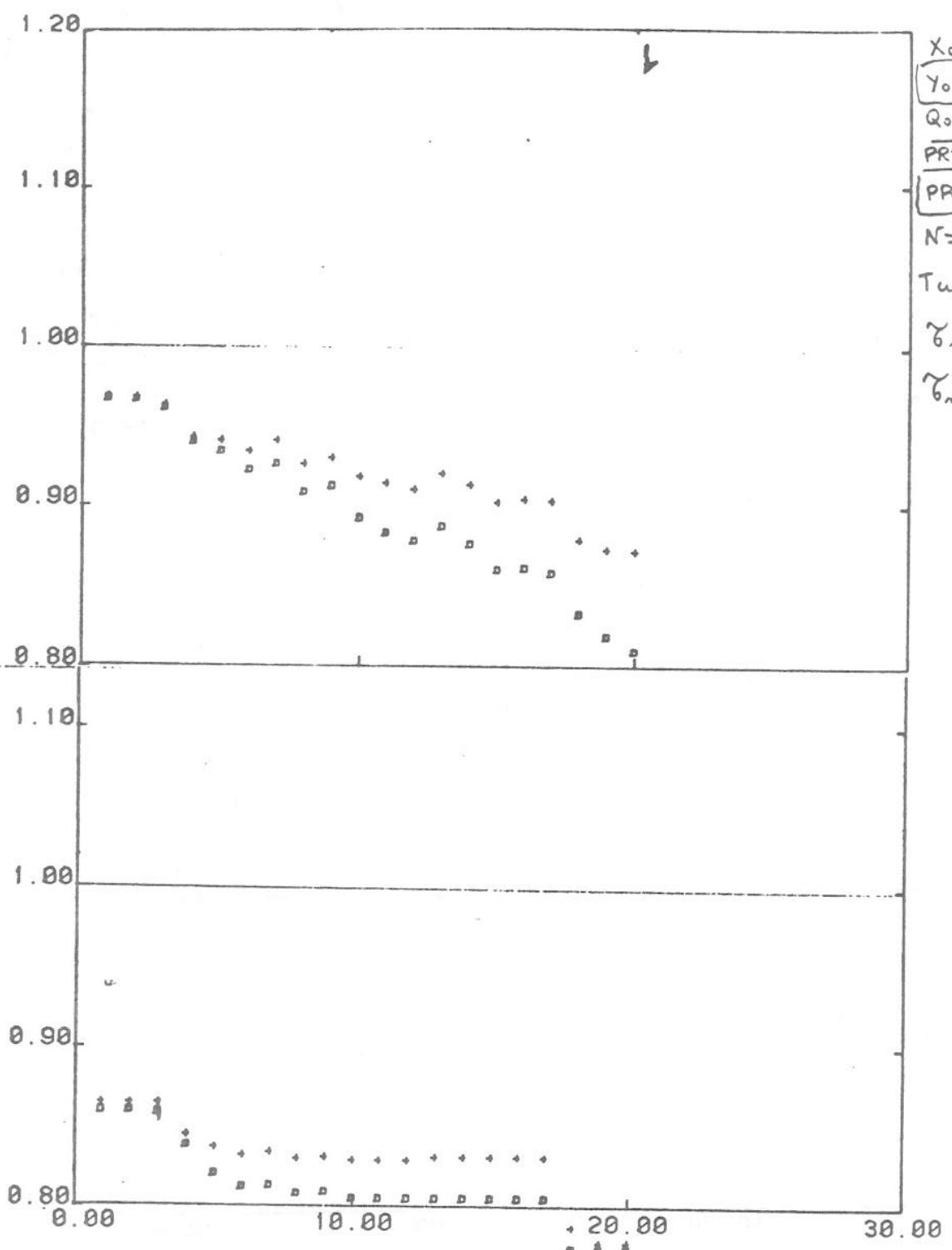
$P = 0$

L3 I



L3 I

$\beta \sim 0$



$$X_0 = 1.$$

$$Y_0 = 3.89$$

$$Q_0 = .62$$

$$\overline{PRY}_0 = 6.20$$

$$\overline{PRT} = 6.20$$

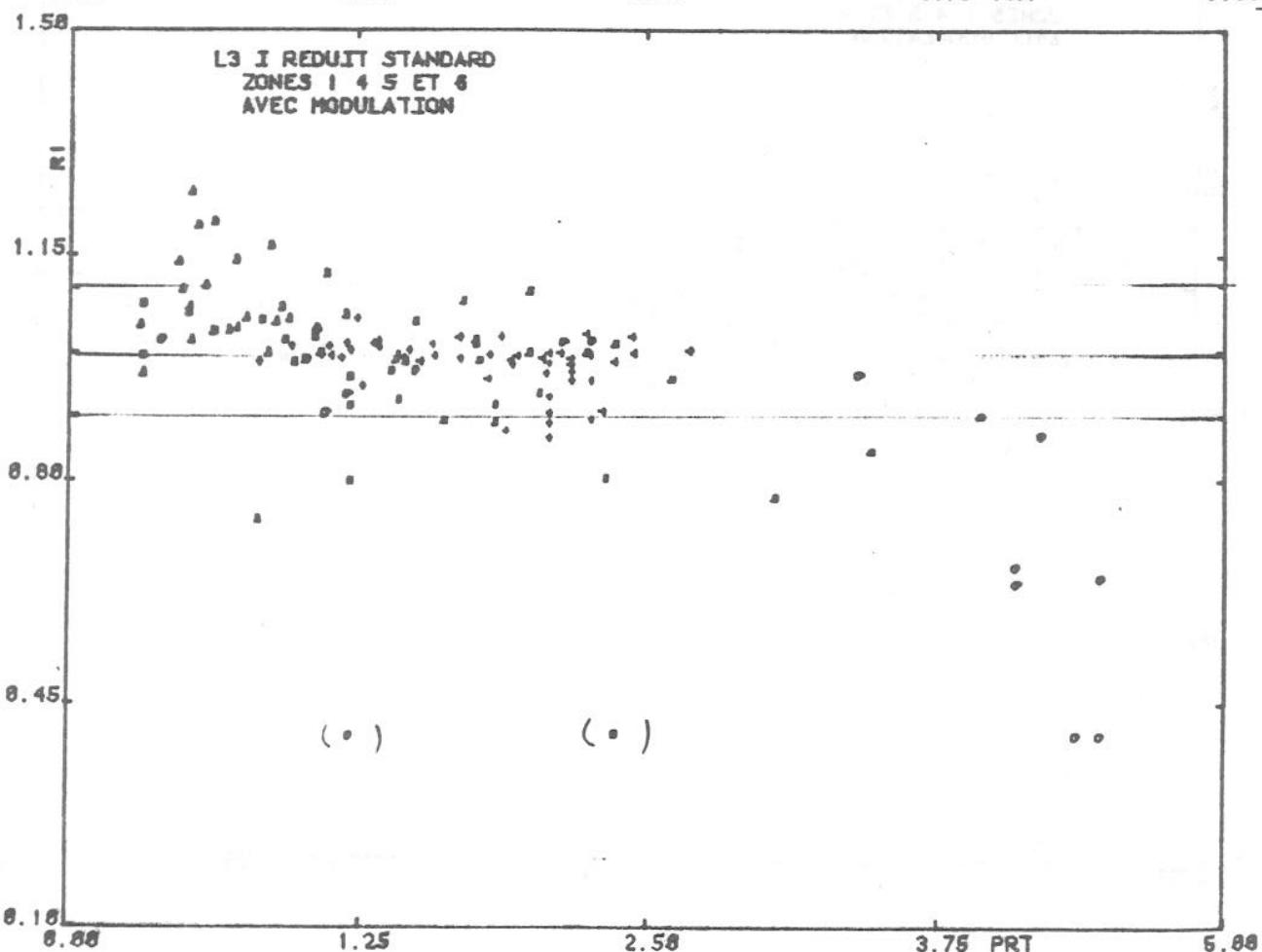
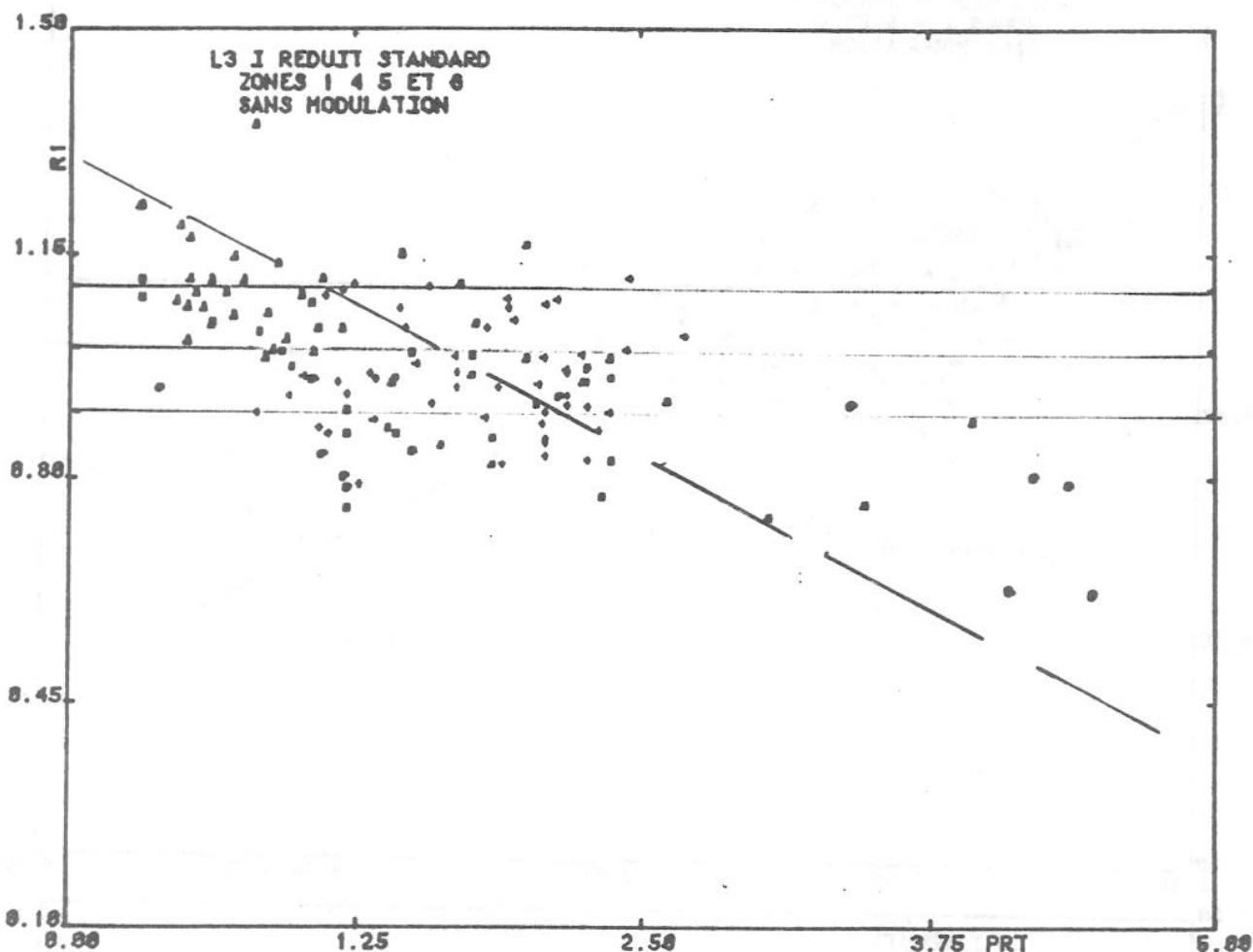
$$N = 49$$

