

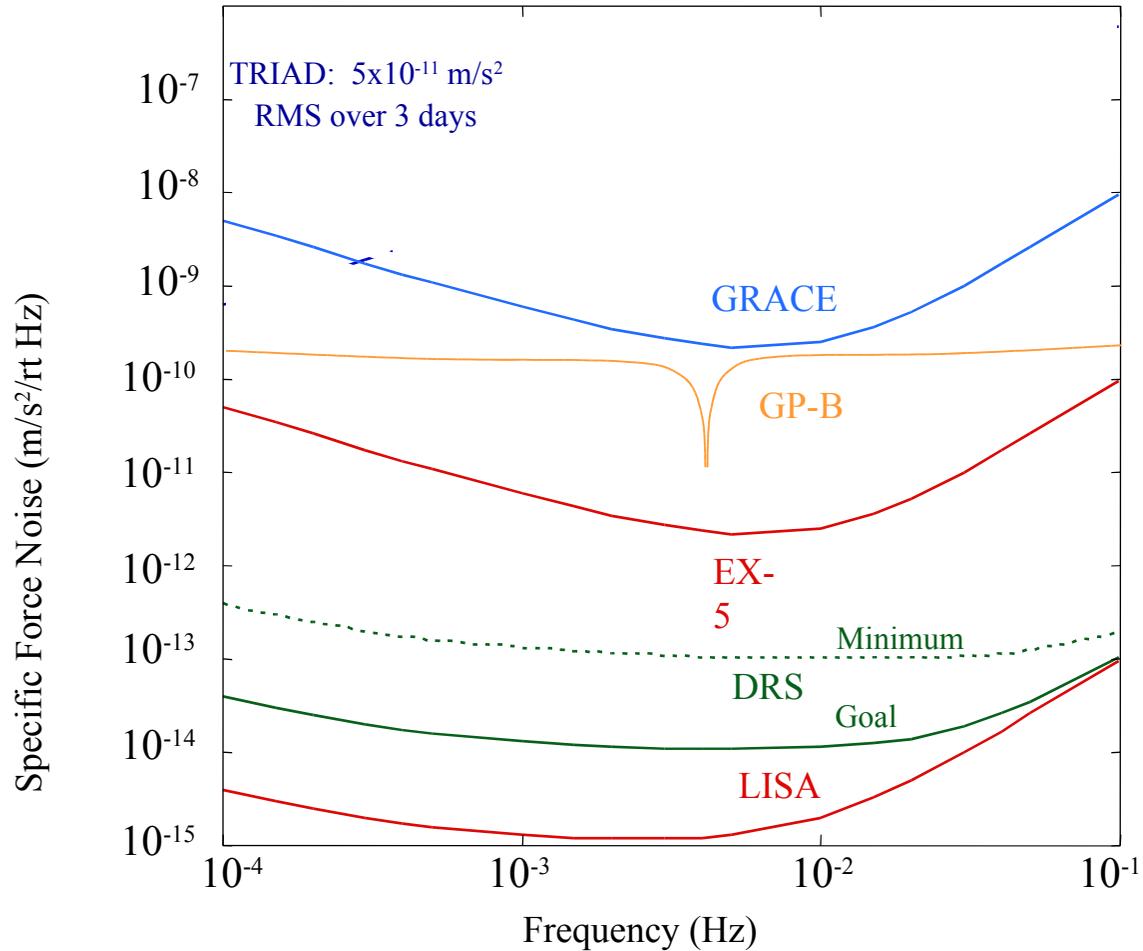
The Stanford Gravitational Reference Sensor

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Mission Drag-Free Requirements



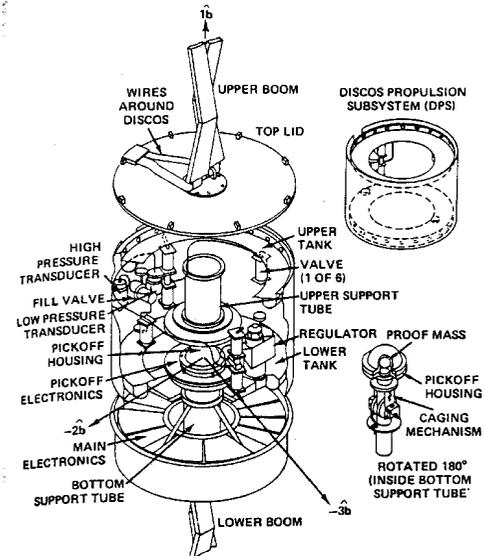
Heritage

- Inertial Sensor based on Stanford experience:

TRIAD (Stanford/APL, 1972)

GP-B (Stanford, 2004)

- Earlier sensors used spherical test masses
 - Fewer degrees of freedom to control**
- Proposed LISA sensor uses a faceted test mass
 - Control position of laser beam on test mass**
 - Allows validation at picometer level**
- Test mass is 4-cm cube of Au/Pt alloy
 - Dense, to reduce motion in response to forces**
 - Low magnetic susceptibility, used on TRIAD**
- Position sensing and charge management design derived from GP-B



