

The ST7 Interferometer

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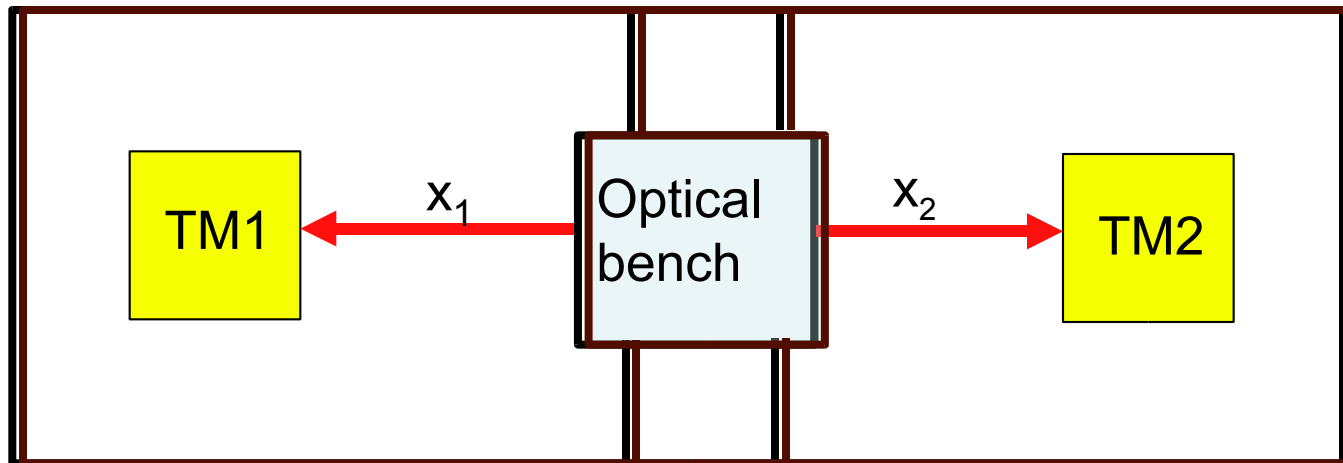
Jet Propulsion Laboratory
California Institute of Technology



ST7 Concept



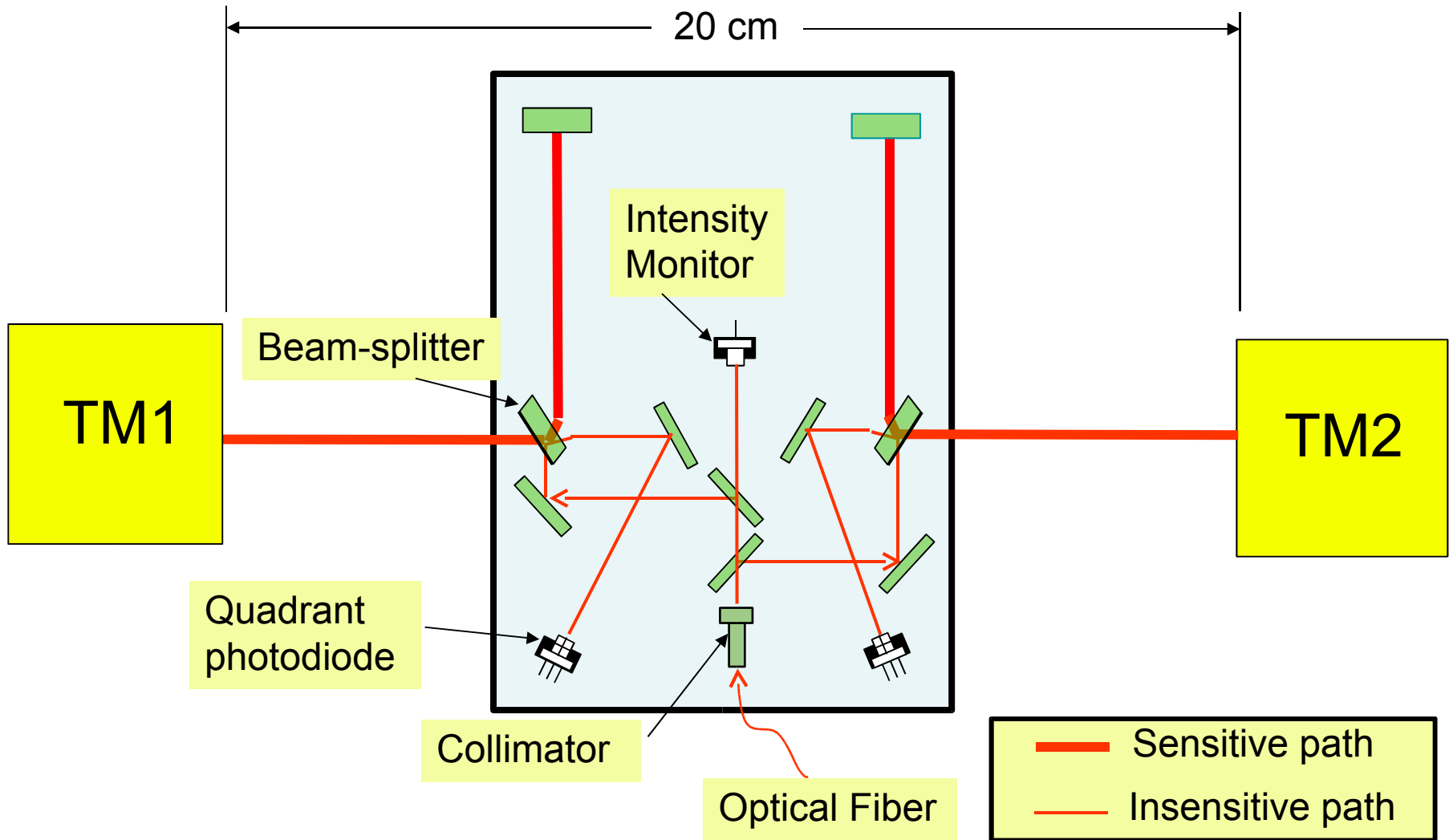
- Measure suspended masses within spacecraft
- Test thruster performance in drag-free control
- Hitch ride on LISA Pathfinder



- Interferometer optical bench fixed to spacecraft
- x_1 and x_2 measured separately; $x_1 + x_2$ is low-noise



Optical Bench





Interferometer Features



Beam diameter 1 mm, Rayleigh range 70 cm, sensitive path lengths 10 cm.

No modulators, phasemeters, intensity stabilization, or frequency stabilization.

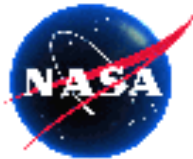
Requires test mass to be positioned near mid-fringe.

Intensity monitored, noise removed in data analysis.

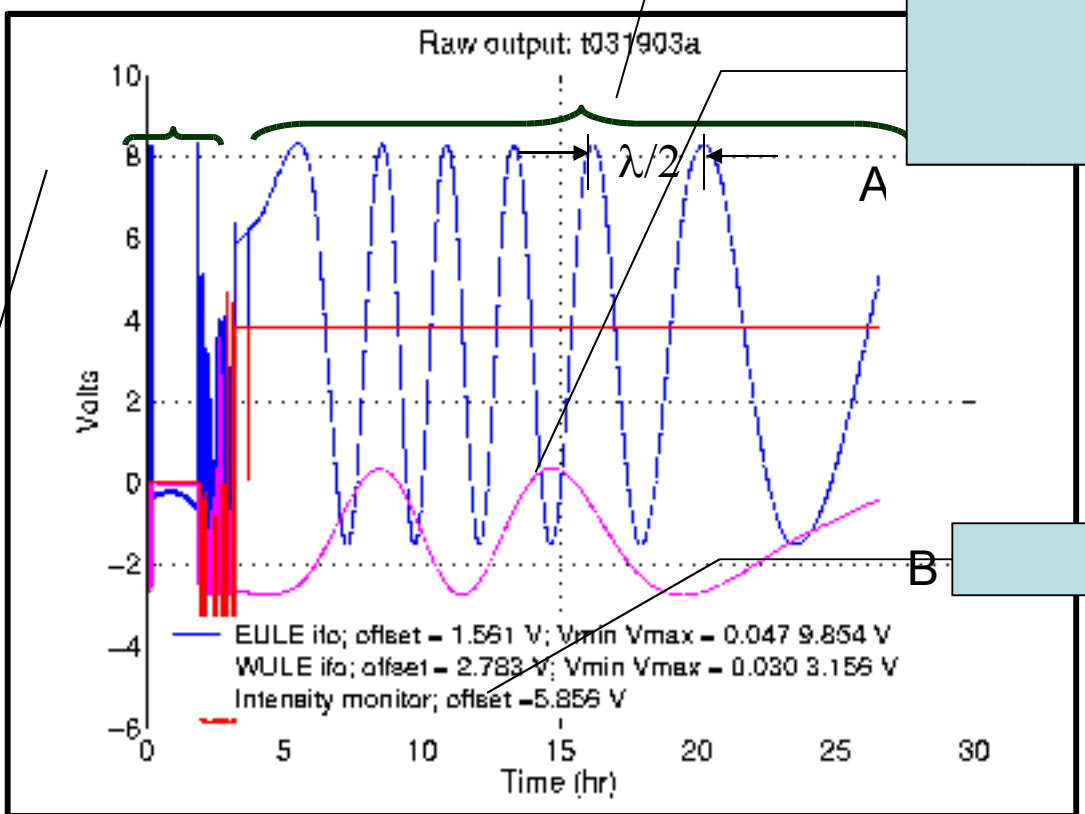
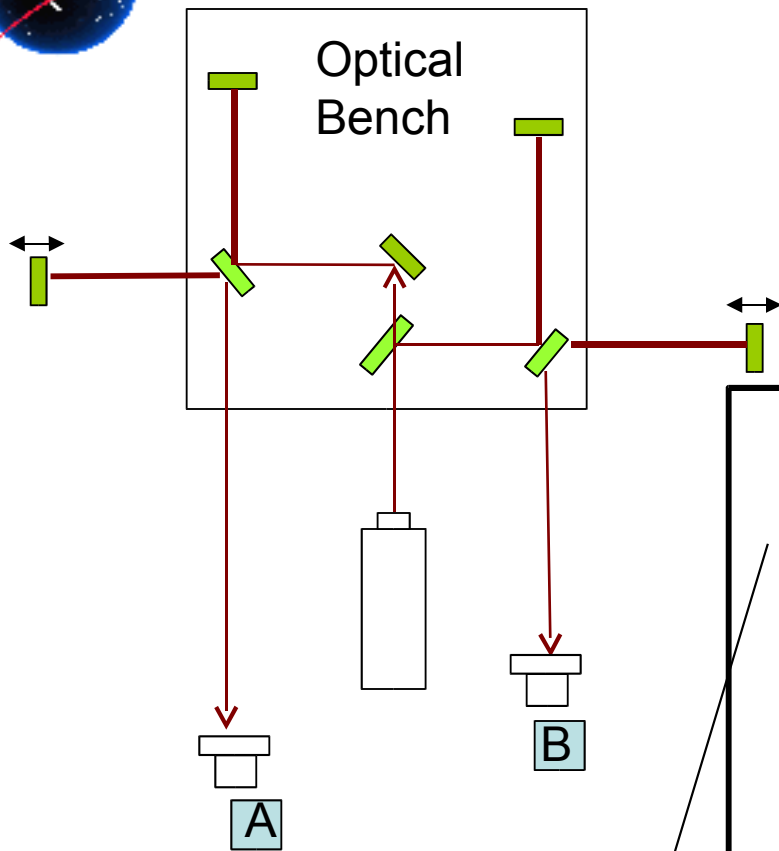
Separate measurements of both bench/test-mass distances.