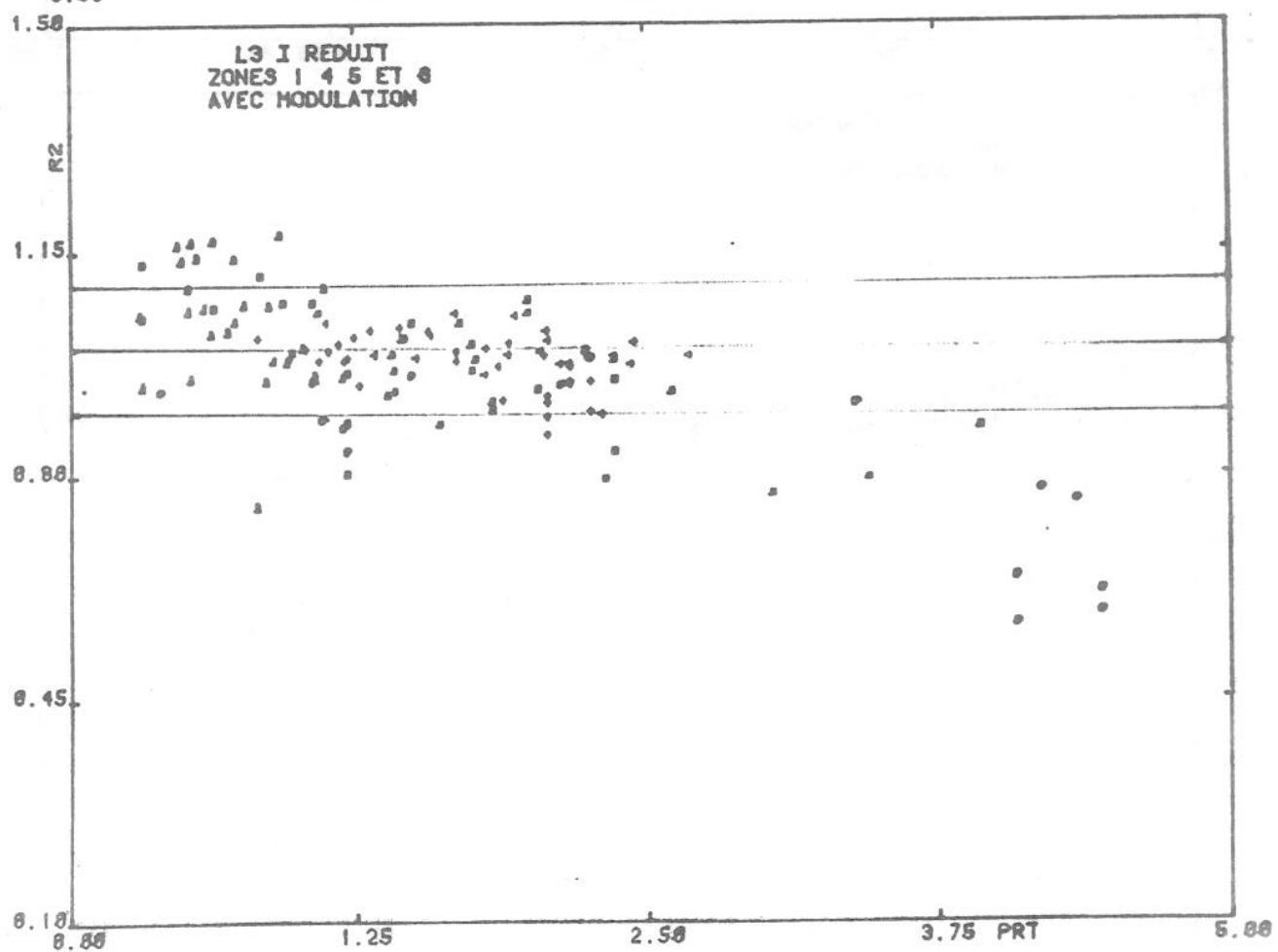
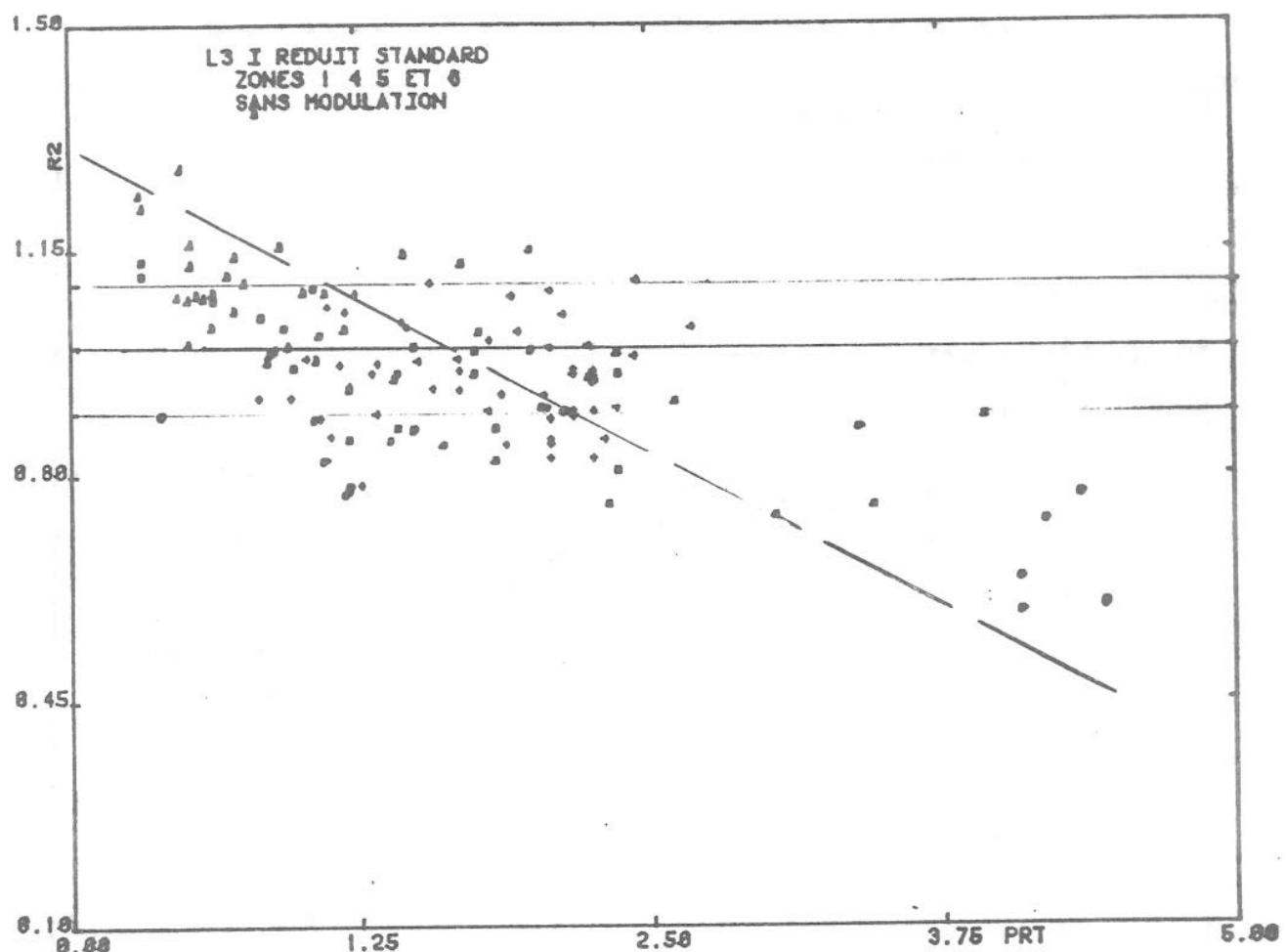
$$T_{ub} = 465.$$

$$\gamma_A = 210.$$

$$\gamma_m = 248.$$

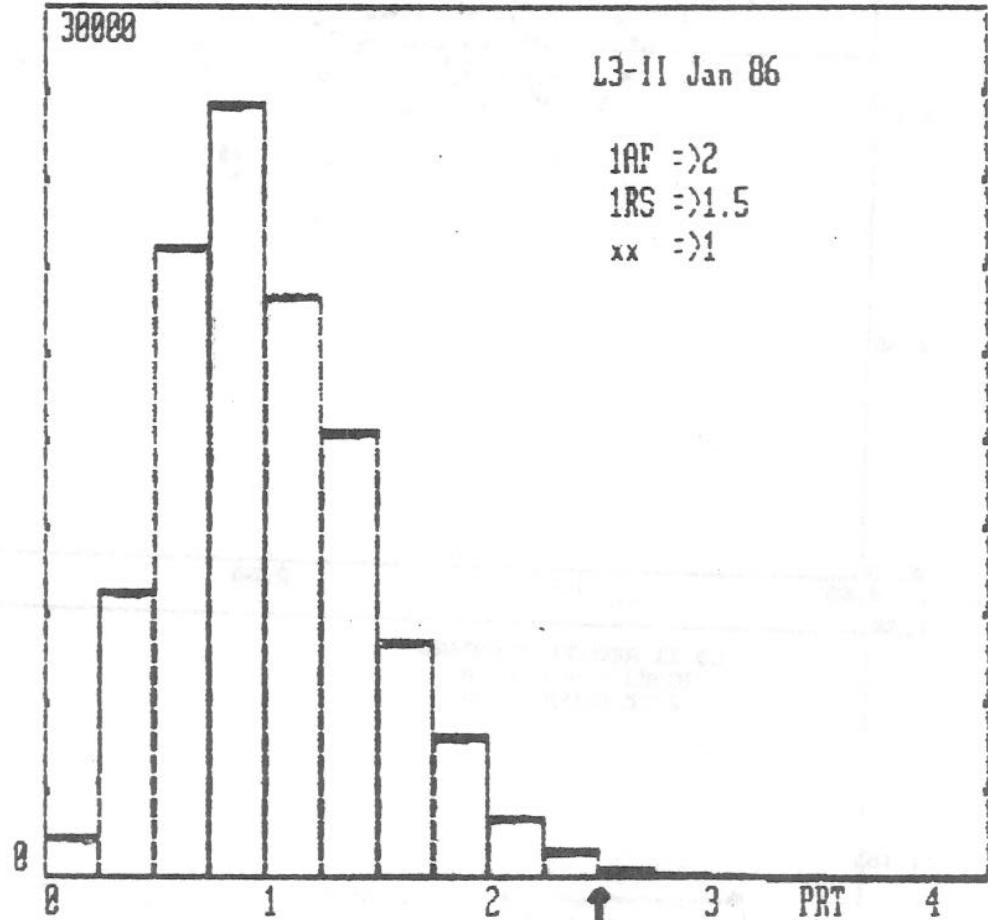
Parallaxe Target Accuracy / Total Pressure  
Achieved  
in red: initial distorted response