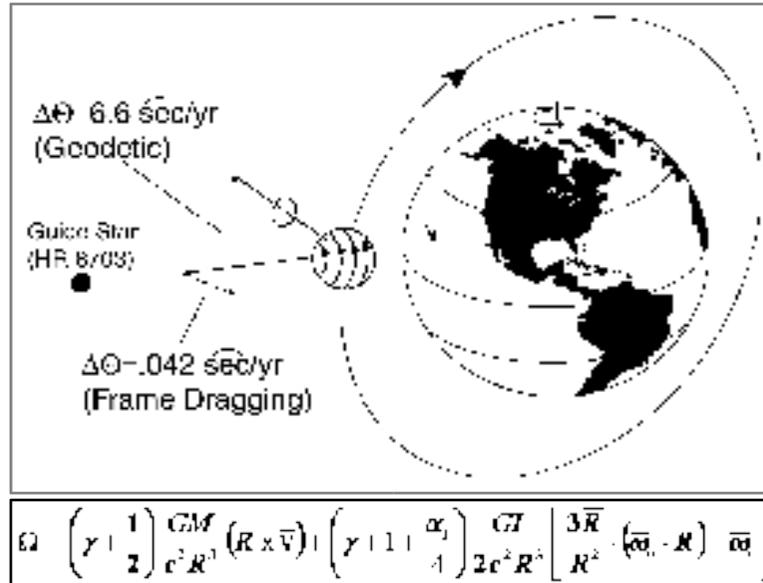
TRIAD sensor- 1972



GP-B Flight Gyroscope



GP-B Launch: April 20, 2004



GP-B Technologies

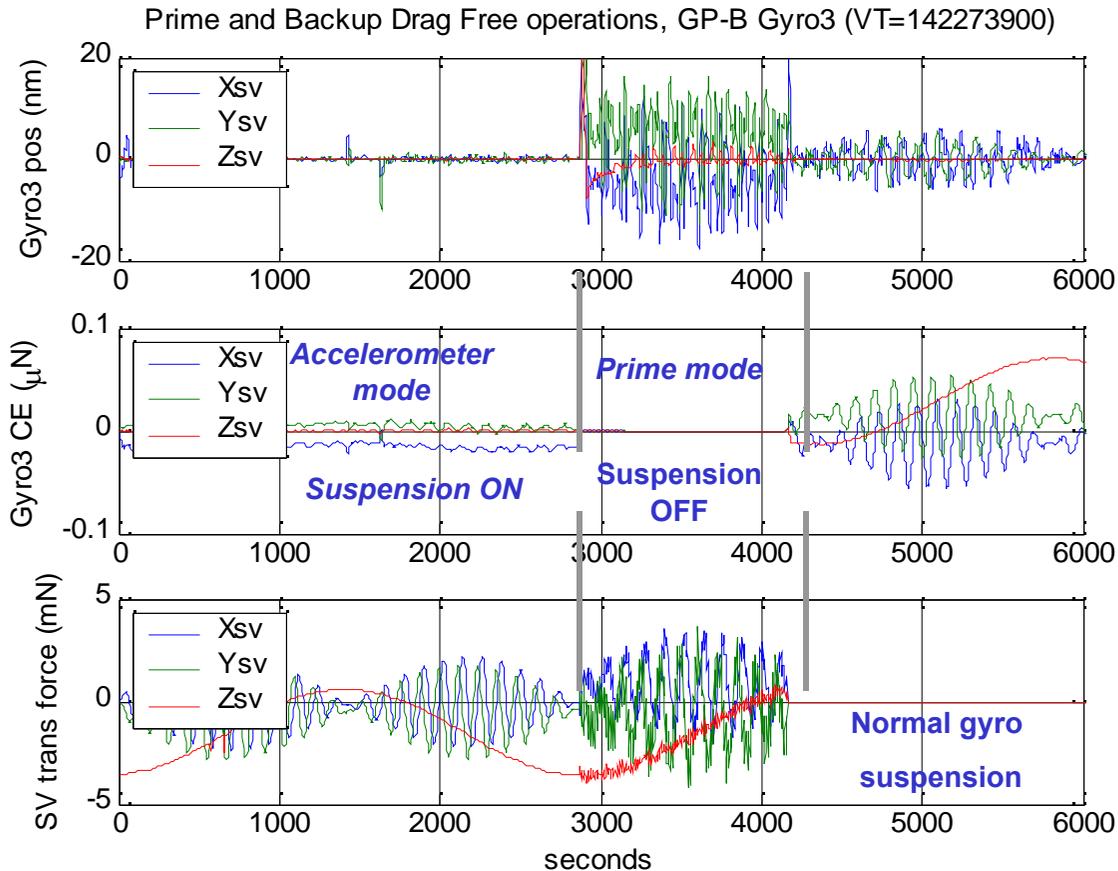
30 years of GRS technology development for TRIAD and GP-B are a very significant stepping stone.

GP-B has showed on-orbit validation of key GRS technologies.