Quadrant photodiodes monitor total fringe signal, and two axes of alignment.

Automatic alignment, autonomous operation.



Homodyne Signal

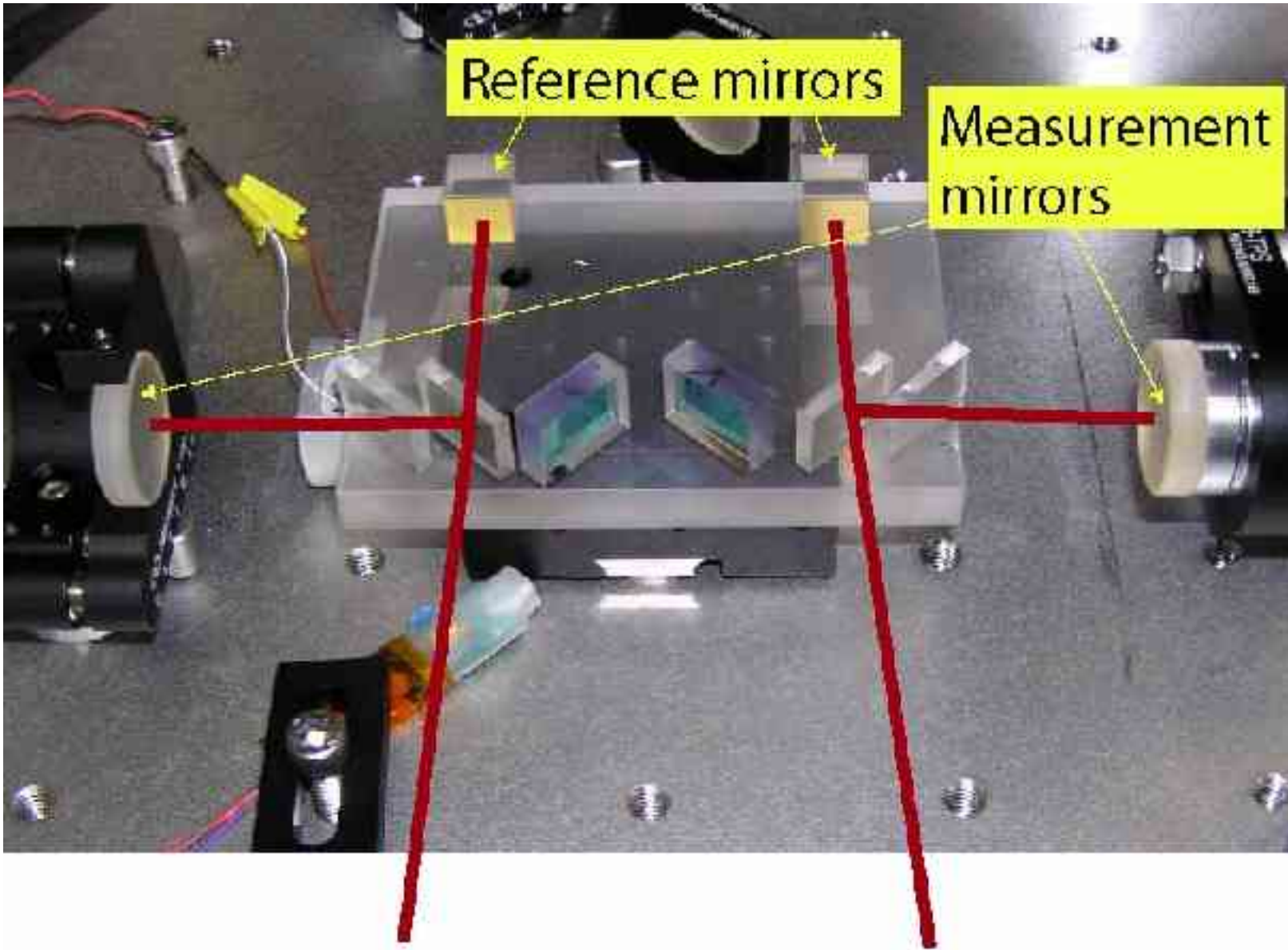


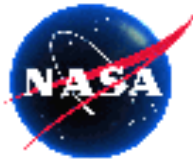
Manual Alignment

Thermal Expansion

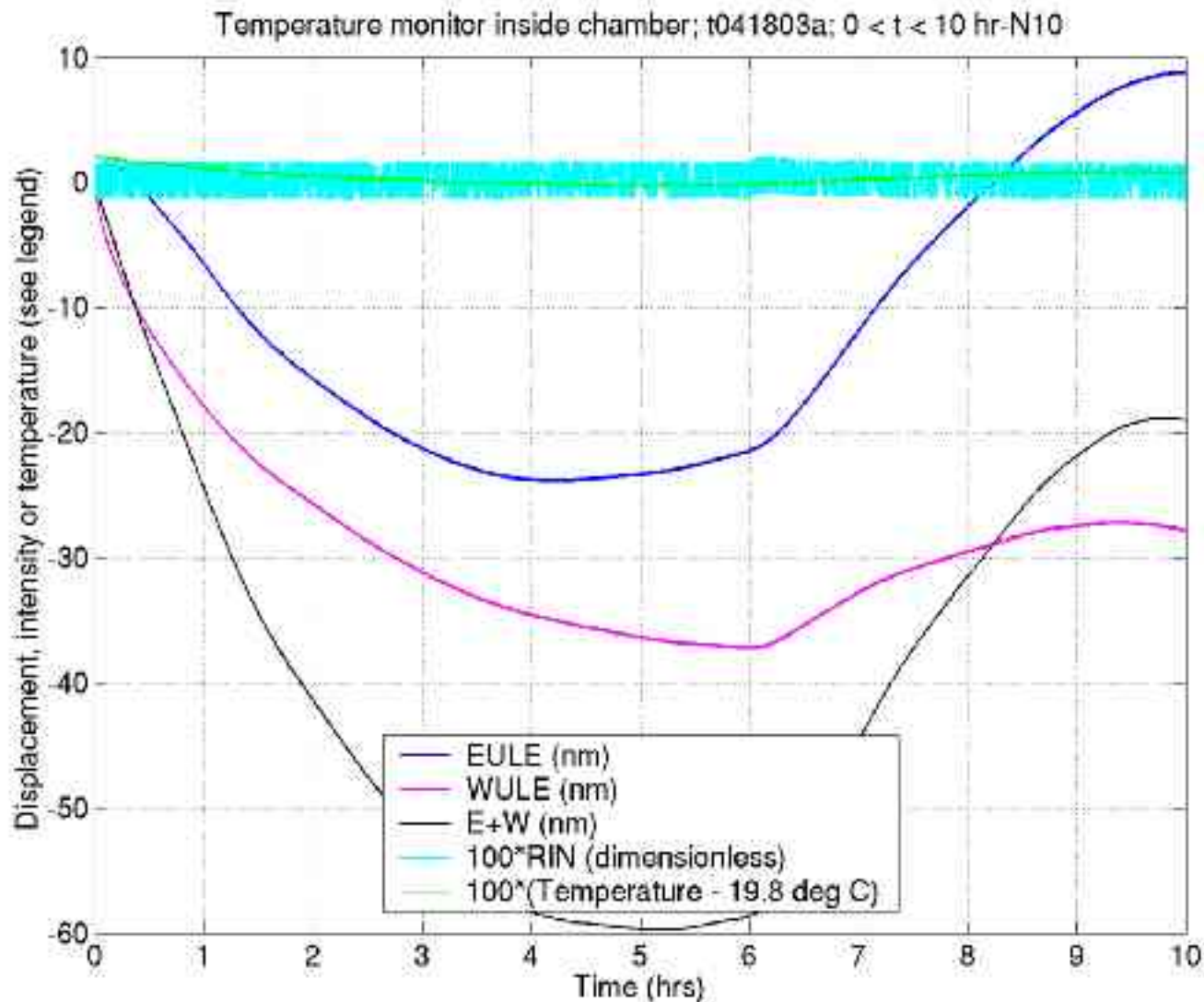


Contacted Optics in Vacuum Chamber



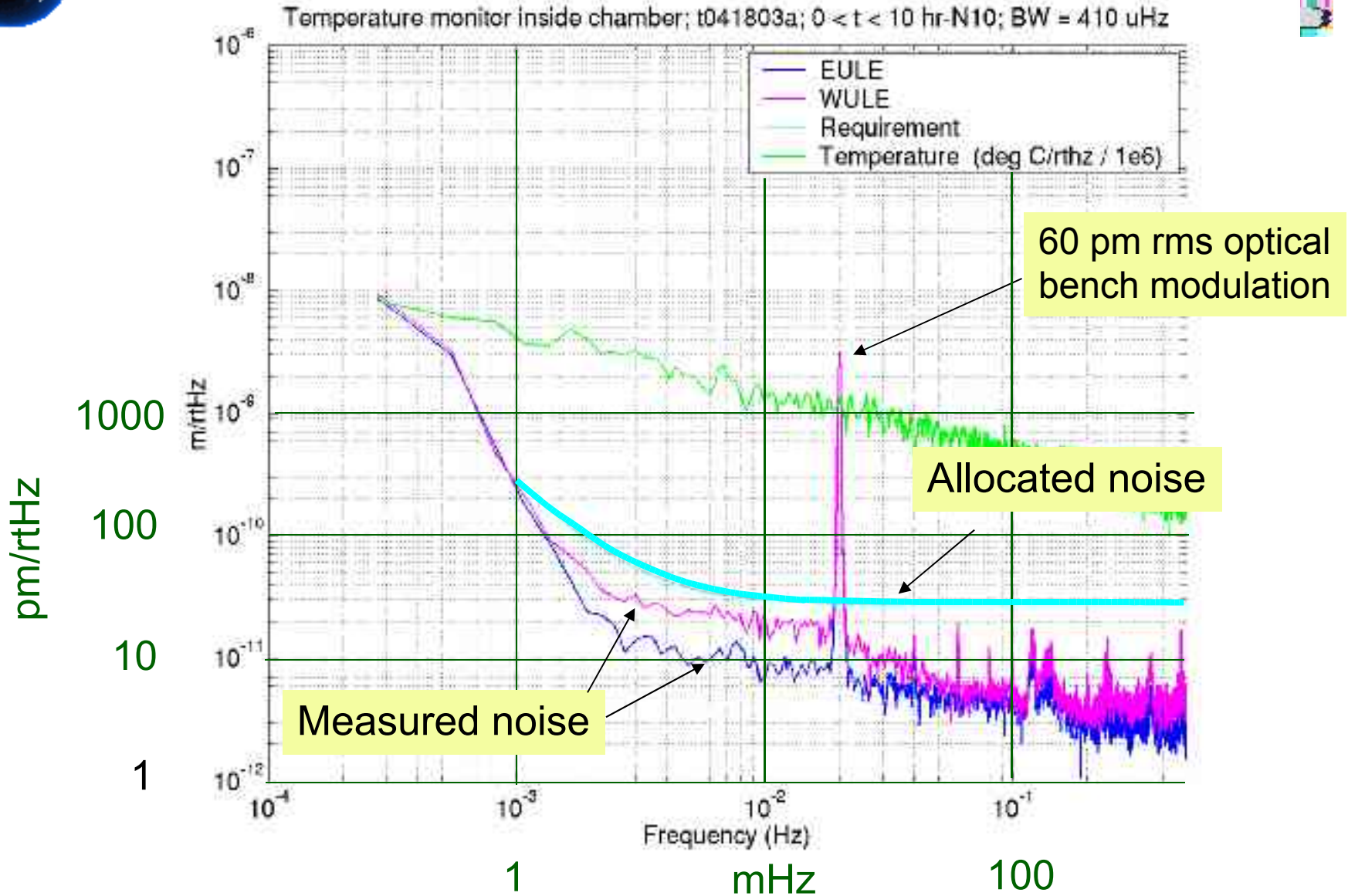


Testbed Drift





Testbed Noise

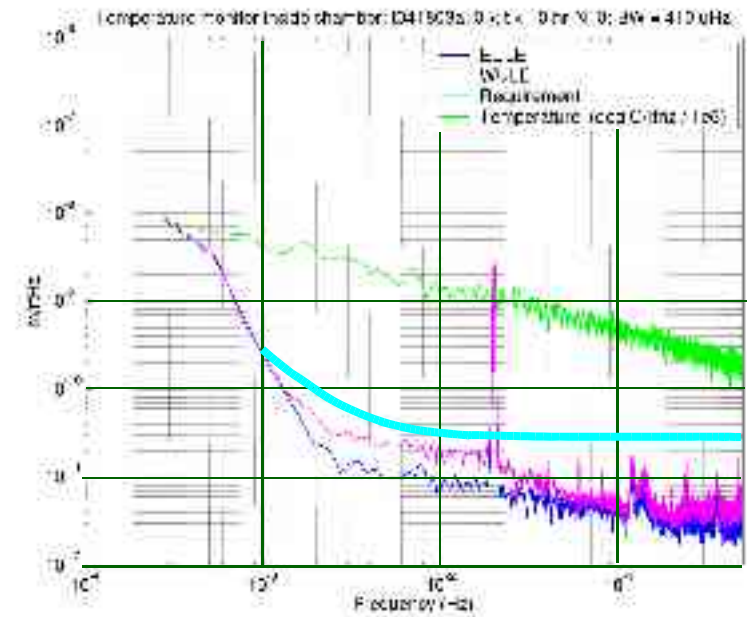




Measurements Demonstrate:

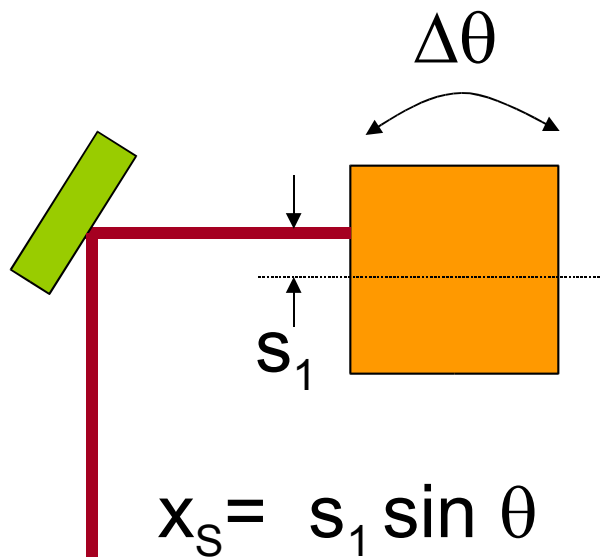