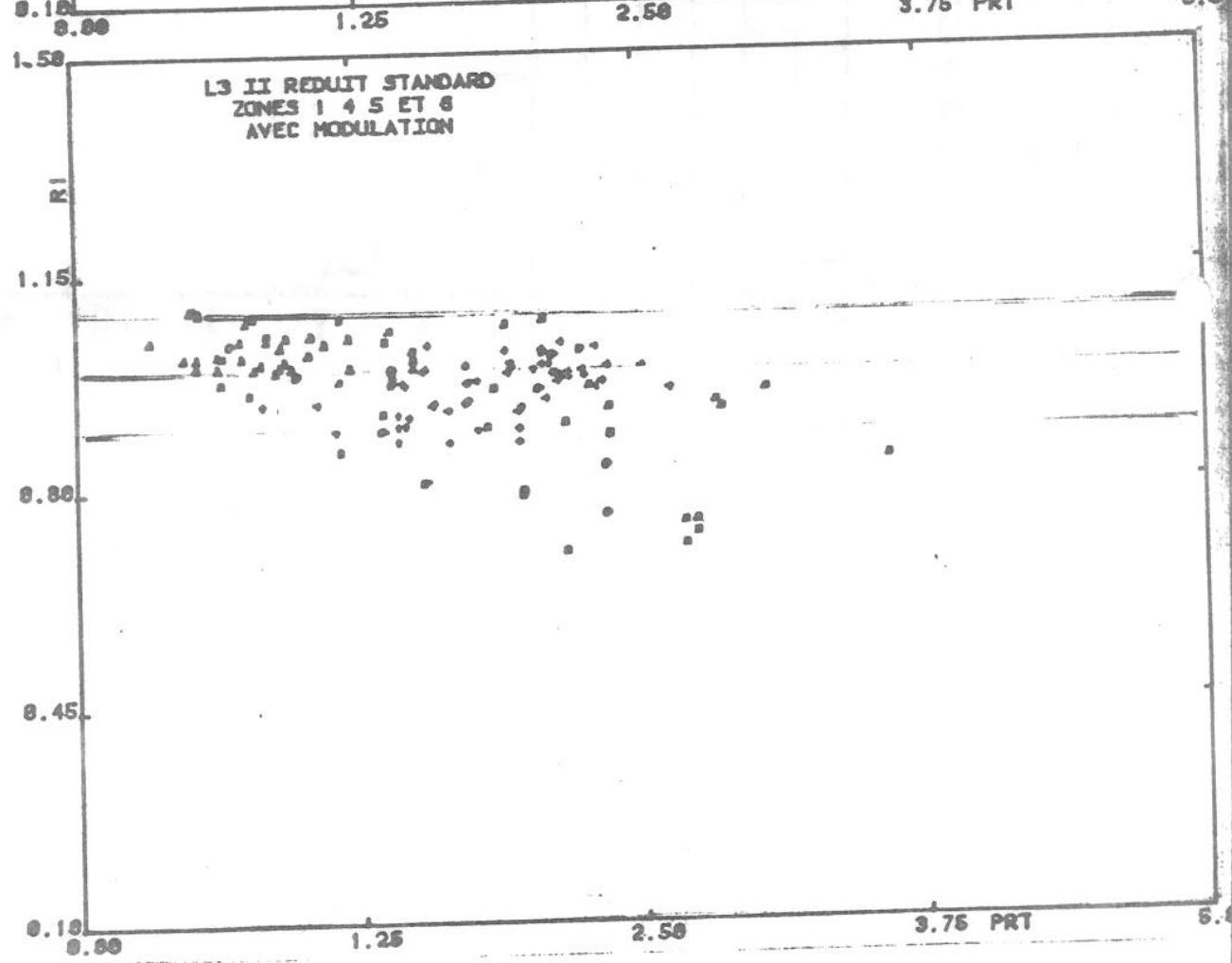
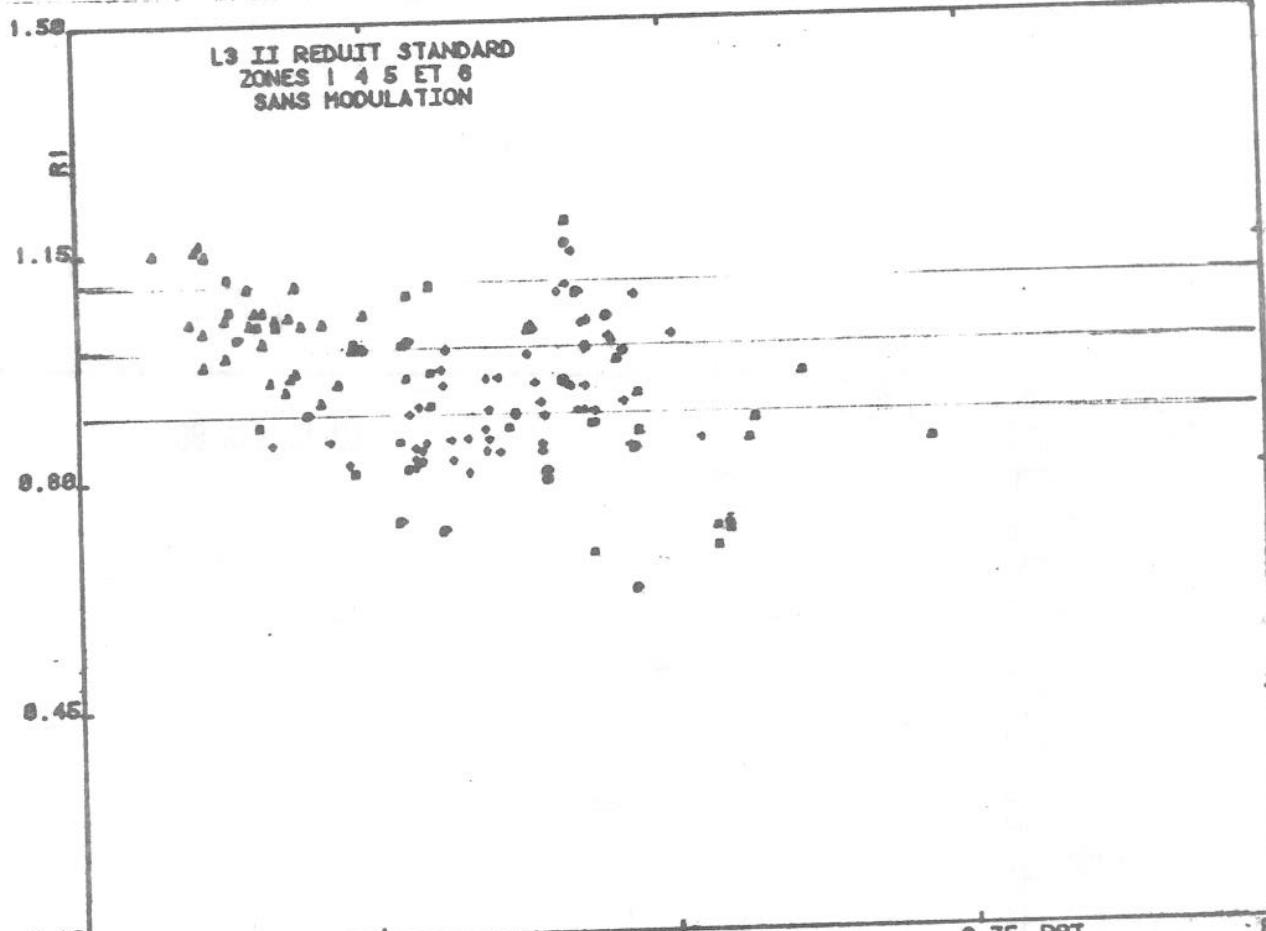
Mtot = 111976

| PRT    | N     |
|--------|-------|
| <.25   | 1470  |
|        | 9878  |
|        | 21718 |
| .75-1  | 26522 |
|        | 29083 |
|        | 15366 |
|        | 8113  |
| 1.75-2 | 4977  |
|        | 2166  |
|        | 998   |
|        | 341   |
| 2.75-3 | 141   |
|        | 63    |
|        | 28    |
|        | 11    |
| 3.75-4 | 2     |
|        | ?     |