- Drag-free Control — 10^{-10} m/s² level
- Electrostatic Positioning System — 0.45 nm rms position noise
- Charge Control System — < 5pC control



Drag Free Performance



Positioning performance

Drag-free: 5.0 nm RMS

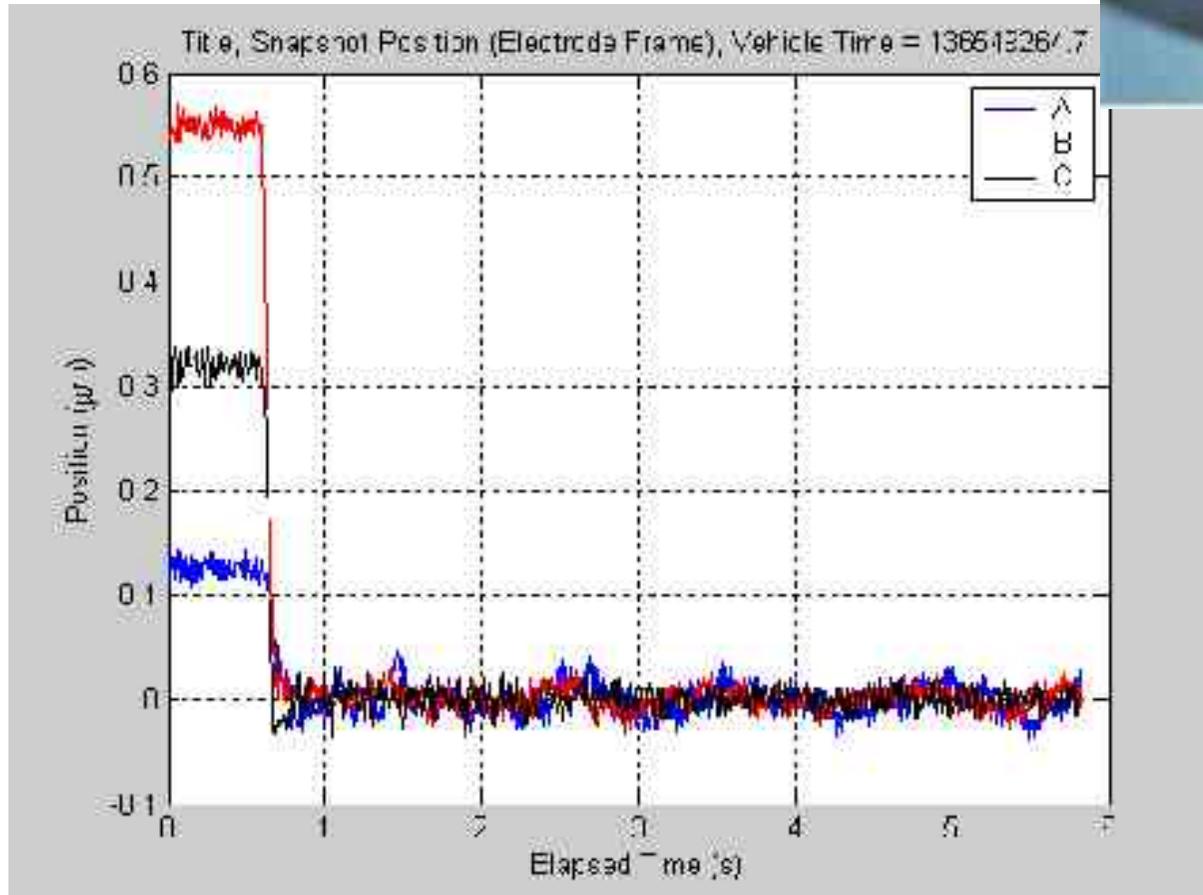
Backup drag-free: 0.6 nm RMS

Normal suspension: 6 nm peak from gravity gradient.