1. Analog electronics and ADC noise adequately low
2. Thermal sensitivity probably adequately low
3. Bench motion suppression typically x200, without calibration (x1000 needed)
4. Frequency stabilization not needed
5. Intensity noise can be suppressed in data analysis



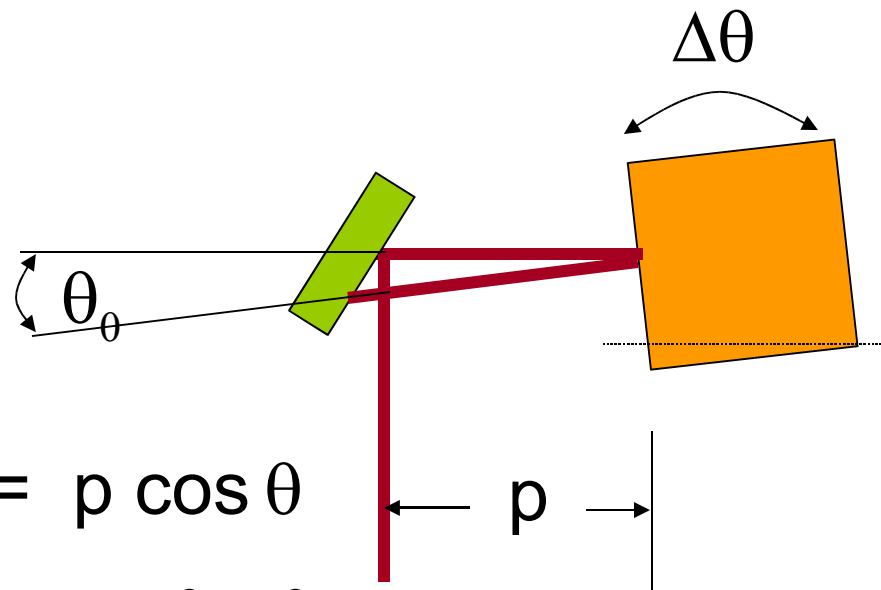


Alignment Sensitivity 1: Geometric error



$$x_s = s_1 \sin \theta$$

$$\Delta x_s = s_1 \Delta \theta$$



$$x_c = p \cos \theta$$

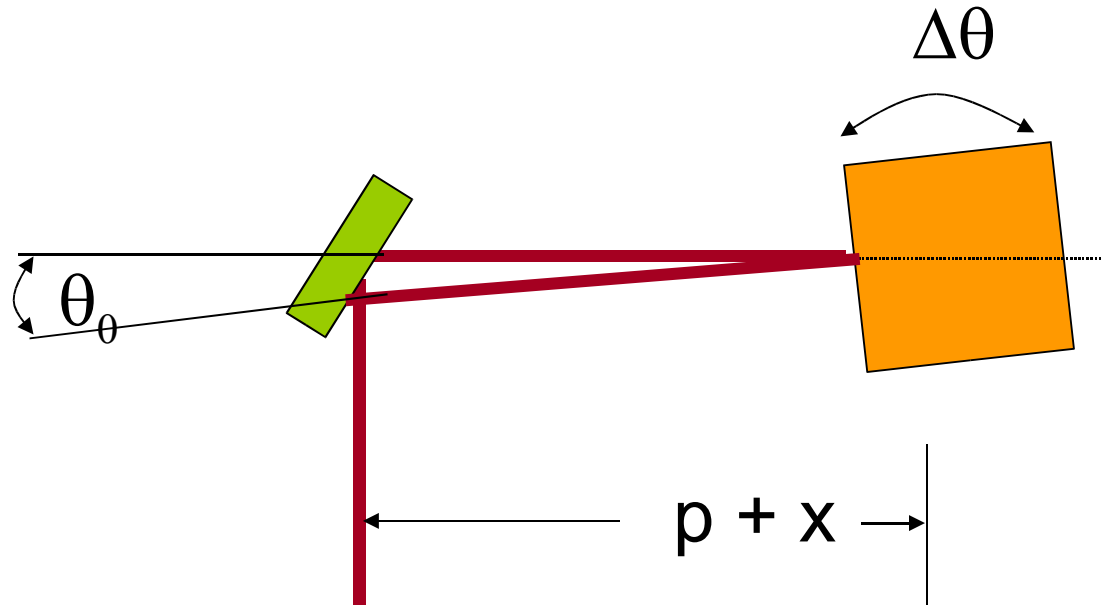
$$\Delta x_c = p \theta_0 \Delta \theta$$