FOLD

77



*μ<sub>A</sub>*

1.58

L3 II REDUIT STANDARD  
ZONES 1 4 5 ET 6  
SANS MODULATION

R2

1.15

0.88

0.45

0.18

0.00

1.25

2.50

3.75 PRT

5.00

1.58

L3 II REDUIT STANDARD  
ZONES 1 4 5 ET 6  
AVEC MODULATION

R2

1.15

0.88

0.45

0.18

0.00

1.25

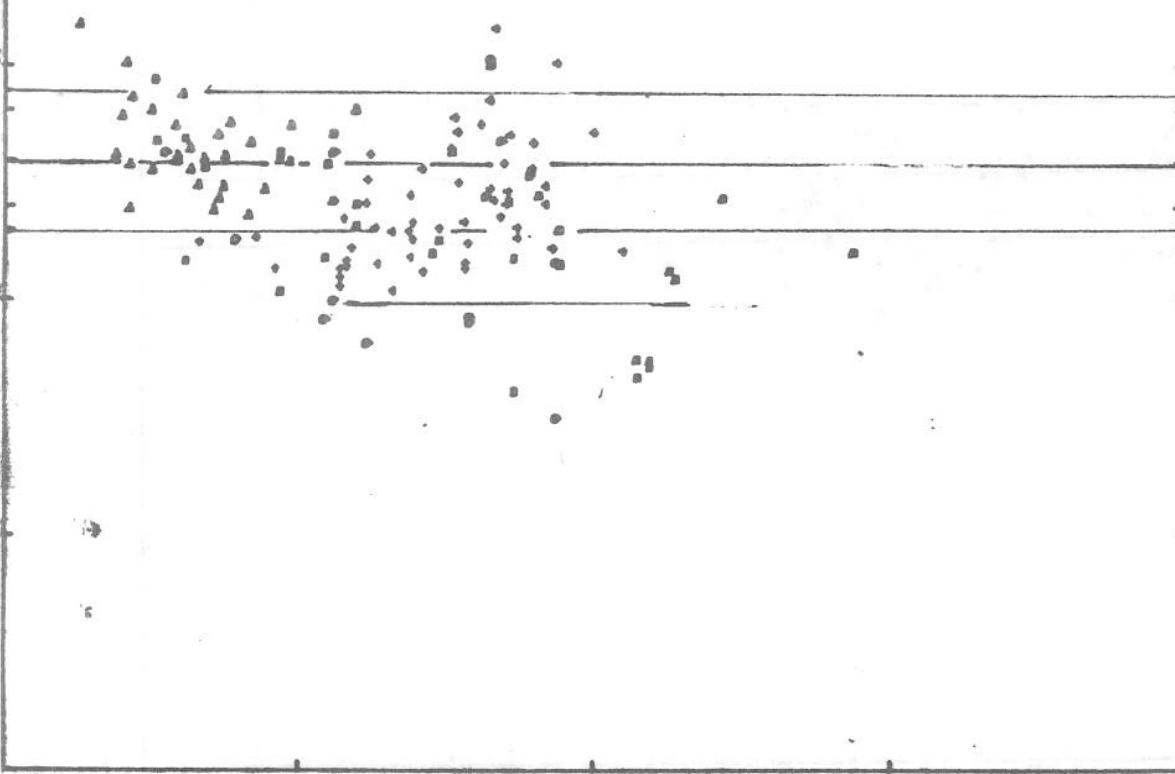
2.50

3.75 PRT

5.00

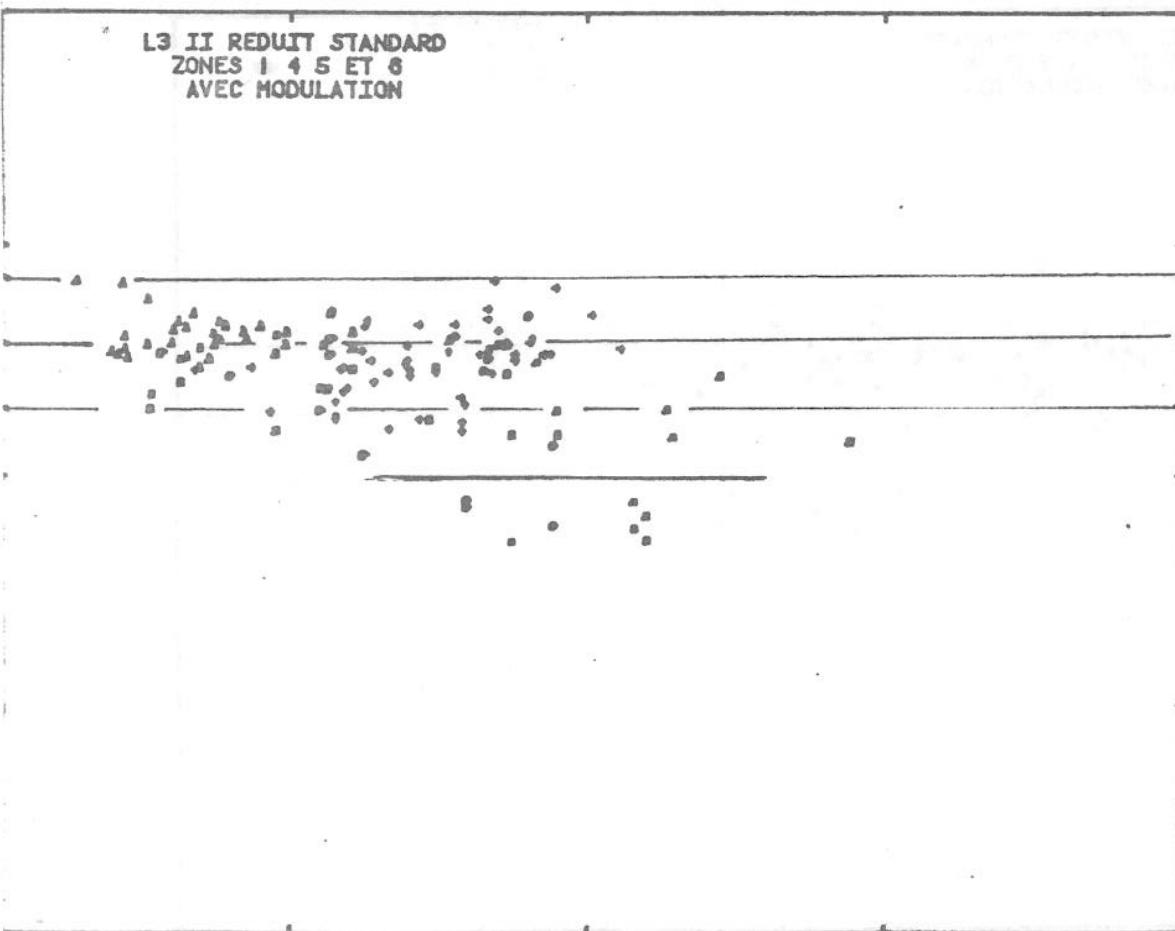
$\mu_B$

L3 II REDUIT STANDARD  
ZONES 1 4 5 ET 8  
SANS MODULATION

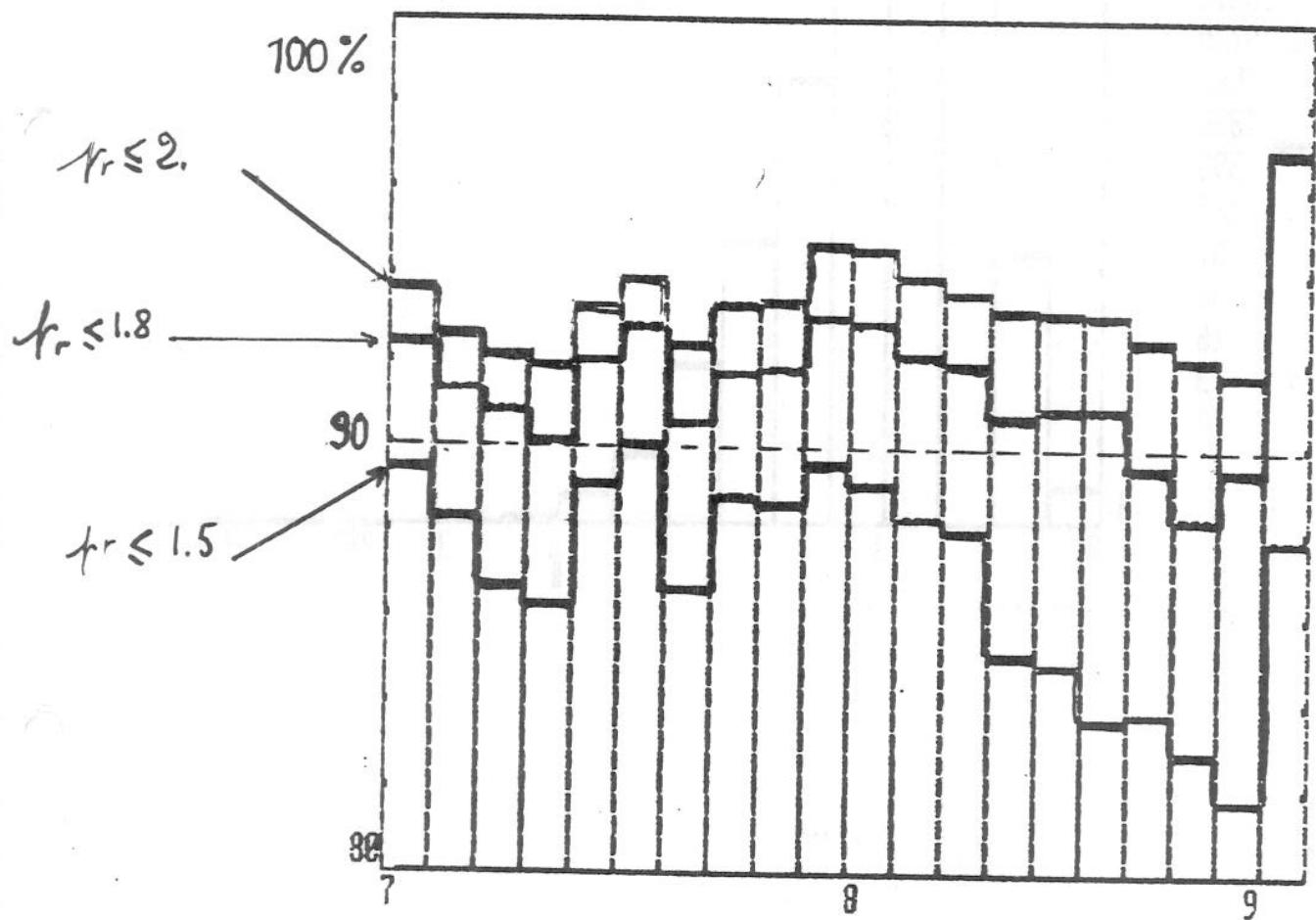


00 1.25 2.50 3.75 PRT 5.00

L3 II REDUIT STANDARD  
ZONES 1 4 5 ET 8  
AVEC MODULATION



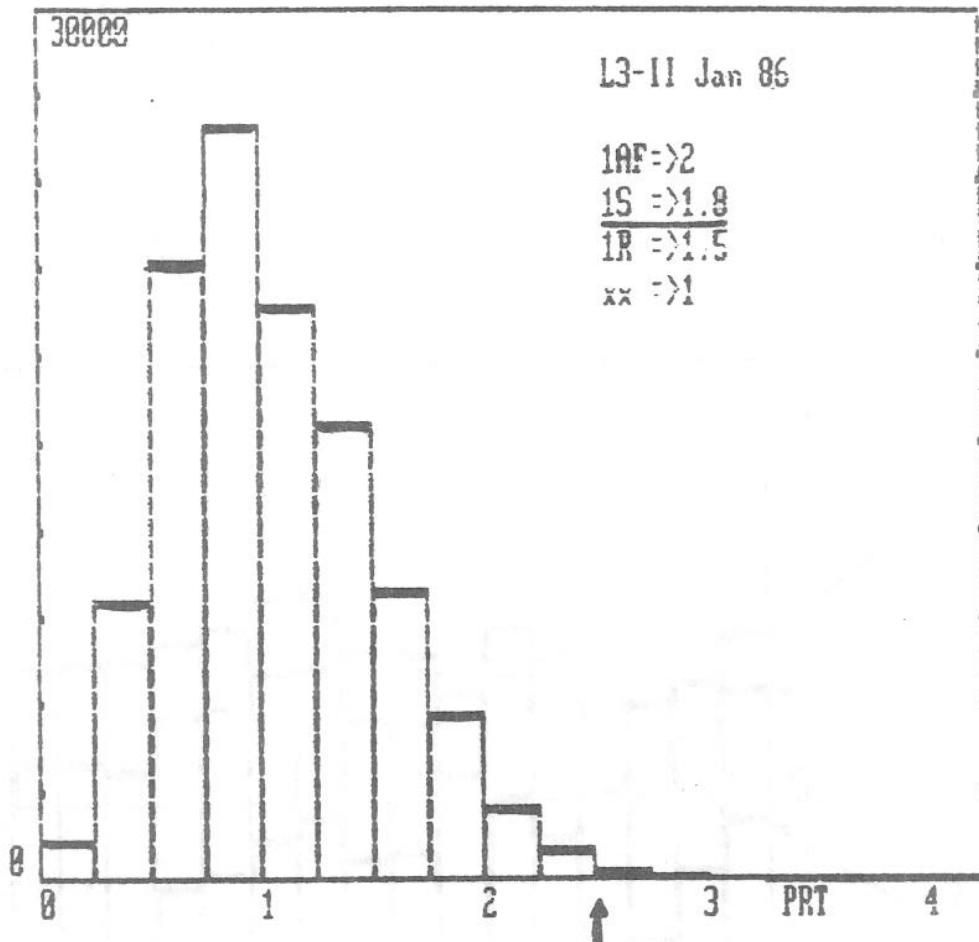
00 1.25 2.50 3.75 PRT 5.00



Survey Completeness

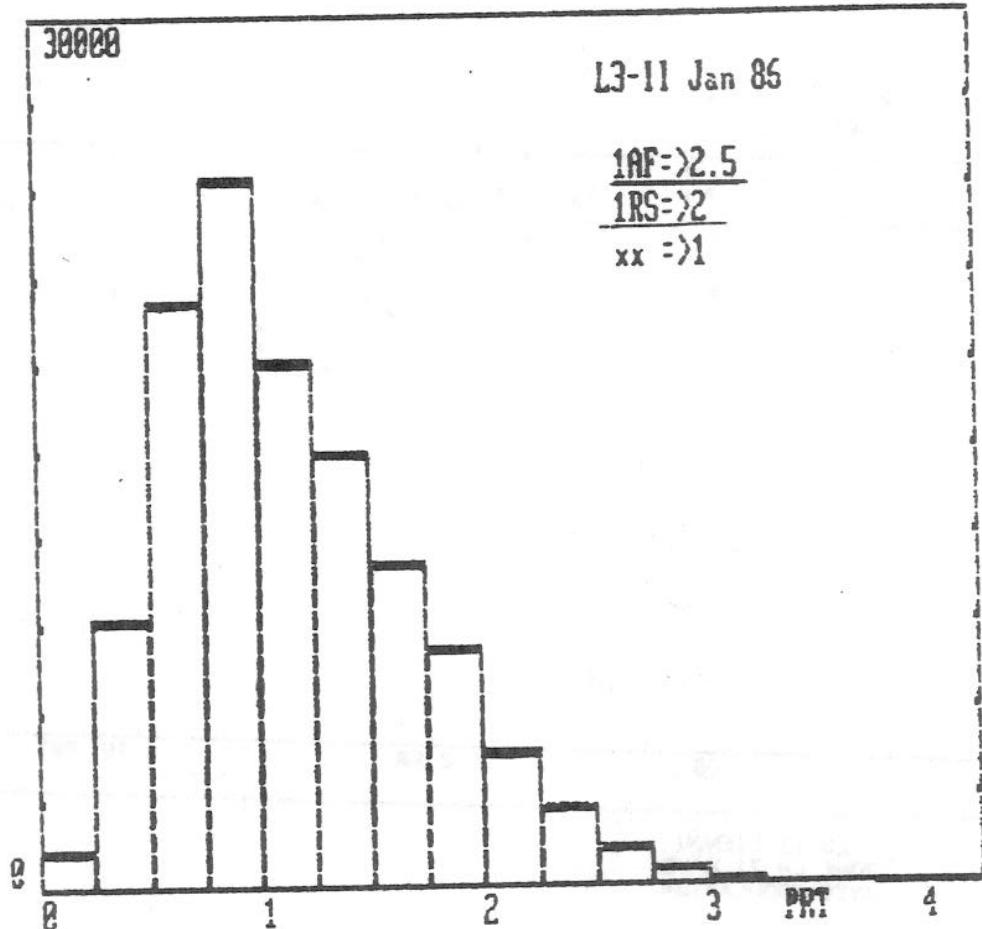
$N_{tot} = 113956$

| PRT    | N     |
|--------|-------|
| <.25   | 1446  |