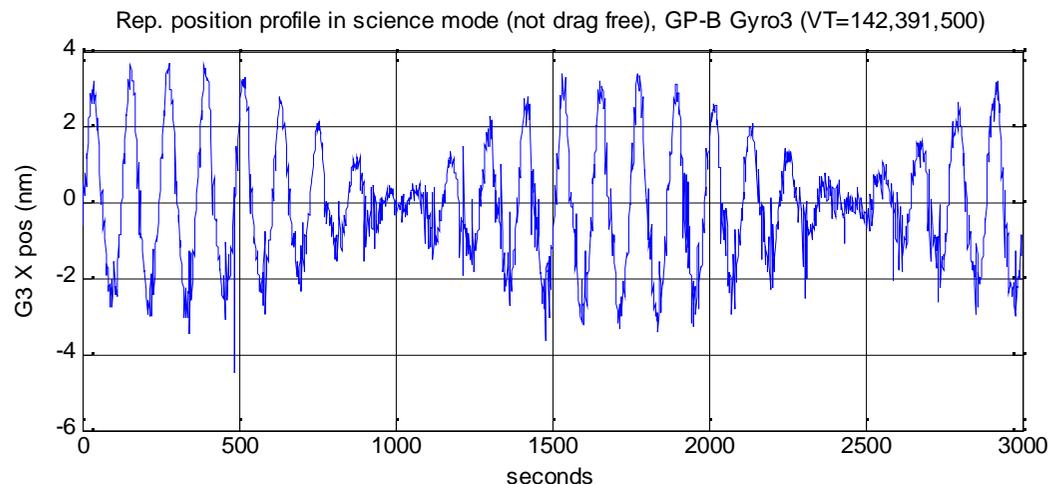


GP-B Gyroscope Suspension

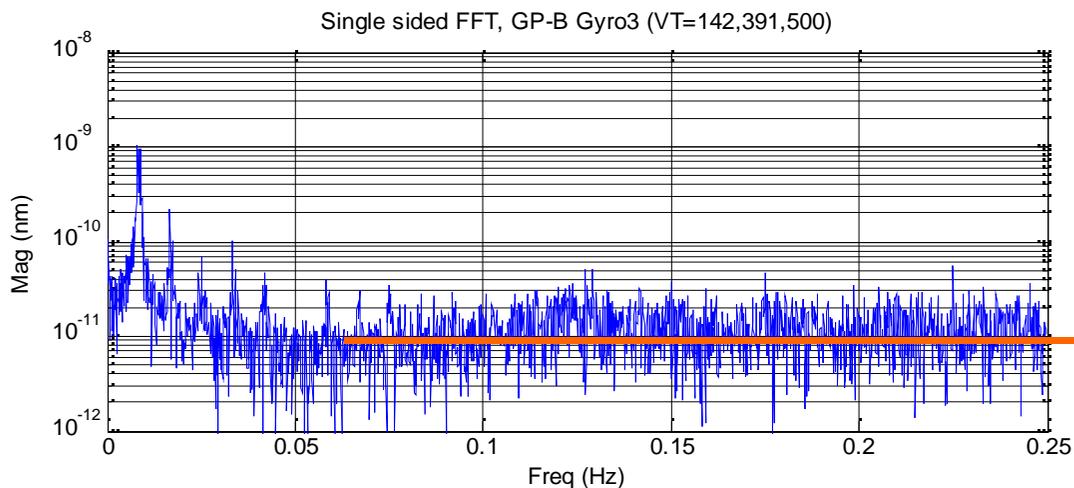
Gyro #4 Digital Levitation



Position Measurement Performance



Representative gyro position trace showing non drag-free gravity gradient effects in Science Mission Mode