$$s_1 = 40 \mu; p = 10 \text{ cm}; \theta_0 = 400 \mu\text{rad}$$

Errors are correlated, and of same order: $s_1 \sim p \theta_0$



Alignment Sensitivity 2: Fringe position error

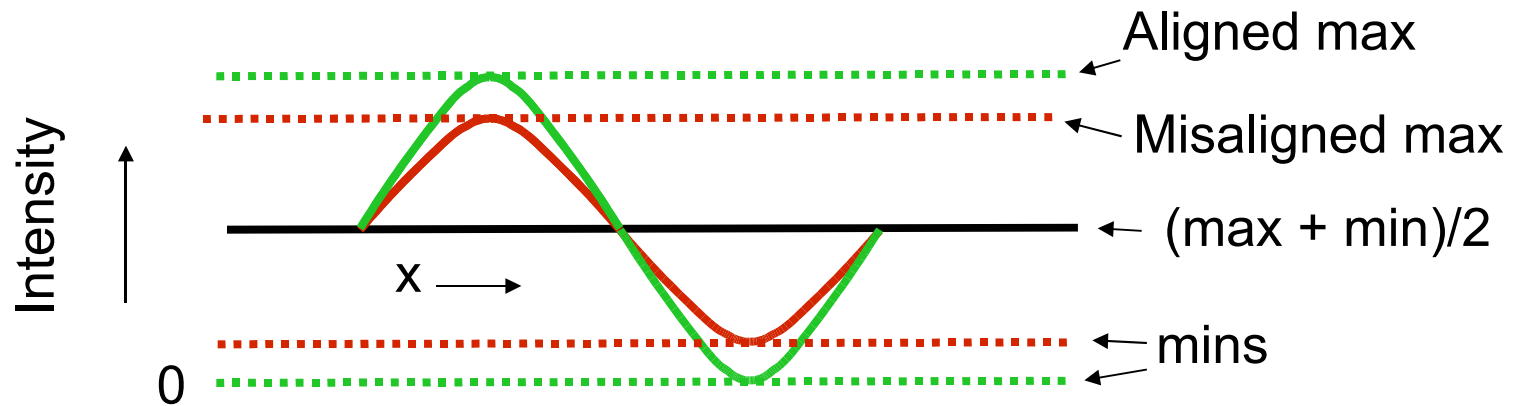


$$\Delta x_x = \alpha x \theta_0 \Delta\theta,$$
$$\alpha = (\pi w / \lambda)^2 = 2.2 \times 10^6,$$

$w = \text{beam radius}$



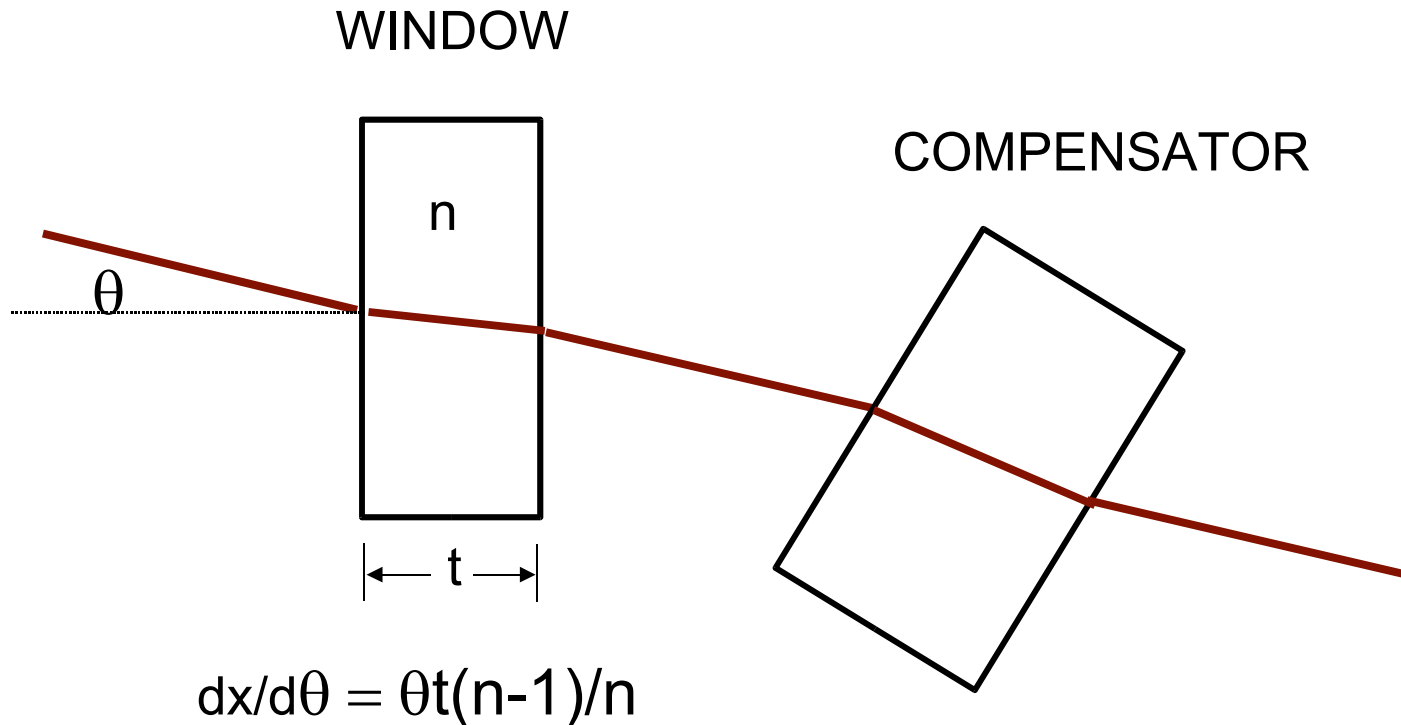
Alignment Sensitivity 3: Half-intensity operating point



At the $x = 0$ half-intensity operating point, detected intensity is independent of alignment θ .



Alignment Sensitivity 4: Refraction through window



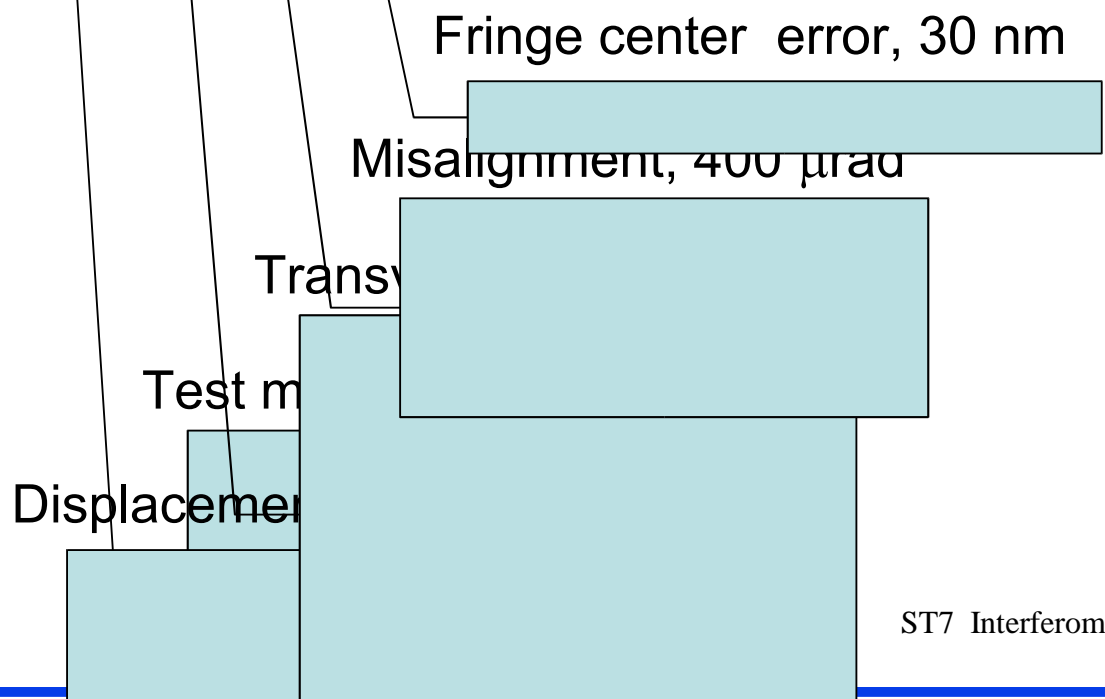
- Window tilted by ~ 2 deg to avoid spurious interferometer
- Compensator thickness and angle adjusted to cancel $dx/d\theta$



Total angle-jitter noise



$$\frac{dx}{d\theta} \approx h + \theta [\alpha x - p]$$
$$\tilde{x}(f) \approx \tilde{\theta}(f) (h + \theta [\alpha x - p])$$