|        | 9622  |
|        | 21248 |
| .75-1  | 26903 |
|        | 19799 |
|        | 15777 |
|        | 10012 |
| 1.75-2 | 5720  |
|        | 2565  |
| →      | 1086  |
|        | 393   |
| 2.75-3 | 162   |
|        | 67    |
|        | 36    |
|        | 10    |
| 3.75-4 | 3     |
|        | ?     |

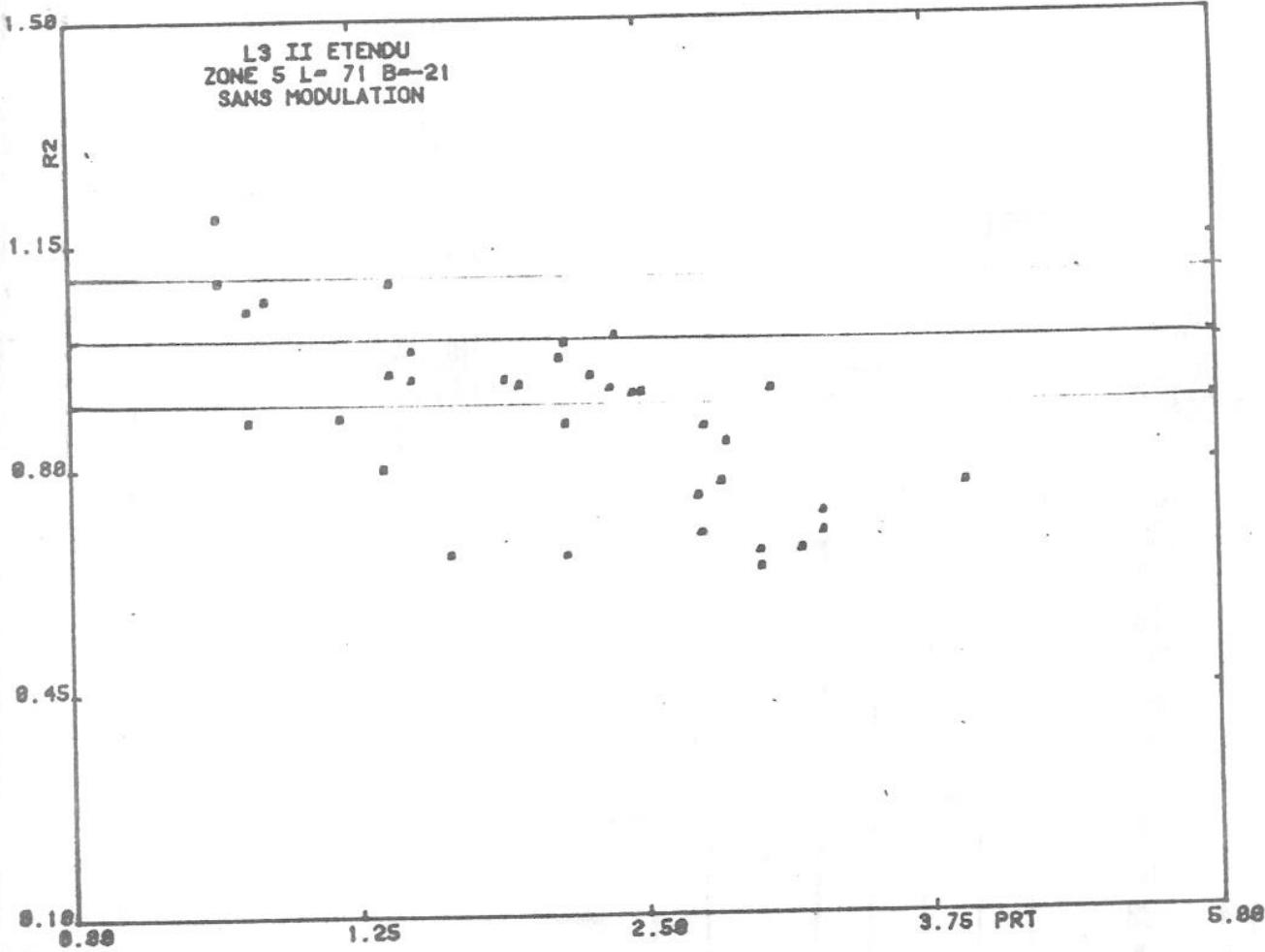


$N_{tot} = 118119$

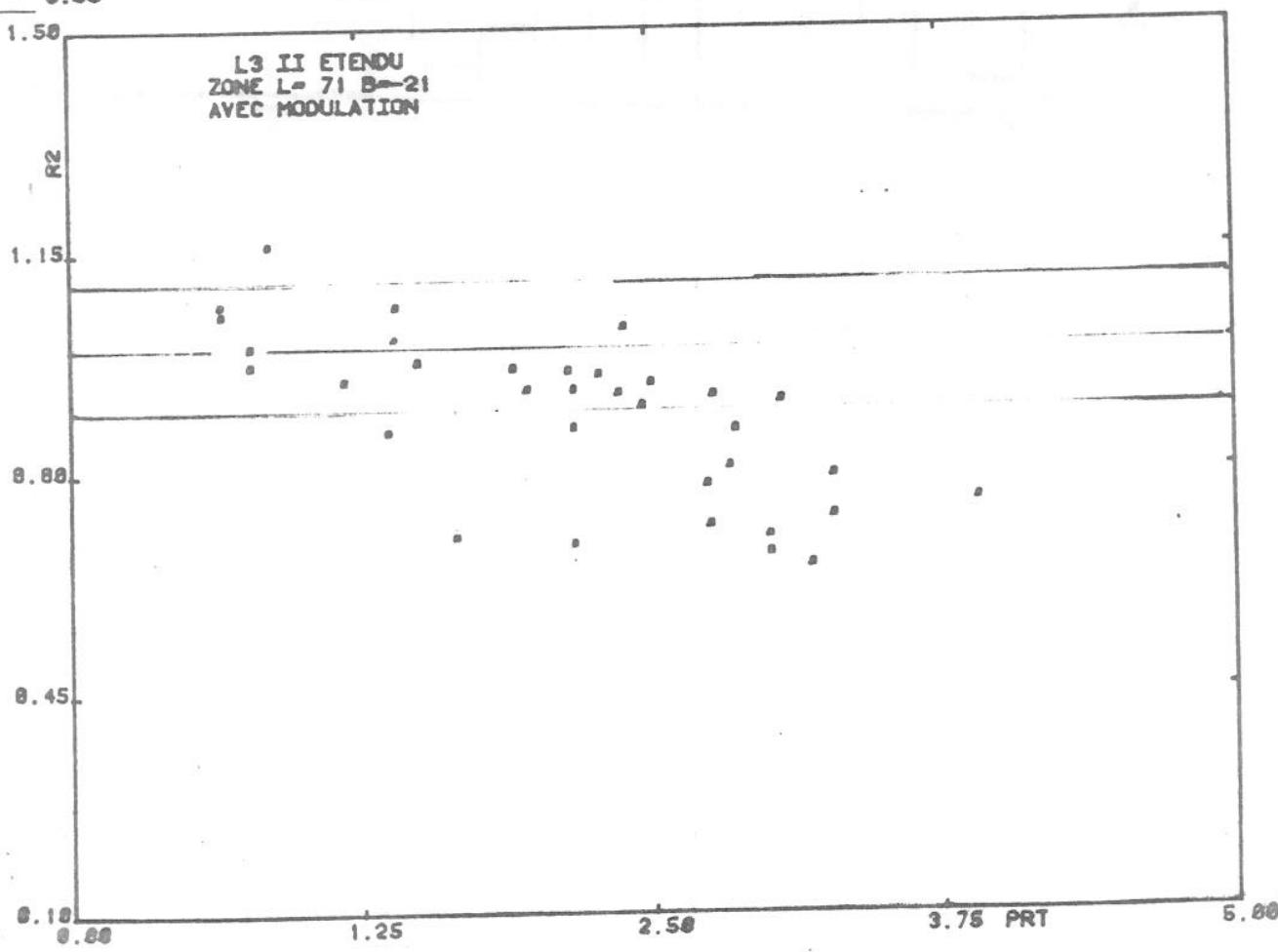
| PRT    | N     |
|--------|-------|
| <.25   | 1401  |
|        | 9240  |
|        | 20240 |
| .75-1  | 24484 |
|        | 18175 |
|        | 15825 |
|        | 11136 |
| 1.75-2 | 8258  |
|        | 4715  |
|        | 2791  |
|        | 1380  |
| 2.75-3 | 687   |
|        | 319   |
|        | 139   |
|        | 66    |
| 3.75-4 | 28    |
|        | 35    |