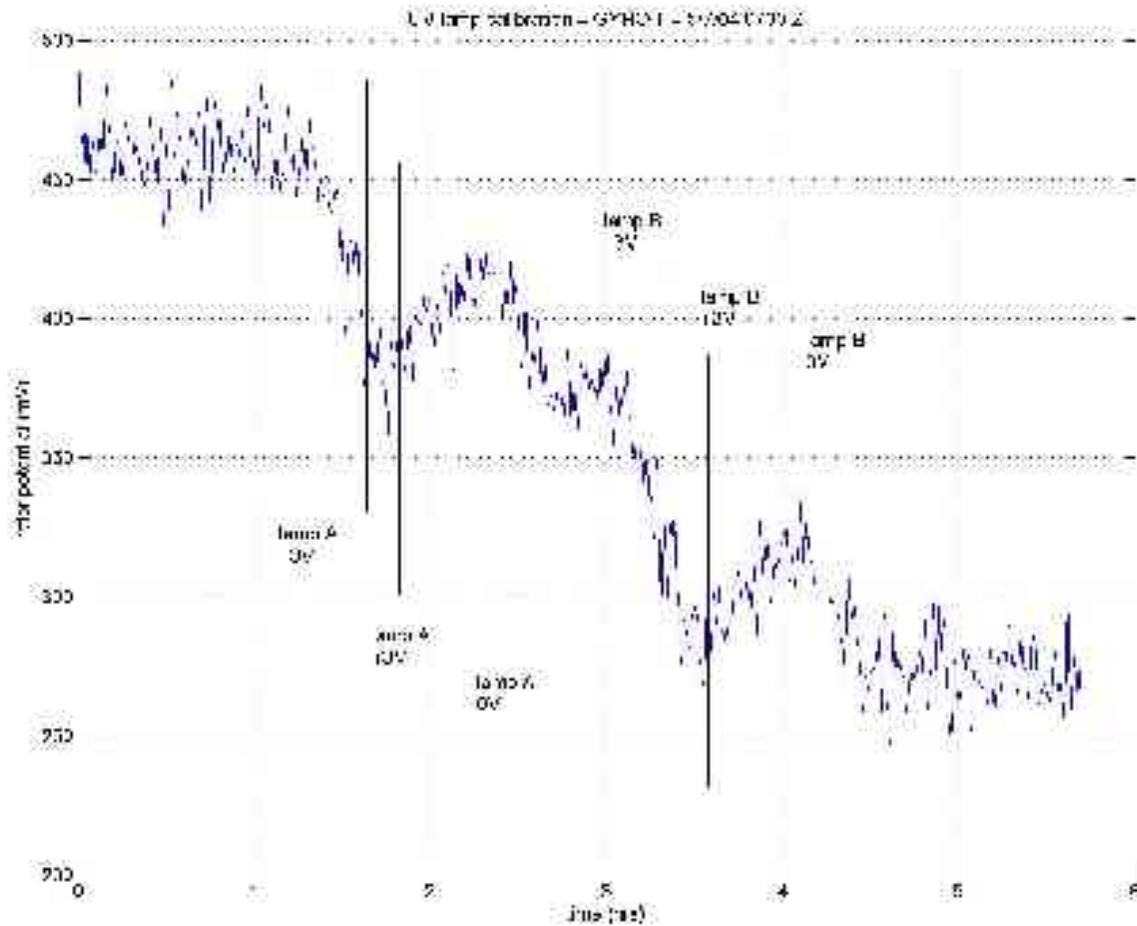
Measurement noise 0.45 nm rms

Noise floor



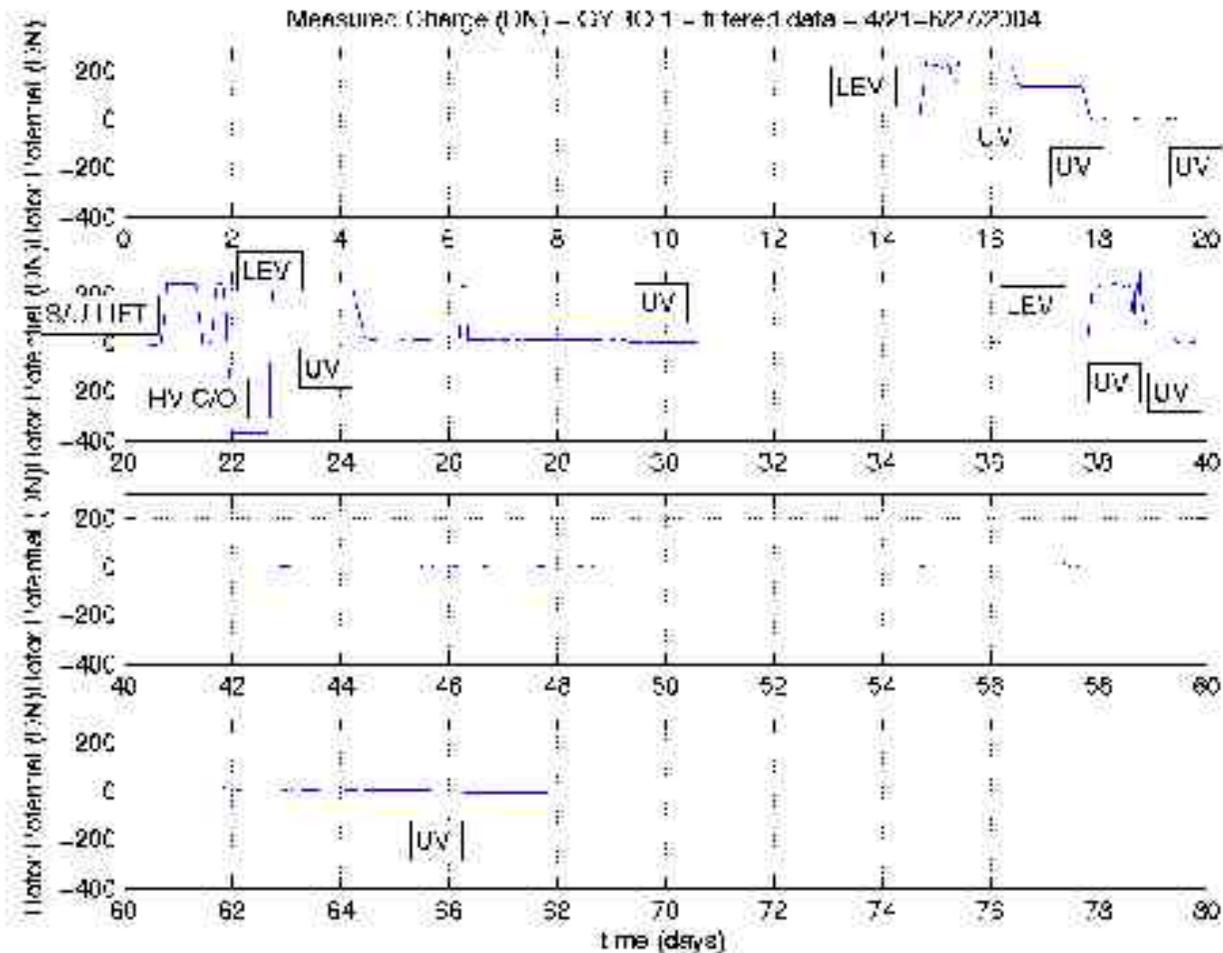
GP-B Charge Management

Gyro #1 UV System Calibration



GP-B Charge Management

Gyro #1 Charge Control (mV)



GRS Overview

Salient Features

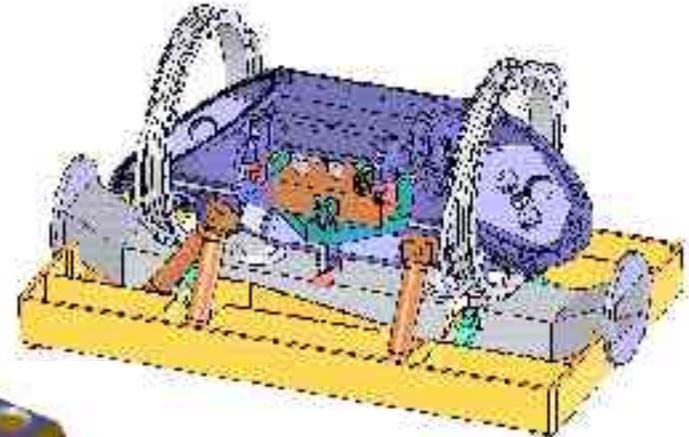
- Test mass noise $< 2.8 \times 10^{-14} \text{ m/s}^2/\sqrt{\text{Hz}}$, 1 mHz to 30 mHz
- Position measurement to $< 3 \text{ nm}/\sqrt{\text{Hz}}$, 1 mHz to 30 mHz
- Accelerometer mode
- Validation of thruster performance
- Force noise diagnostics
- Validation of drag free environment models

Gravitational Reference Sensor Technologies

- Test mass is 4-cm cube of Au coated Au/Pt alloy
- Beryllia housing with plated Au electrodes
- Vacuum system supporting 10^{-5} Pa EOL
- Caging system capable of supporting launch loads and re-caging
- Capacitive sensing system providing $< 3 \text{ nm}/\sqrt{\text{Hz}}$ measurement
- Electrostatic forcing system providing $2 \times 10^{-7} \text{ m/s}^2$ peak acceleration



DRS chassis and interferometer



BeO Housing



GRS Test Mass
Prototype



Precision Reference Housing

- Electrode isolation groove
BeO sample end-milled at
Axsys.
- Stepped Precision Alignment
BeO Walls.
- Bulk Precision Alignment
Alumina Reference Walls.
- Precision tooling sphere
demonstrated.
- 7 EM BeO housing walls
received 3 weeks early.
- Alignment performance
verified in test.
- Laser milling demonstrated.
- All 72 flight BeO blanks
delivered by Brush Wellman
on schedule.