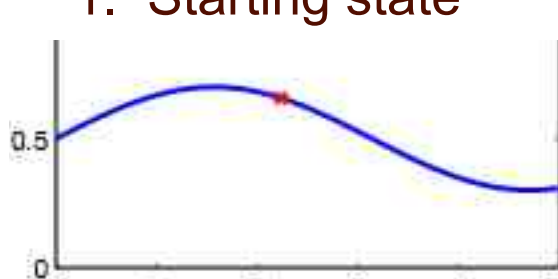




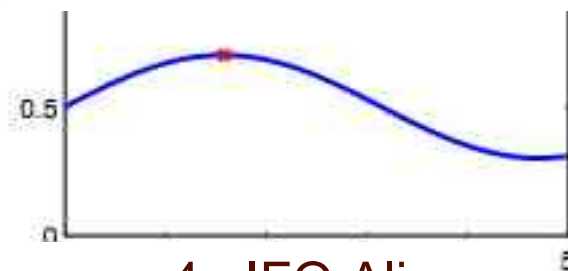
Initialization



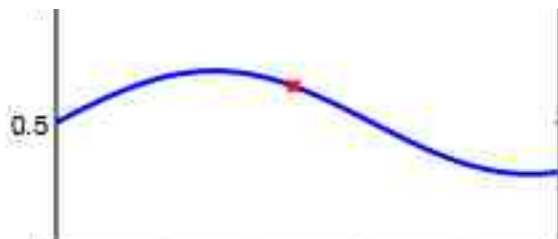
1. Starting state



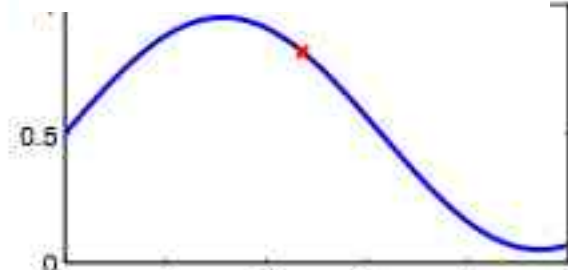
2. IFO finds bright fringe



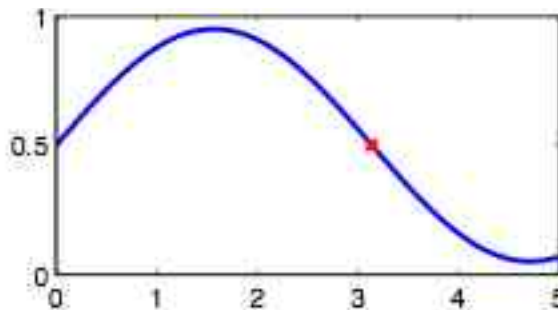
3. GRS moves to quarter fringe



4. IFO Aligns



5. GRS to half fringe

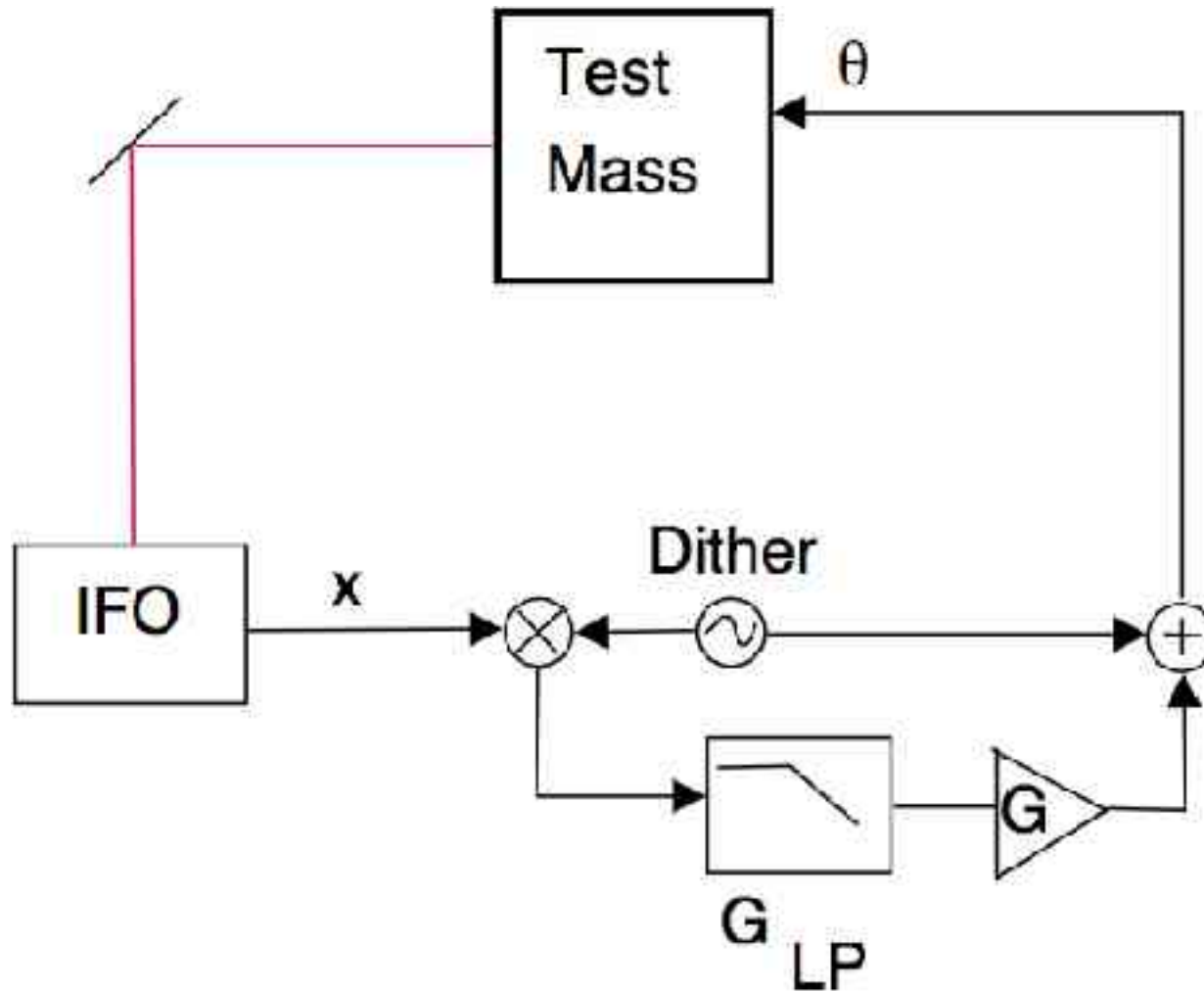


Intensity ↑

Position →



Dithered alignment -- concept

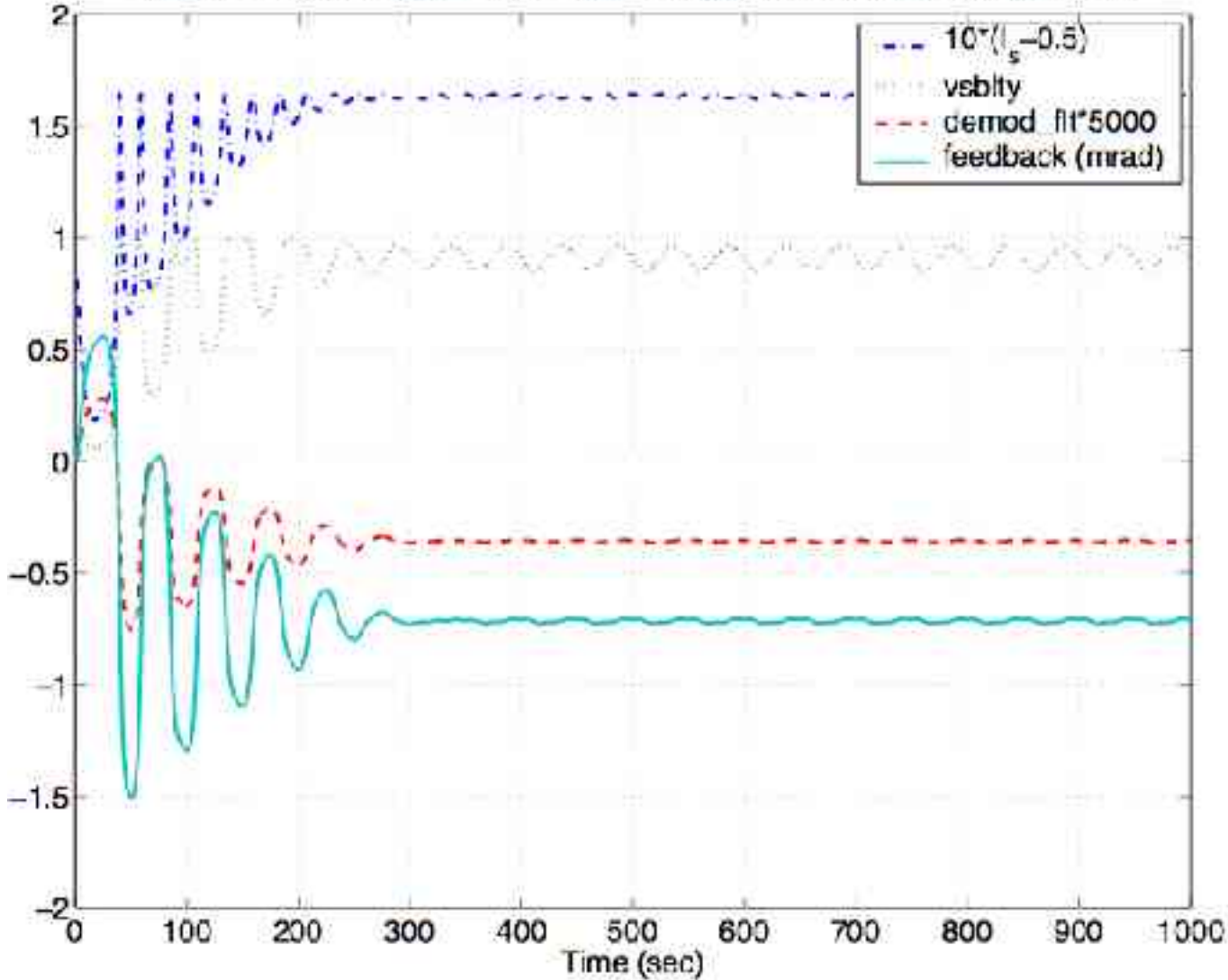




Dithered alignment -- Simulink run



th_offset = 1.0e-03; ph_offset = 0.3; h_offset = 20 um
ampltd = 1.0e-04; tmod = 0.02 HzLP, 1-pole, 4.0e-05 Hz; fb_gain = 10.0