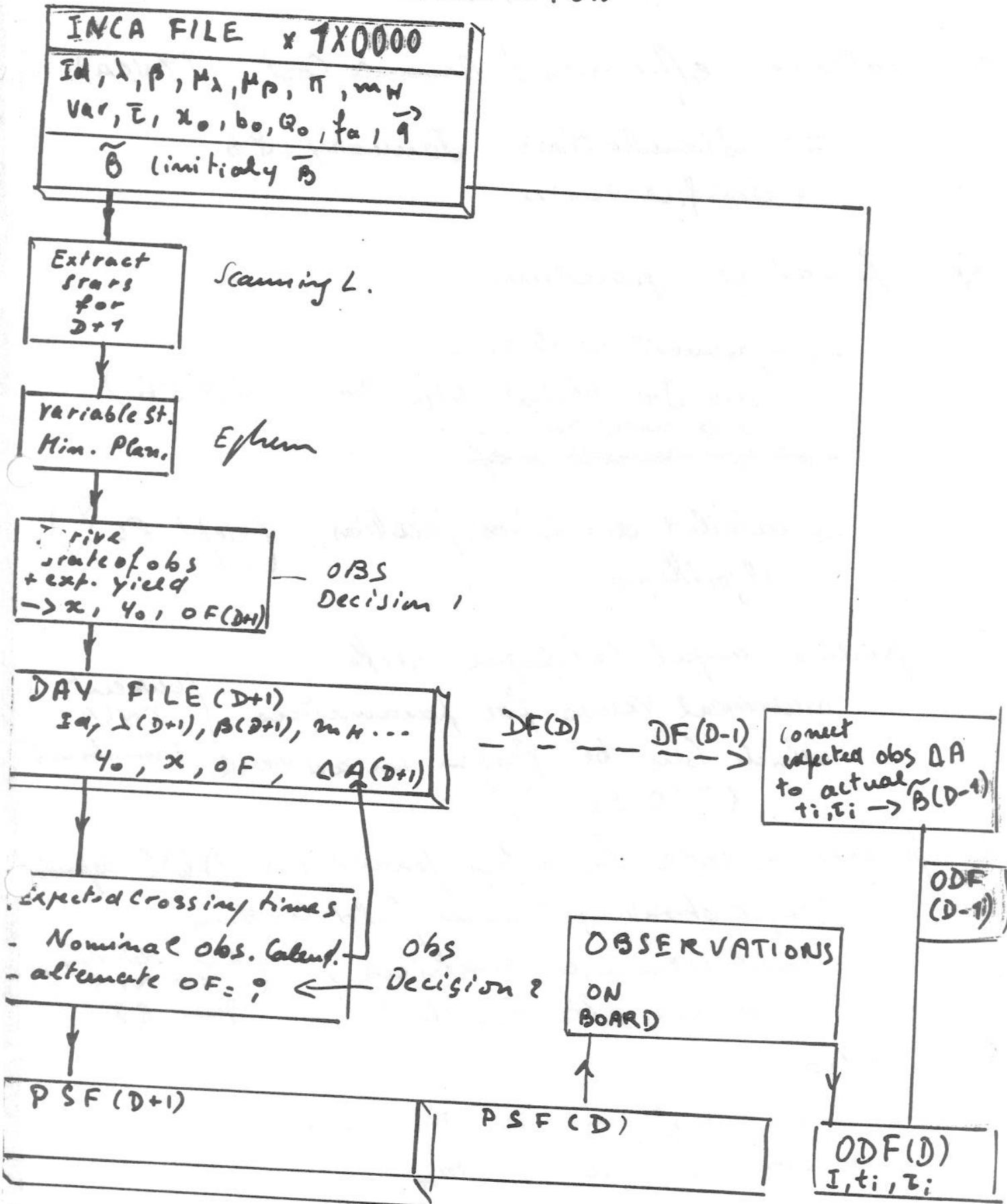
L3 II ETENDU  
ZONE 5 L= 71 B=21  
SANS MODULATION



L3 II ETENDU  
ZONE L= 71 B=21  
AVEC MODULATION



# PSF PRODUCTION



## NEXT STEPS

1) balance efficiency / Resource Cost (INCA)

⇒ Simulations January 86  
+ Clarified version

2) finalize procedure

→ agreement with ESOC  
and On global Algorithm (Mid 86)  
file description ...  
~~target acceptance of~~

→ detailed description peculiar (Sept. 86?)  
algorithms

3) produce input Catalogue with

numerical values for parameters  
which can be frozen in advance  
(PMO stars?)

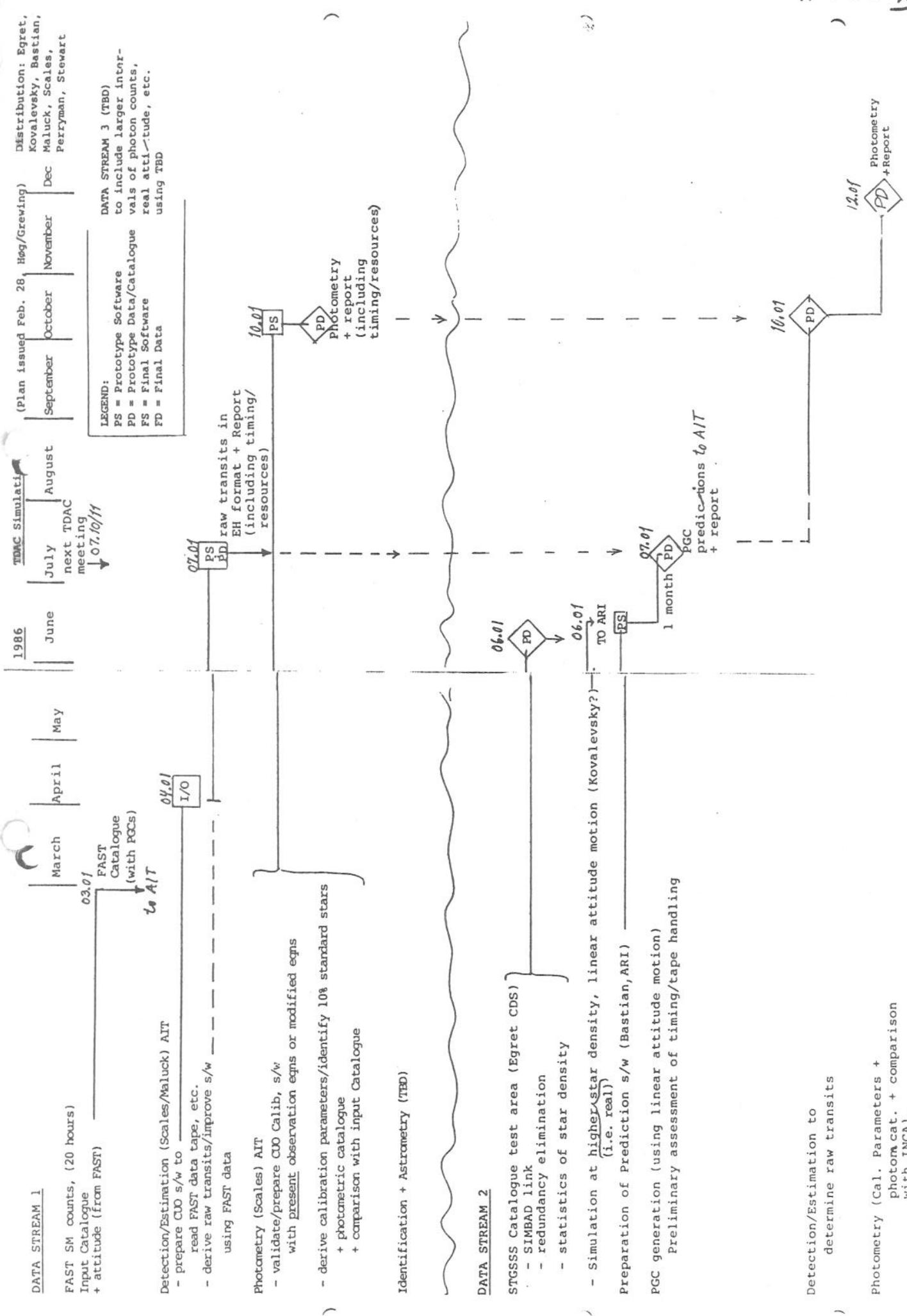
Current  
INCA

Commitment

4) produce a code for other parameters (NDC depends  
(target observing time for field working  
target Covariance matrices) (first delivery  
(to be run after launch) - Jan 87  
for tests)

5) Expected

- final constraints on minimum  
observing times  $x_0(m_H)$
- comments, questions about  
proposed procedure
- check of possible interactions with  
other off





## ACCURACY OF STAR ABSCISSAE

(Simulation studies Reduction on circles)

A. INCREASING NUMBER OF STARS

B. VARIABLE STAR DENSITY

A. Distinguish : increase

- at all magnitudes proportionally

Code : P

- at magnitude g exclusively

Code : g

A & B. Distinguish : - geometrical altitude

Code : G

- smoothed altitude

Code : S

19.6.86-2

## SUMMARY EARLIER RESULTS (Copenhagen)

1 SCANNING CIRCLE      800 \*\* /circle  
 = 100,000 /sphere

+ 50% = 1200 \*\* /circle  
 150,000 /sphere

GEOMETRIC MODE ONLY

| (mas)    | 800  | 1200 (+ mag g) | 1200 (prop.) |
|----------|------|----------------|--------------|
| overall  | 6    | 7.00           | 8.01         |
| mag g    | 6.22 | 6.64           | 6.97         |
| rigidity | 2.6  | 2.4            | 2.3          |

| (mas) | 800 | 1200 (+ g) | 1200 (P) |
|-------|-----|------------|----------|
| mag 8 | 6   | 6          | 7        |
| 9     | 6   | 7          | 7        |
| 10    | 7   | 7          | 8        |
| 11    | 8   | 9          | 9        |
| 12    | 11  | 12         | 13       |

CONCLUSION: INCREASING THE CATALOGUE  
 DOES LITTLE HARM  
 (GEOMETRIC MODE)

19.3.86.3

## SUMMARY EARLIER RESULTS

(Copenhagen) (Dwingeloo)

### 1 SCANNING CIRCLE

Sphere: 100000 120,000 150000 200000

| Code   |    | OVERALL ACCURACY ( $\sigma$ (mas)) |     |      |      |
|--------|----|------------------------------------|-----|------|------|
| year   | GP | 800                                | 960 | 1200 | 1600 |
| smooth | SP | 7.                                 | 7.2 | 8    | 8.3  |
|        |    | 5.5                                | 6.1 | 6.9  | 7.4  |
| Gg     |    |                                    |     |      |      |
| Sg     |    | 7.                                 | 6.9 | 7.4  | 7.4  |
|        |    | 5.5                                | 5.9 | 6.3  | 6.4  |

Code : Sg (smooth + mag. g)

| $\zeta$ (mas) | 800 | 960  | 1200 | 1600 |
|---------------|-----|------|------|------|
| mag 9         | 4.5 | 4.8  | 5.2  | 5.6  |
| 10            | 5.3 | 5.9  | 6.4  | 6.8  |
| 11            | 6.9 | 7.9  | 8.4  | 8.8  |
| 12            | 9.8 | 11.0 | 12.3 | 12.8 |

CONCLUSION : WITH SMOOTHING OF ATTITUDE  
INCREASING THE CATALOGUE  
DOES MORE HARM THAN  
WITHOUT SMOOTHING

19.3.86.4

NEW RESULTS :

5 SCANNING CIRCLES

2900 SIMULATED STARS =

1600 OBSERVED STARS =

87,000 \*\* /sphere

87%

2880 STARS - 104,000

3600 STARS - 130,500

/sphere

104 %

/sphere 130 %

OVERALL  $\sigma$  (MAS)

|    | 87 % | 104 % | 130.5 % |        |
|----|------|-------|---------|--------|
| GP | 5.0  | 5.0   | 5.2     | +4%    |
| SP | 4.0  | 4.2   | 4.7     | +12%   |
| G9 | 5.0  | 4.7   | 4.7     | (!)-6% |
| S9 | 4.0  | 4.0   | 4.2     | +5%    |

GEOMETRIC P/g

| (MAS) | 87 % | 104 %   | 130.5 %     |  |
|-------|------|---------|-------------|--|
| 8     | 3.7  | 3.6/3.5 | 3.5/3.5 -5% |  |
| 9     | 4.2  | 4.0/3.9 | 4.1/3.9 -4% |  |
| 10    | 4.7  | 4.6/4.6 | 4.7/4.7 0   |  |
| 11    | 5.9  | 6.1/5.9 | 6.3/6.2 +5% |  |
| 12    | 8.4  | 8.6/8.5 | 8.9/8.6 +6% |  |

SMOOTHING P/g

|    | 87  | 104     | 130        | + |
|----|-----|---------|------------|---|
| 8  | 2.2 | 2.4/2.3 | 2.4/2.4 9  |   |
| 9  | 2.3 | 2.9/2.9 | 3.2/3.1 14 |   |
| 10 | 3.6 | 3.8/3.8 | 4.1/4.1 14 |   |
| 11 | 5.2 | 5.4/5.2 | 6.2/6.2 19 |   |
| 12 | 8.0 | 8.2/8.2 | 8.9/8.6 10 |   |

CONCLUSION : WITH MORE CIRCLES THE RESULTS  
LOOK BETTER AGAIN

Fig. 3.86.5

### WORK LOAD WITH HIGHER DENSITIES

|             | 87% | 64% | 130% |
|-------------|-----|-----|------|
| NORMAL EQU. | 14  | 17  | 21   |
| CHOLESKI    | 8   | 17  | 33   |
| SOLUTION    | 2   | 2   | 3    |
| VARIANCES   | 23  | 49  | 96   |
| SMOOTHING   | 21  | 22  | 25   |
| TOTAL       | 69  | 108 | 179  |

CPU - seconds on IBM 3083

179 seconds ~ 6 minutes on CDC 750

CONCLUSION : CHOLESKI & VARIANCES  
INCREASE RAPIDLY  
BUT ARE ONLY A PART  
OF THE REDUCTION

HIGHER DENSITIES LEAD TO BETTER RIGIDITY

SO, QUESTION: COULD WE TAKE LESS  
REVOLUTIONS IN ONE RGC, AND STILL GET  
GOOD RIGIDITY (AND LESS CPU-TIME)?