Kelvin Probe Measurements at GSFC: Contact Potential Difference Variations

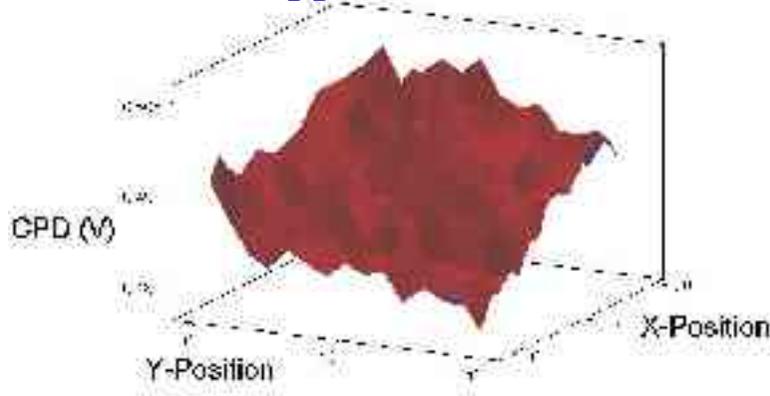
Two coatings studied: gold (Au) and diamond like carbon (DLC), to avoid cold welding when caging

3 mm probe used, 1cm x 1cm area studied

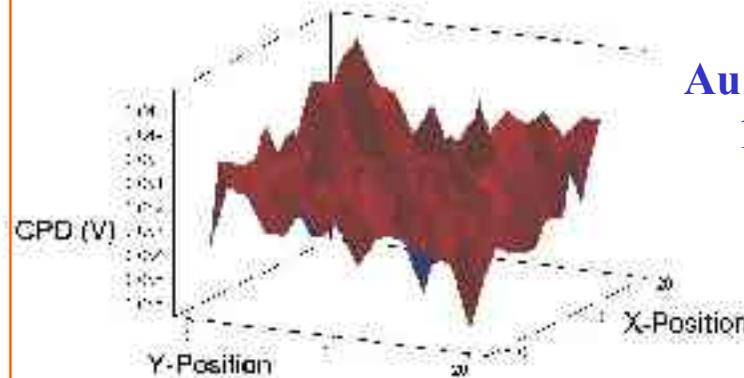
Conclusions:

- DLC essentially as good as Au
- Both meet requirements

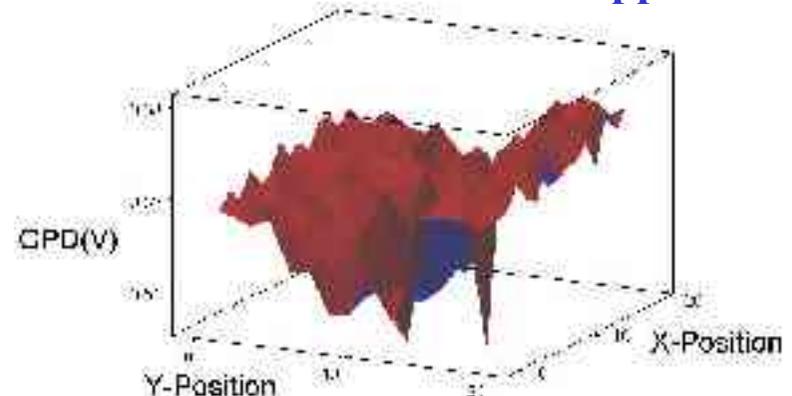
DLC/Au/BeO
20 mV pp



Au on Alumina
10 mV pp



DLC/Au/Ti
20 mV pp

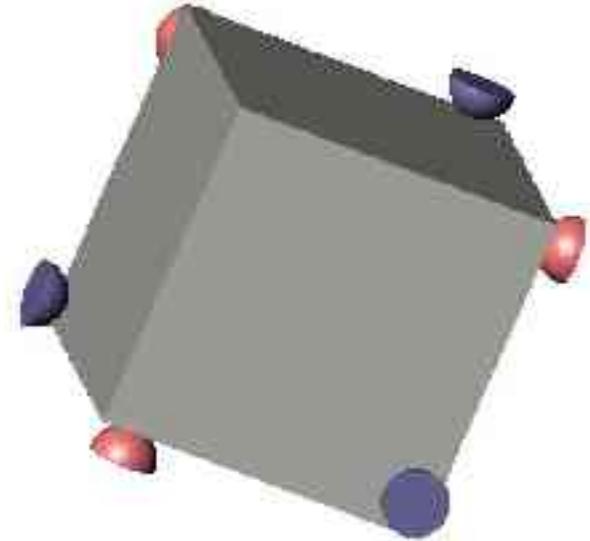


data taken in collaboration with Jordan
Camp and John Blackwood, GSFC



Caging Design

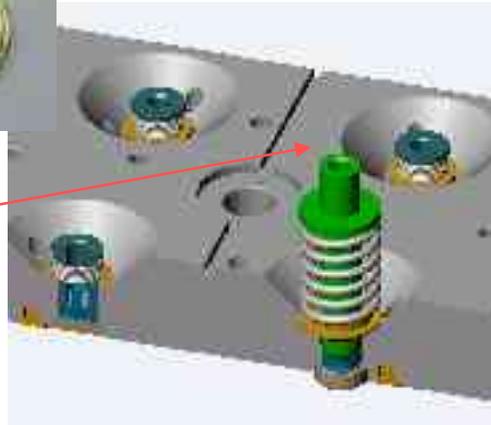
- Test mass constrained by 6 travel-limited push actuators.
- Travel overlap = 0.1mm.
- Static loads taken by 3 pads + pneumatic pressure.
- Dynamic loads taken by all pads and actuator stiffness.
- Pads pivot to self-align to TM face.
- Actuators powered by central pressure supply
- Plungers normally retracted, retracted 0.1mm into housing wall



- Pads mimic wall properties: BeO, gold and DLC coatings.
- Pads are self aligning
- Pad diameter is 5mm
- Return spring provides uncaging force > 10N



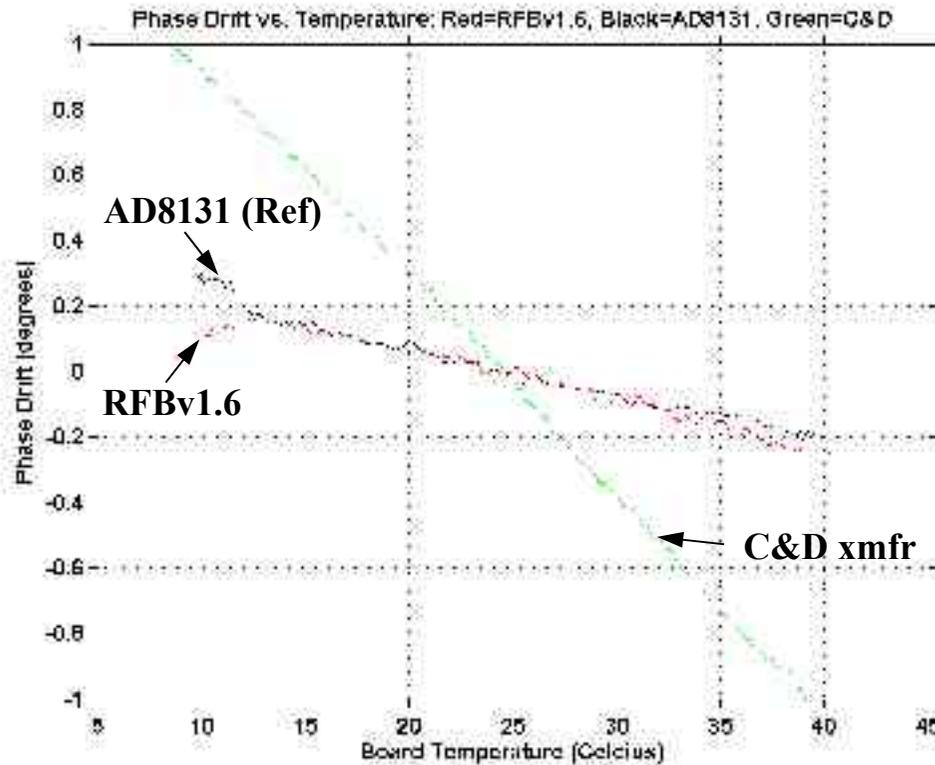
plunger unit: sits on top of pad unit



Analog Electronics Testing

Eight RFB 1.6 boards populated and under test

- No PCB defects
- All analog circuits functioning as expected
- Firmware complete and digital interface tested



RFBv1.6 differential output driver testing shows phase temperature coefficient performance equivalent to the best commercial balanced drivers (e.g. AD8131).