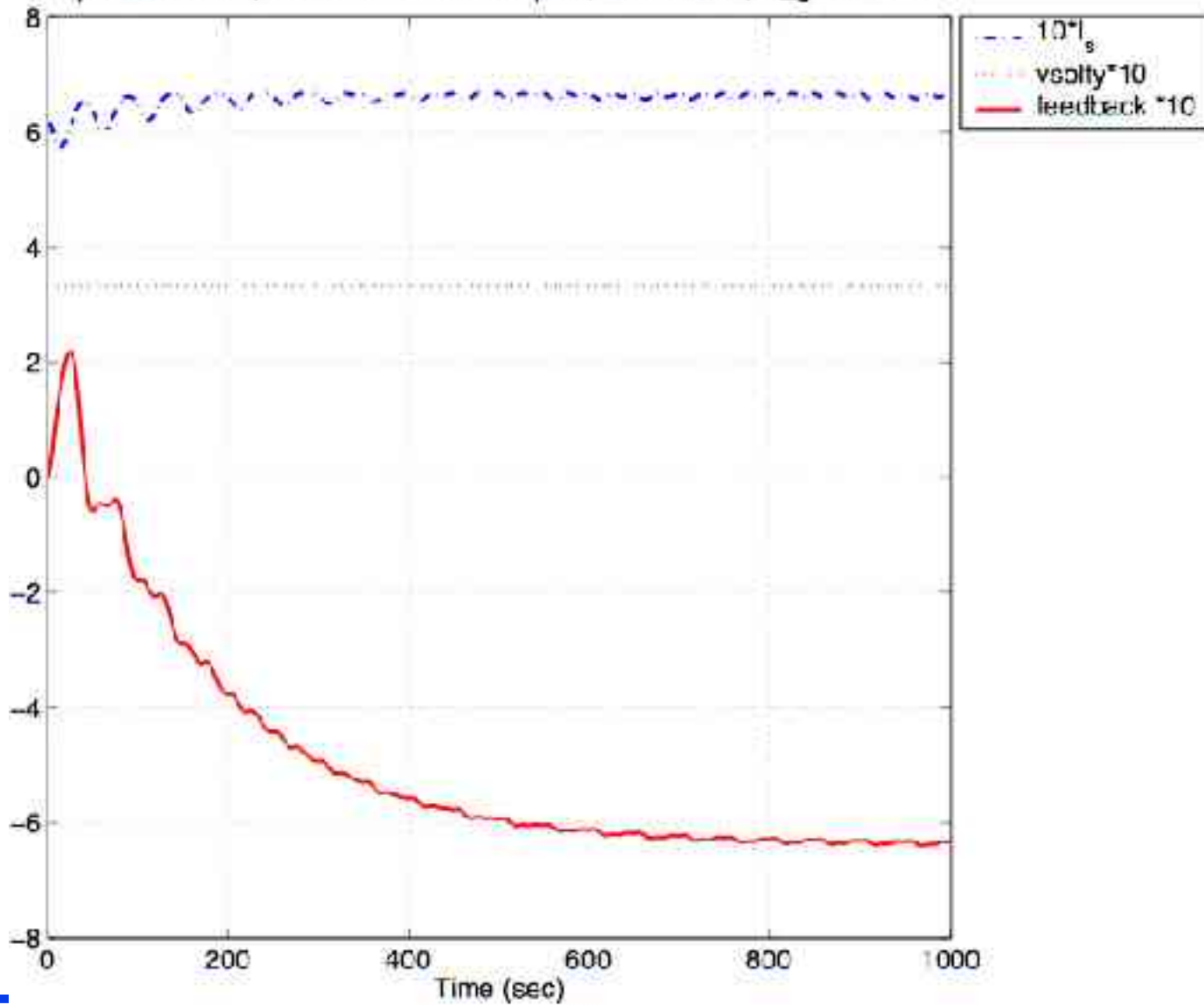


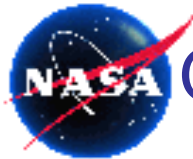


Bright fringe finder -- Simulink run

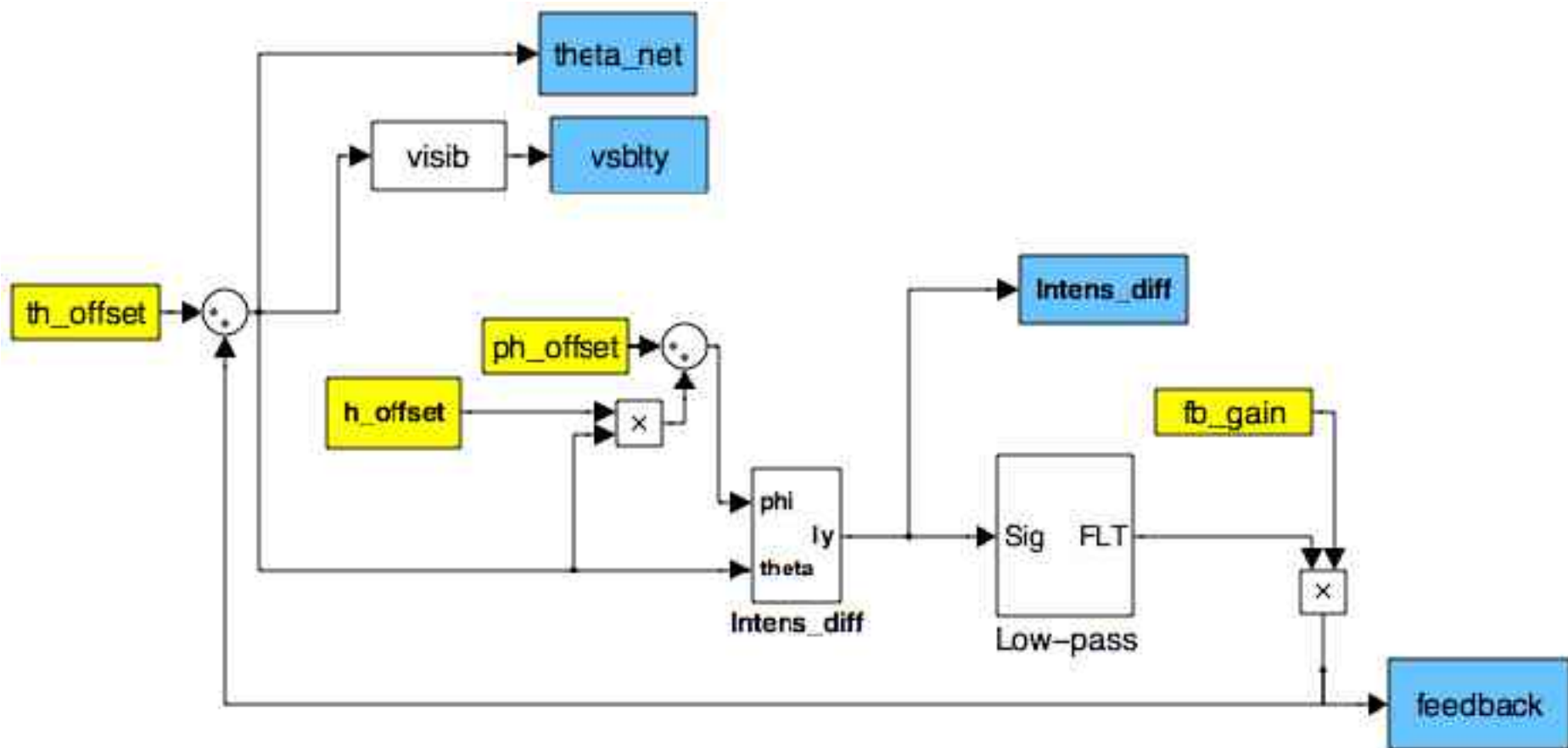


Fringe Dither — $th_offset = 1.0e-03$; $ph_offset = 2.0$; $h_offset = 20 \mu m$
 $ampltd = 3.0e-01$; $freqd = 0.02 \text{ Hz}$ LP 1-pole, $4.0e-05 \text{ Hz}$; $fb_gain = 1000.0$