TYPICAL RIGIDITY, 5 CIRCLES, GEM.  $\nu = 1.7$

AND, 1 CIRCLE : 800 960 1200 1600

$\nu = 2.6 \quad 2.5 \quad 2.4 \quad 2.1$

ANSWER : NO (similar with smoothing)

19.3.86.6

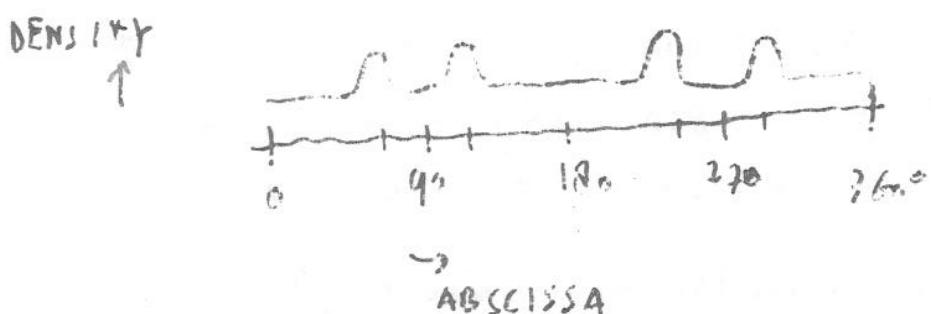
## B. VARIABLE DENSITY

- NOT ALL ECLIPSTIC LATITUDES  $\beta$  ARE SCANNED AS OFTEN
- DEFINE  $N(\beta)$  = NUMBER OF SCANS
- IDEA : TO COMPENSATE THIS BY INCLUDING MORE STARS AT  $\beta$ 'S WITH LARGER  $N(\beta)$
- DENSITY :  $D(\beta) \sim 1/N(\beta)$

QUESTION : EFFECT OF THIS ON OVERALL ACCURACY  
" " " " " RIGIDITY

EXPERIMENTS : 1 CIRCLE      MAGNITUDE  $\eta$   
800 \*\*      STARS ONLY  
GEOMETRIC &  
SMOOTHING

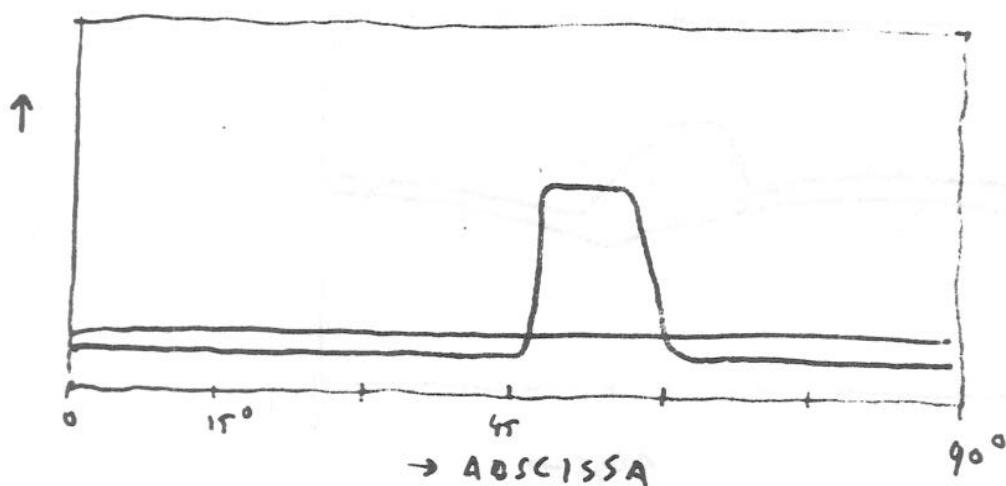
DENSITY PEAK AT  $55^\circ$  (ABSCISSA ON CIRCLE)  
2 TIMES HIGHER THAN AVERAGE  
PEAK WIDTH  $\sim 10^\circ$



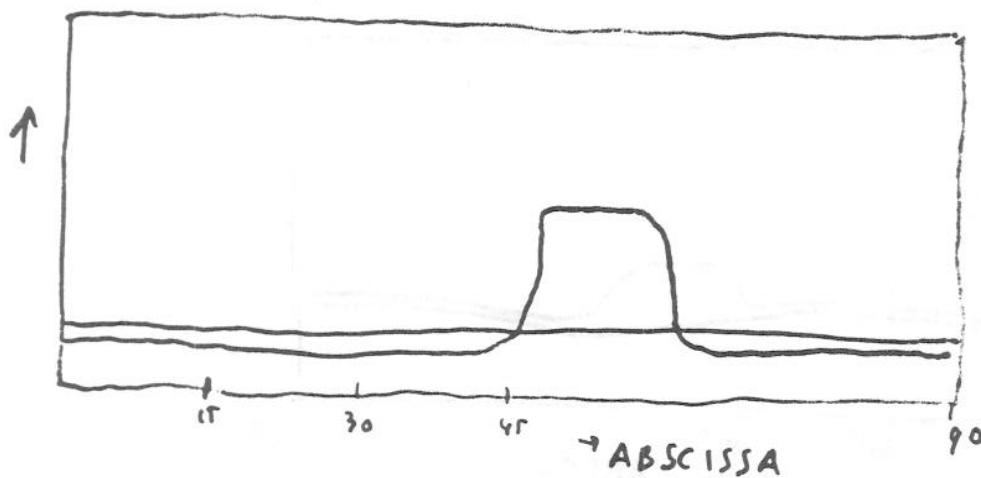
PEAK AT 55°

19.3.86.7

STAR DENSITY



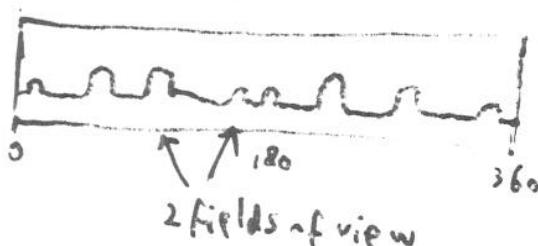
$1/\text{OBS. WEIGHT} (*)$



— = constant density  
— = variable density

(\*) OVER THE WHOLE CIRCLE

$1/\text{OBS. WEIGHT}$  IS  
LIKE THIS



### OVERALL RESULTS

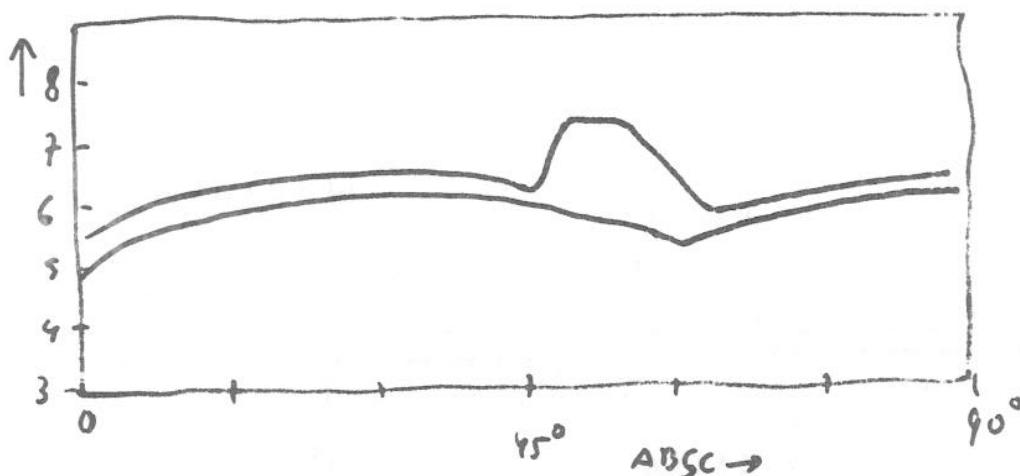
| GEOM  |  | $\sigma^*(\text{mas})$ | rigidity |
|-------|--|------------------------|----------|
| const |  | 5.8                    | 4.4      |
| var   |  | 6.4                    | 4.2 (!)  |

| SMOOTH |  | $\sigma^*(\text{mas})$ | rigidity |
|--------|--|------------------------|----------|
| const  |  | 4.5                    | 2.6      |
| var    |  | 4.9                    | 2.4 (!)  |

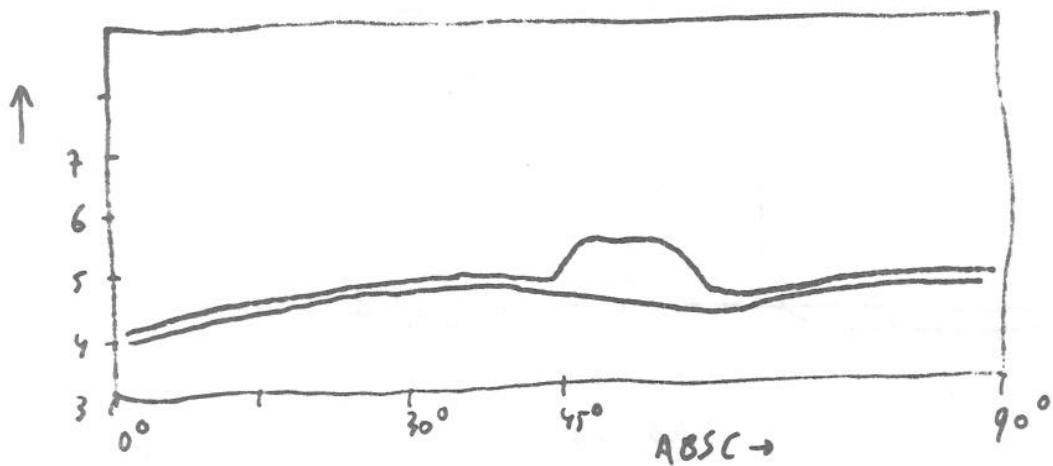
19.3.86.8

6' GEOM.

PEAK AT 55°



6' SMOOTH



— = const. dens.

— = var. dens.