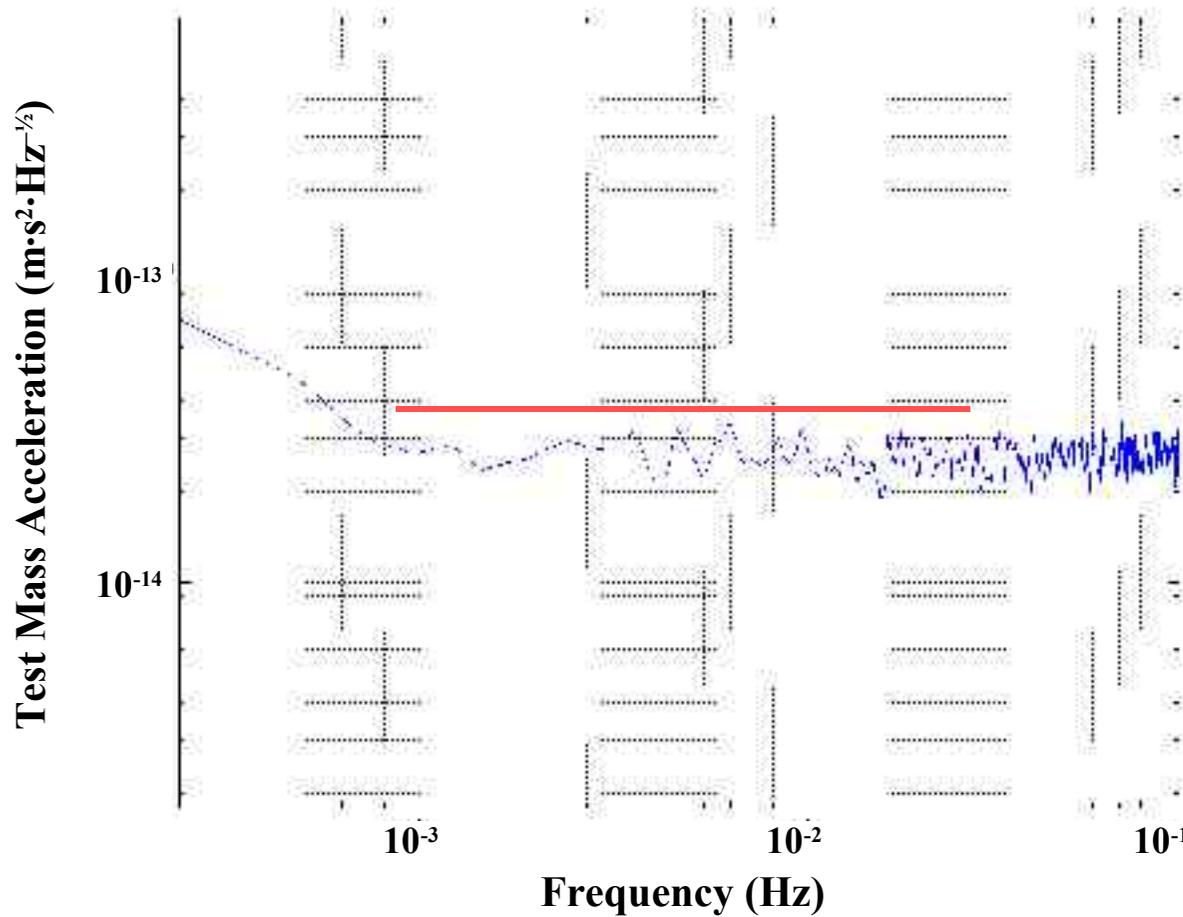
Noise Budget

Source	Requirement ($10^{-15} \text{ m}\cdot\text{s}^{-2}\cdot\text{Hz}^{-1/2}$)	CBE ($10^{-15} \text{ m}\cdot\text{s}^{-2}\cdot\text{Hz}^{-1/2}$)
Coupled Spacecraft Motion (Sensitive)	14	14
Coupled Spacecraft Motion (Transverse)	3.8	3.8
Coupled Spacecraft Motion (Orientation)	4.5	4.5
ES Suspension – Backaction	10	10
Dielectric Effect	2.2	2.2
Test Mass Charge Variation	10	10
Lorentz Force	1.0	1.0
Magnetic Field Interactions	2.7	5.4
Housing Temperature Gradient	4.0	4.0
Residual Gas Pressure Damping	4.5	4.5
Interferometer Laser Pressure Variation	0.5	2.6
Time Varying Mass Attraction	10	10
Low Frequency Suspension Force	4.5	4.5
Control Force Cross-talk	2.3	2.3
Total Acceleration Noise	24.8	25.2
<i>GRS System Margin</i>	<i>13.0</i>	<i>12.1</i>
Level 3 Requirement	28	28

CBE =
current best
estimate

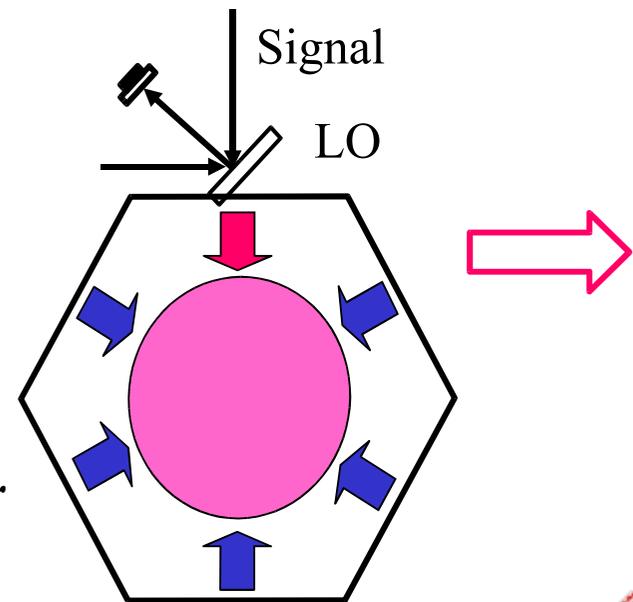


GRS Performance Simulation Results



Advanced Concepts - Stanford

- Single proof mass (PM) per S/C
- Non constraint GRS
- Multiple stage disturbance isolation
- Gravitational sensor separation from S/C Interferometry
 - Measure PM position in housing
 - Use housing for interferometry
- Fiber utilization
- Reflective Optics



GRS with double sided grating for PM and interferometer reference



GRS Path to Flight

April, 2003	GRS Established Technology Readiness Level 5
May, 2004	GRS Subsystem Critical Design Reviews
August, 2004	DRS Critical Design Review
May, 2005	GRS Delivered to JPL
January, 2006	DRS Delivered to ESA
May, 2008	LAUNCH