QPD difference alignment -- Simulink model

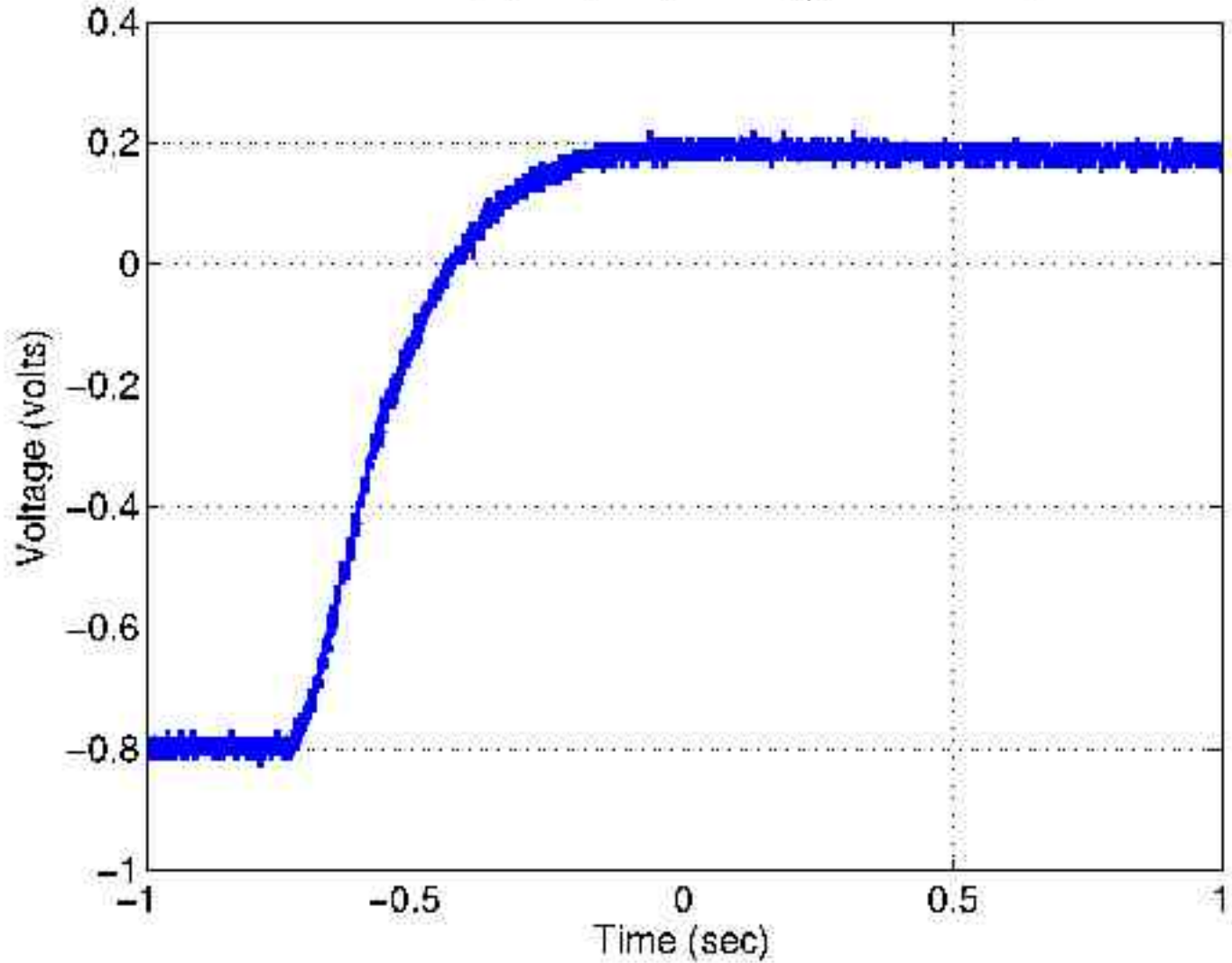


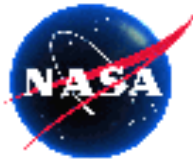


QPD difference alignment -- Experiment

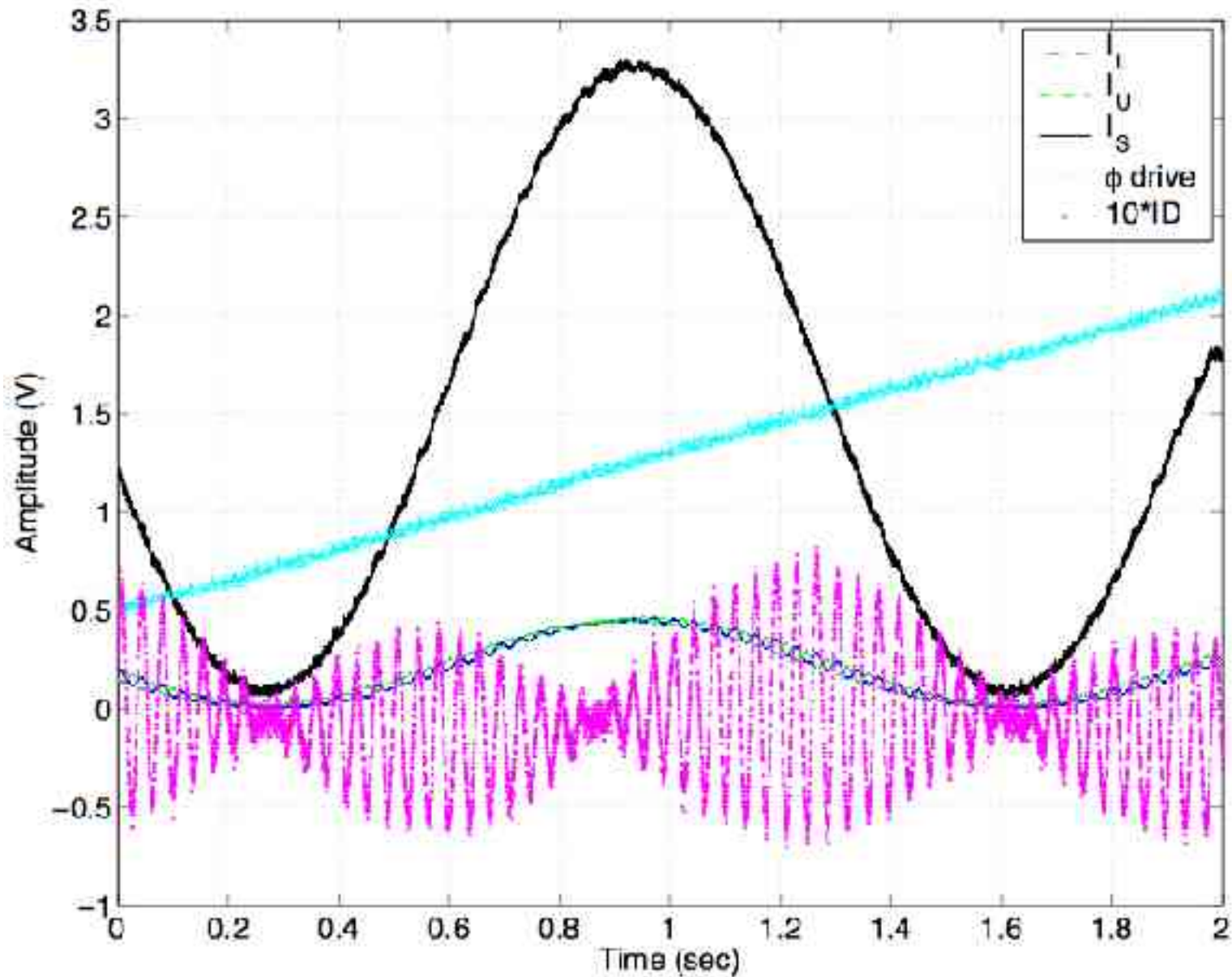


DAC output, step response, I_y Labview loop



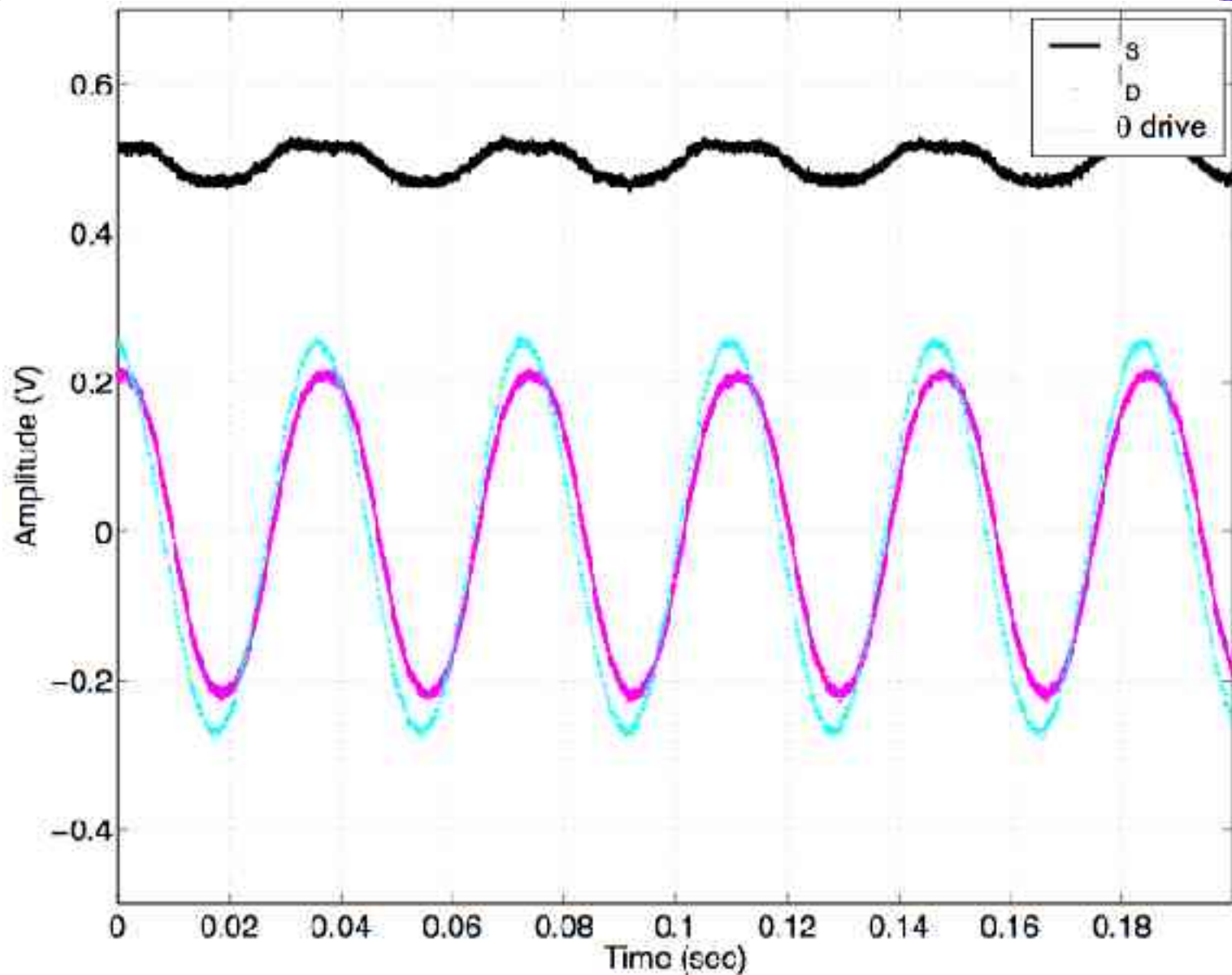


QPD difference signal alignment sensitivity





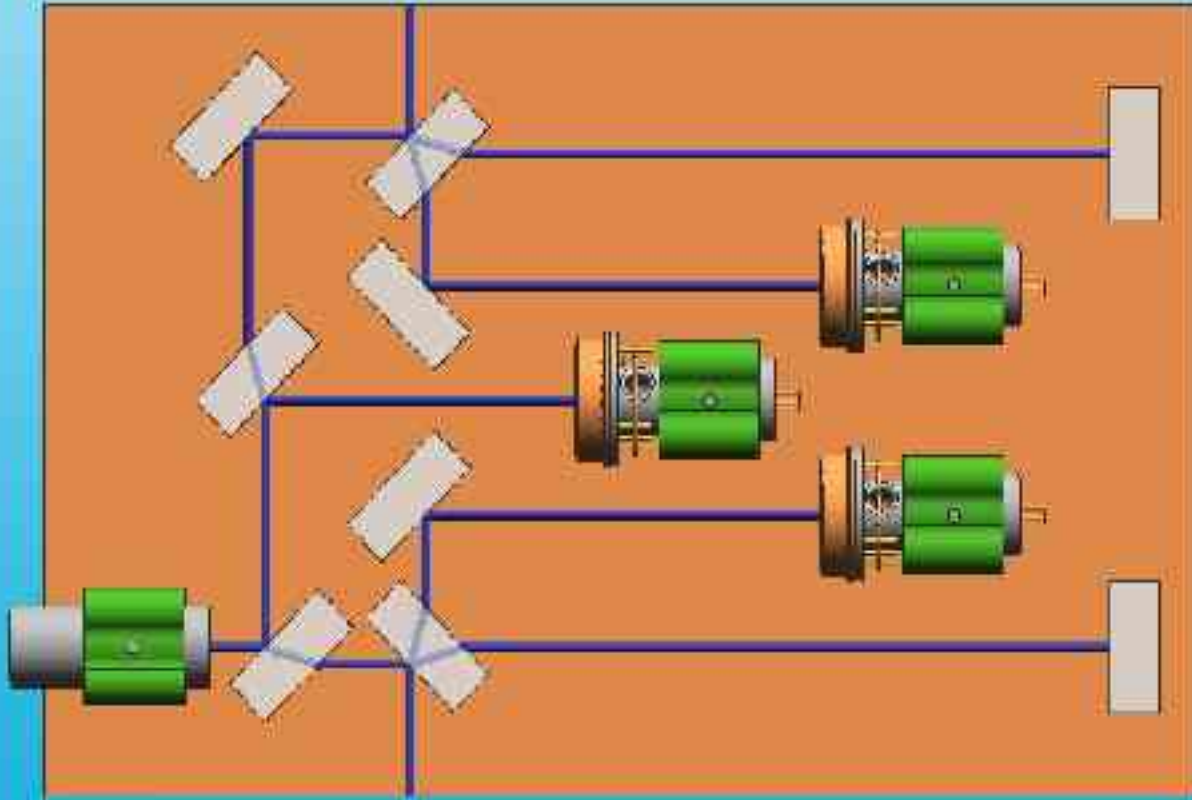
Sum vs. difference signals at half-fringe