CONCLUSION: THE EFFECT REMAINS  
① ALMOST LOCAL, IN PARTICULAR  
IN CASE OF SMOOTHING

② THE RIGIDITY REMAINS  
GOOD

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### ESOC - HIPPARCOS STATUS

#### PRINCIPAL RECENT MILESTONES:

- MISSION IMPLEMENTATION PLAN FINALISED
- SOFTWARE REQUIREMENTS REVIEW COMPLETED
- COMPUTER CONFIGURATION DEFINED

#### PRESENT ACTIVITIES:

- SOFTWARE ARCHITECTURAL DESIGN HAS STARTED
- SOFTWARE REQUIREMENTS BEING FINALISED
- HIPPARCOS USER MANUAL BEING ANALYSED  
FOR DEFINITION OF OPERATIONS PLAN
- STUDIES ON INITIALISATION BEING PERFORMED



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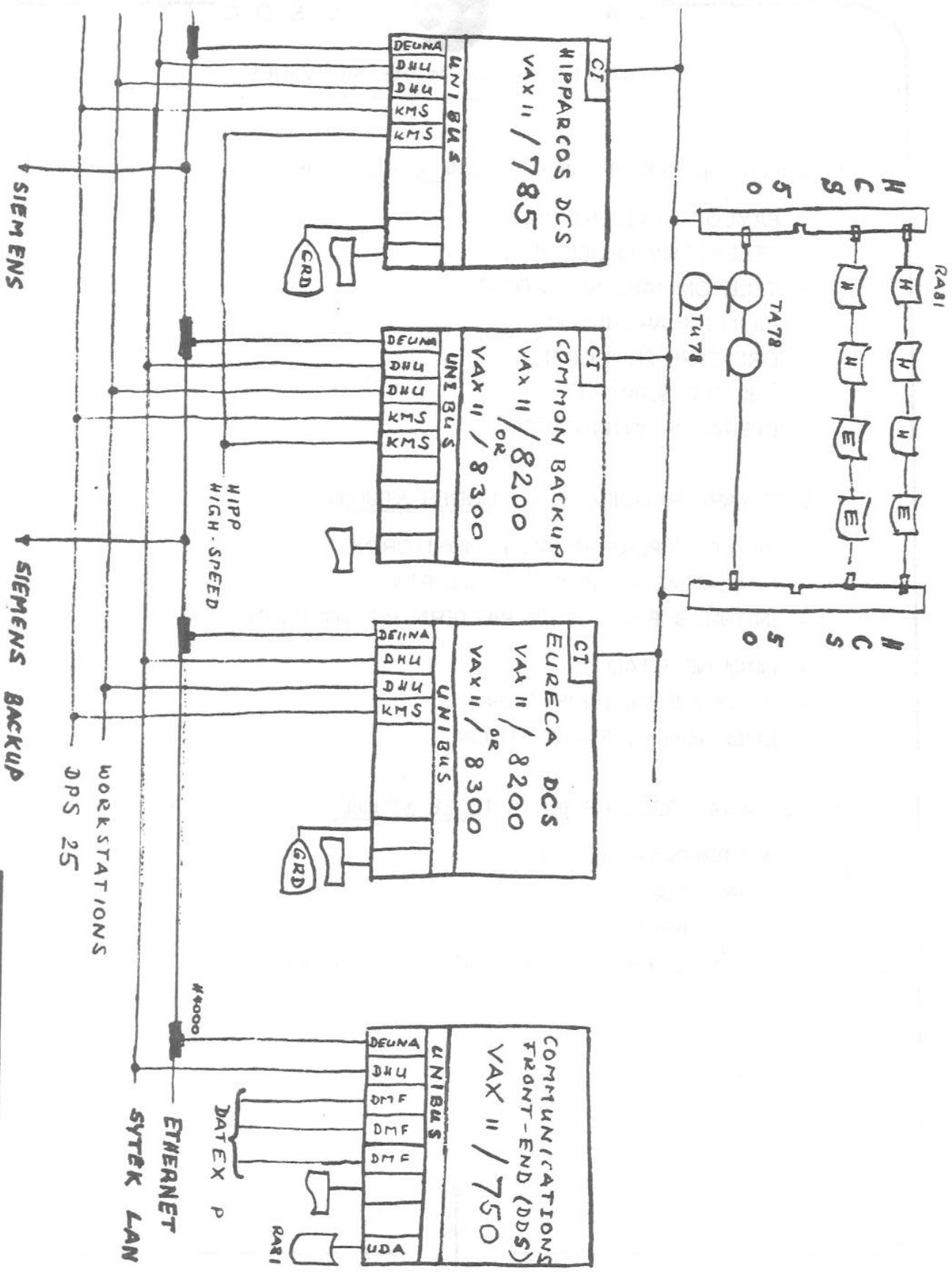
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### COMPUTER CONFIGURATION

#### \* VAX CLUSTER CONFIGURATION:

- VAX 11/785 DEDICATED TO HIPPARCOS
- VAX 11/8200 (or 8300) FOR EURECA
- VAX 11/8200 (or 8300) AS BACKUP  
FOR EITHER HIPPARCOS OR EURECA
- TWO (REDUNDANT) HIERARCHICAL STORAGE  
CONTROLLERS (HSC 50)
- DUAL-PORTED DISC AND TAPE DRIVES
- 3 ONLINE AND 2 BACKUP DISCS OF 456 MBYTES EACH
- 8 MBYTE PHYSICAL MEMORY NEEDED





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## STATUS OF SOFTWARE ACTIVITIES

\* SOFTWARE REQUIREMENTS COMPLETED IN AREAS:

- PAYLOAD CALIBRATIONS
- TELEMETRY PROCESSING
- TELECOMMANDING SUPPORT
- FILING & ARCHIVING
- DRC TAPE PRODUCTION
- OBC/CLE SUPPORT
- OPERATOR INTERFACES

\* SOFTWARE REQUIREMENTS UNDER STUDY:

- PAYLOAD PERFORMANCE MONITORING
- REAL-TIME ATTITUDE MONITORING
- INITIAL & FINAL STAR PATTERN RECOGNITION
- GROUND RTAD
- ATTITUDE INITIALISATION
- EMERGENCY REACQUISITION

\* SOFTWARE REQUIREMENTS TO BE STUDIED:

- PSF PREPARATION
- INCA UPDATES
- LEOP SUPPORT
- ORBIT DETERMINATION & STATIONKEEPING



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## INITIALISATION PHASE STUDIES:

- \* SUN POINTING ACCURACY ASSESSMENT:

- ROUGH CALIBRATION OF:
  - . SAS POINTING BIASES
  - . X, Y GYROS DRIFT RATES
- SIMULATION OF SUN POINTING CONTROL

- \* STAR PATTERN RECOGNITION:

- SIMULATIONS OF ALGORITHM ON BASIS OF:
  - . STAR MAPPER MEASUREMENTS
  - . Z GYRO RATE READINGS
- EXTERNAL MATRA CONTRACT:
  - . ALTERNATIVE APPROACHES
  - . FINAL STAR PATTERN RECOGNITION



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## PERFORMANCE MONITORING

### OBJECTIVES:

- i) QUICK IDENTIFICATION OF PERFORMANCE DEGRADATION DUE TO ONBOARD ANOMALY
- ii) COMPILED LIST OF PERFORMANCE PARAMETERS OVER THE MISSION

### CONSEQUENCES:

- i) INITIATION OF DIAGNOSTIC AND REMEDIAL ACTIVITIES
- ii) BASIS FOR DECISION ON CALIBRATIONS, USE OF REDUNDANT ELEMENTS OR ANALYSIS



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### IDT PERFORMANCE MONITORING TASKS

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- i) EXTRACTION OF IDT SAMPLES FOR SELECTED STARS
- ii) ESTIMATION OF COUNT RATE  $I_0$  AND MODULATION COEFFICIENT  $M_1$
- iii) CALCULATION OF EXPECTED  $I_0$  AND  $M_1$
- iv) DETERMINATION OF BACKGROUND COUNT RATES
- v) COMPILED OF EXPECTED AND OBSERVED COUNT RATES AND MODULATION COEFFICIENT



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### EXTRACTION OF IDT SAMPLES

- \* Reference stars with  $6 \leq B \leq 9$  are selected at random with separation of at least one minute
- \* Downlinked IDT observation reports are scanned for selected stars
- \* Dwell periods over one observation frame are identified
- \* Relevant IDT samples are retrieved from telemetry

### LEAST SQUARE FIT OF OBSERVED IDT COUNTS

- \* Algorithm produces estimates for:

$$I_o' = I_o + I_{BK} : \text{total (observed + background) count rate}$$

$$\left. \begin{matrix} I_o'M_1' \\ I_o'M_2' \end{matrix} \right\} \text{contain first two modulation coefficients}$$

$$\psi_o : \text{phase w.r.t. grid reference}$$

- \* On the basis of a priori value of  $M_1$  :

$$I_{BK} = (1 - M_1'/M_1) I_o'$$

$$I_o = I_o' - I_{BK}$$

$$M_1' = (I_o' M_1') / I_o'$$



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### CALCULATION OF EXPECTED COUNT RATE

- \* Expected count rate  $I_0$  modelled as function of:
  - star's magnitude
  - star's colour
  - position in FOV
- \* Expected reference values for  $M_1'$  and  $I_{BK}$  may not be needed

### COMPILATION OF OBSERVED AND EXPECTED COUNT RATES

- \* Collected data are analysed in batches of about 15 minutes for feedback to operator
- \* Data are categorised according to star magnitude and colour classes
- \* Averages are calculated for batches of 10 stars in each category. If discrepancies exceed preset limits alarms are raised.
- \* Long-term statistics are compiled using daily averages for each star category



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#### STAR MAPPER PERFORMANCE MONITORING TASKS

- i) RETRIEVAL OF  $B_T$  AND  $V_T$  SAMPLES FOR SELECTED STARS
- ii) CALCULATION OF  $B_T$  AND  $V_T$  COUNTS FROM SAMPLES
- iii) CALCULATION OF EXPECTED  $B_T$  AND  $V_T$  COUNTS
- iv) DETERMINATION OF BACKGROUND COUNTS
- v) COMPILEDATION OF PREDICTED AND OBSERVED SM COUNTS



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### CALCULATION OF EXPECTED COUNTS

- \* EXPECTED COUNT RATE IS MODELLED AS FUNCTION OF STAR MAGNITUDE, COLOUR AND SSR'S (FOR EACH OF  $B_T$ ,  $V_T$  CHANNELS)

### COMPILATION OF OBSERVED AND EXPECTED COUNTS

- \* AVERAGES OF OBSERVED COUNT RATES AND BACKGROUND COUNT RATES ARE COMPILED FOR EACH BATCH OF STARS
- \* RESULTS ARE CATEGORISED ACCORDING TO  $B_T$  OR  $V_T$ ; INCLINED OR VERTICAL SLITS; MAGNITUDE
- \* IF DISCREPANCIES EXCEED PRESET THRESHOLDS ALARMS ARE RAISED
- \* LONG-TERM STATISTICS ARE COMPILED BY COLLECTING DAILY AVERAGES FOR EACH CATEGORY



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### CALIBRATION STATUS

- \* FIRST ISSUE OF SOFTWARE REQUIREMENTS COMPLETED
- \* ARCHITECTURAL DESIGN UNTIL SEPTEMBER 86
- \* START OF SINGLE TESTS: JAN 87
- \* START OF INTEGRATED TESTS: JAN 88

### UNDER STUDY

- \* EXACT TASK DISTRIBUTION  
DRC'S - ESOC
- \* DATA INTERFACES  
DRC'S - ESOC