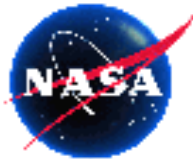
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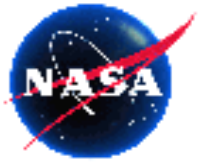


ERROR SOURCE	TERMS	VALUE	pm/rthz	Corrltn
Intensity Noise Equation 6	RIN $I_0(f)$ (1/rthz)	1.0E-02	0.2	A
	Non-simultaneity tau (sec)	5.0E-04		
	Frequency f (Hz)	3.0E-02		
Frequency Noise Equation 10	Arm length diff Delta L (m)	1.5E-04	5.3	A
	Frequency Noise nu (f) (Hz/rthz)	1.0E+07		
Analog Electronic Noise Equation 7	Half-max point V_0 (V)	2.0E+00	0.8	
	Voltage noise $V(f)$ (V/rthz)	1.0E-05		
Digitization Noise Equation 9	Sample rate f_s (Hz)	1.0E+00	1.2	
	ADC quantization (V)	5.0E-05		
Mirror angle sensitivity (Running, Equation 12)	Angle jitter $\theta(f)$ (rad/rthz)	1.0E-06	13.2	
	Mirror-splitter distance p (m)	1.0E-01		
	Mis-centering h (m)	2.0E-05		
	Drift from half-fringe x (m)	3.0E-08		
Mirror angle sensitivity (Initialization error)	Misalignment θ_0	1.0E-04	10.0	
Transverse displacement Equation 14	Beam displacement y_0 (m)	2.0E-04	0.2	B
	Transverse motion $y(f)$ (m)	1.0E-08		
Transversion test mass Equation 16	Coupling constant μ	3.0E-04	3.0	B
Thermal optical bench Equation 17	Temperature $T_b(f)$ (K/rthz)	1.0E-04	10.0	C
	Arm length (m)	2.0E-01		
	Tempo κ_b (/K)	5.0E-07		
Thermal, transmissive optics, Equation 18	BK7 total K_{BK7} (1/K)	9.0E-06	11.8	C
	Window thickness, t_W (m)	4.0E-03		
	Fused silica total K_{FS} (1/K)	1.2E-05		
	Algmnt cube thckns, t_A (m)	5.0E-03		
	Splitter thickness t_S (m)	6.0E-03		
	Splitter index, nS	1.4E+00		
Splitter t_{sO} (calculated, m)	6.9E-03			
Diffrentl Thrml, DiffTh			10.0	
SUM				29.9



TUM WEBX





Backups



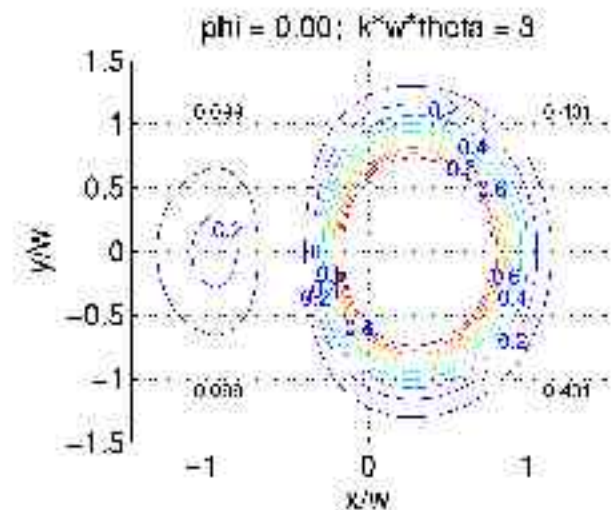
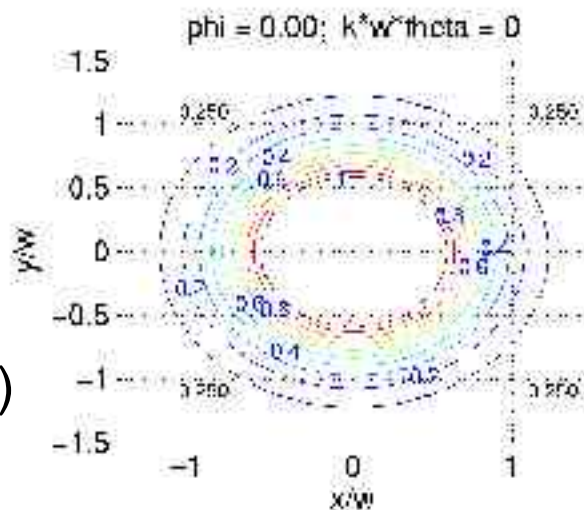
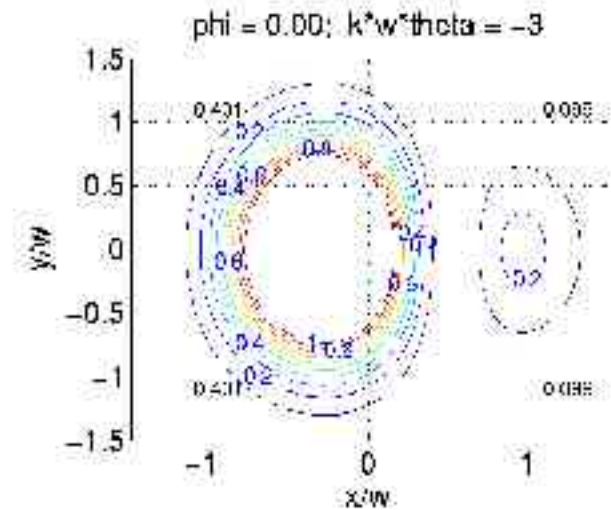
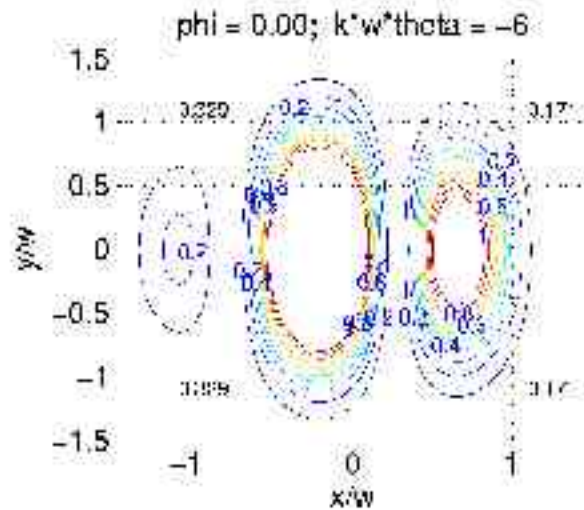


Intensity Pattern with Misalignment



- Horizontal misalignment shown.
- Pattern insensitive to fringe offset near mid-fringe.
- Sample with 4 pixels (quadrant photodiode). Difference/sum response:

$$dQ/d\theta = \sqrt{8kw/\pi^3}$$

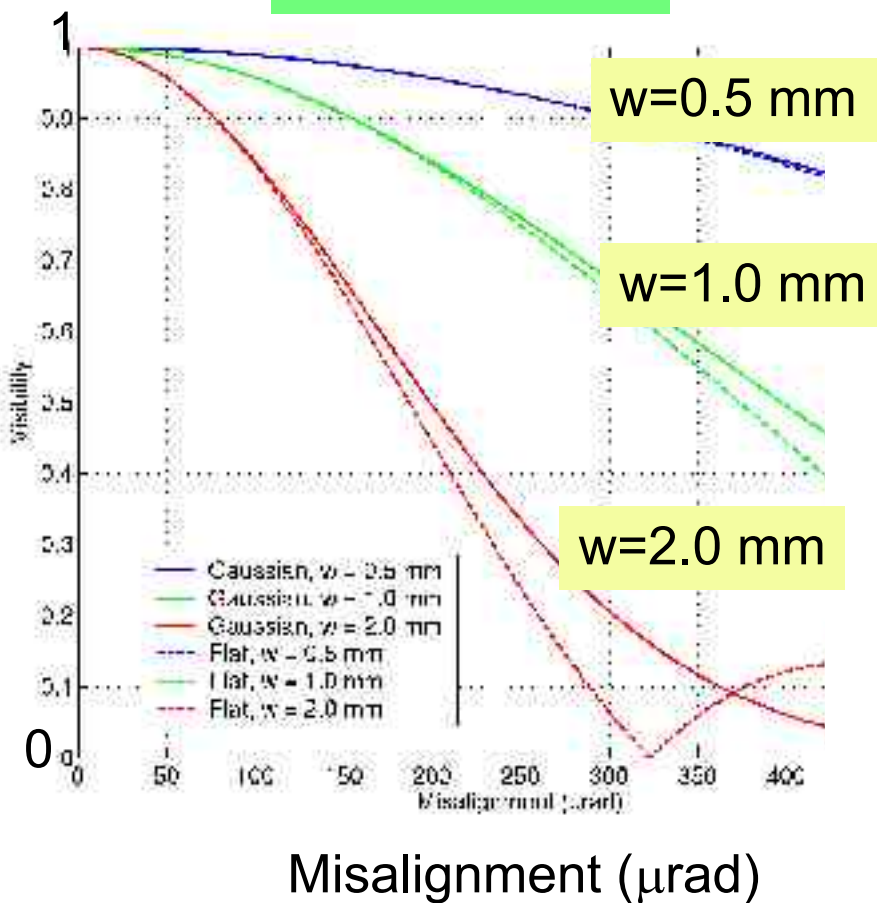




Static Misalignment and Static Longitudinal Error



Fringe Visibility



Error Sensitivity

